

CTTRANS  
A MONTE CARLO PROGRAM FOR RADIATIVE  
TRANSFER IN PLANE PARALLEL ATMOSPHERES  
WITH IMBEDDED FINITE CLOUDS --  
DEVELOPMENT, TESTING AND  
USER'S GUIDE

Prepared for  
National Aeronautics and Space Administration  
Goddard Space Flight Center  
Greenbelt, Maryland 20771

(NASA-CR-166759) CTRANS: A MONTE CARLO  
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PARALLEL ATMOSPHERES WITH IMBEDDED FINITE  
CLOUDS: DEVELOPMENT, TESTING AND USER'S  
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**WASHINGTON ANALYTICAL SERVICES CENTER, INC.**

WOLF RESEARCH AND DEVELOPMENT GROUP

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## SECTION 1.0

### INTRODUCTION

This report describes the program called CTRANS which has been designed to perform radiative transfer computations in an atmosphere with horizontal inhomogeneities (clouds). Since the atmosphere-ground system was to be richly detailed, the Monte Carlo method was employed. This means that results are obtained through direct modeling of the physical process of radiative transport. The effects of atmospheric or ground albedo pattern detail are essentially built up from their impact upon the transport of individual photons. CTRANS actually tracks the photons backwards through the atmosphere, initiating them at a receiver and following them backwards along their path to the sun as shown schematically in Figure 1.0.1. Backwards tracking has several advantages: the pattern of incident photons generated through backwards tracking automatically reflects the importance to the receiver of each region of the sky. Further, through backwards tracking, the impact of the finite field of view of the receiver and variations in its response over the field of view can be directly simulated. The backwards tracking method, additionally, is well suited for segregating results according to the character of the final scattering suffered prior to entering the receiver.

Section 2.0 describes the backwards tracking Monte Carlo method. In Section 3.0, the results of a range of test applications are reported which serve to illuminate the capabilities and limitations of the program. Section 4.0 contains brief descriptions of each routine comprising CTRANS. Since CTRANS is a highly generalized program with many operational modes and a variety of data structures, Section 5.0 outlines the input parameters. Finally, Section 6.0 contains a FORTRAN listing of CTRANS.



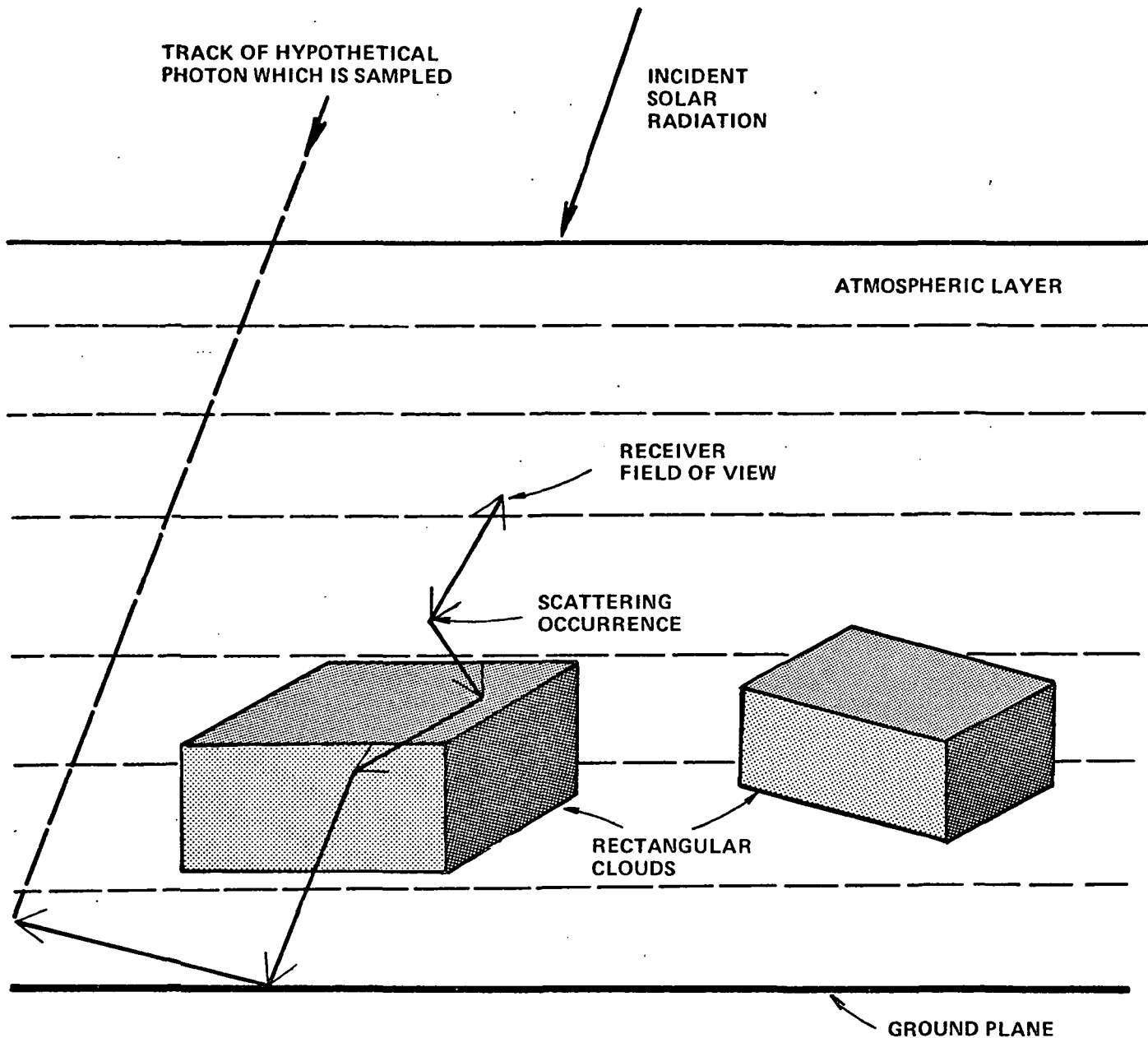


FIGURE 1.0.1. SCHEMATIC REPRESENTATION OF THE PROBLEM GEOMETRY AND THE BACKWARDS MONTE CARLO METHOD

## SECTION 2.0

### MONTE CARLO METHOD

CTRANS employs the Monte Carlo method to compute flux or intensity upon a receiver situated in or above a plane parallel atmosphere. Photons are tracked backwards through the atmosphere from the receiver along their path to the sun.

The particular advantage offered by the Monte Carlo method lies in the degree of complexity of the earth-atmospheric system which can be modeled.

The present code can handle a plane parallel atmosphere with up to 100 homogeneous layers. Each layer can be composed of up to five distinct scattering (or absorbing) species: molecular scatterers, monodisperse or polydisperse aerosols or hazes, ozone, etc. Further, there may be up to 10 finite rectangular solid clouds which are superimposed upon the layered atmosphere. Each cloud may be composed of any of the five allowed active atmospheric components with an independently specified density for each cloud. Thus, the atmosphere may be inhomogeneous both vertically and horizontally.

The treatment of ground reflection is also generalized. Reflectance at the ground may be either Lambertian or Fresnel in character. Fresnel regions are further characterized by a surface roughness specified by a probabilistic slope distribution (so chosen as to provide an approximate model of a sea surface with waves). The ground plane need not be uniform; rough Fresnel and Lambertian regions may be intermixed in a patchwork fashion as specified by a reflectance type map. Any Lambertian regions may be further broken down into patches having different Lambertian albedos. Results are computed for up to 50 different overlying maps of the Lambertian albedo, simultaneously. Aside from the gain in computational efficiency,

this is important because it provides a means for computing the relative effects of changing the ground albedo pattern with a precision which far surpasses the absolute precision of the Monte Carlo results for a single map.

## 2.1 PHOTON TRANSPORT AND SAMPLING

CTTRANS tracks photons backwards initiating them at the receiver and following them through successive scatterings on their path through the atmosphere. Backwards tracking has been adopted for a number of reasons. It permits the efficient and direct simulation of receivers with finite fields of view and/or finite extent. A forward tracking scheme would require the distribution of initial photons over a wide area when horizontal inhomogeneities are present and this would introduce large variances in the results. By initiating photons at the receiver, this source of variance is largely avoided.

To understand backward tracking, consider first a single scattering event. If  $\underline{I}_0$  is the Stokes vector of incident unscattered light,  $\underline{S}$  is the scattering phase matrix and  $\underline{R}$  is a rotation matrix which serves to rotate the plane of reference of the Stokes vector into the scattering plane, the Stokes vector after scattering  $\underline{I}_f$  is given by

$$\underline{I}_f = \underline{R}_r \underline{S} \underline{R} \underline{I}_0$$

where  $\underline{R}_r$  rotates the final Stokes vector into the reference plane of the receiver. After two scatterings, the final Stokes vector will be

$$\underline{I}_f = \underline{R}_r \underline{S}_2 \underline{R}_2 \underline{S}_1 \underline{R}_1 \underline{I}_0$$

Cast in this way, it is apparent that what is important is the product matrix which is built from the scattering matrices appropriate to the string of scatterings suffered by the photon. This product can be built up either from the left or from the right with the same result; i.e., we may equally well follow the photon's history forward or backwards if we accumulate scatterings properly into the product [which we call the cumulative scattering matrix].

There is a further advantage in tracking backwards: contributions from several solar directions may be accumulated from a single track. For example, if the photon is tracked backwards from the receiver, only the last rotation and scattering contain any reference to solar direction. Replacing one sun by another means changing only these two matrices. For each solar direction, at most, two  $4 \times 4$  matrix multiplications must be performed.

Photons are initialized at the receiver; which may be general in the following ways: it may have finite or infinitesimal (conical) field of view; it may be oriented pointing toward any zenith angle with any azimuthal angle; it may be at any altitude and have any specified x-y coordinate. On the other hand, for flux calculations the receiver aperture may be finite. This is accomplished by letting the receiver be an entire cloud face (any face of any cloud, pointing into or out of the cloud).

First, initial photon coordinates are created. If the receiver is a cloud face, initial photon coordinates are chosen from a uniform distribution over the cloud face. The photon direction is then determined using: 1) uniform distribution over solid angle for a cloud-face receiver, or 2) cosine distribution over the conical field of view of an infinitesimal receiver, or 3) in a specified direction if the field of view



is infinitesimal. For each type of distribution, the appropriate weight is computed (to be multiplied into the sampled values upon sampling).

The distance to be traversed to a scattering is computed on the basis of optical distance to be traversed: if  $\rho$  is a uniformly distributed random number, the optical distance to be traversed is given by

$$\tau = -\ln \rho \quad (2.1.1)$$

Through reference to a table containing the optical thickness of each layer of the ambient atmosphere and taking into account the added optical density in the interior of clouds, the optical distance traversed and physical distance traversed are incremented until an optical distance  $\tau$  has been reached. If, before this has occurred, the photon exits the atmosphere, the photon is terminated. If the photon strikes the ground, the scattering will be a ground scattering and a ground scattering indicator is set (ISCAT=1).

Having located the position of a scattering, the scatterer type is chosen on the basis of the relative contribution of each scattering species at that point to the local optical density. Here, a cumulative distribution function, which has been tabulated for each layer of the ambient atmosphere, is used in conjunction with any additional optical density due to the presence of a cloud. Photons are not explicitly absorbed. Instead, a weight is accumulated which at any point along the path reflects the probability that the photon has not been absorbed.

After having determined the scatterer type, the probability that the photon could have come from each sun is sampled. If  $\underline{S}_I$  is the cumulative scattering matrix at the point of sampling, the sampled Stokes vector will be

$$\underline{I}_s = \underline{S}_j \underline{R}_j \underline{S}_j \underline{I}_o e^{-t_j w} \quad (2.1.2)$$

Where  $R_j$  is a rotation matrix appropriate to a scattering into the  $j^{\text{th}}$  solar direction;  $S_j$  is a scattering matrix (a Mueller matrix if the scatterer is an atmospheric constituent);  $I_o$  is the incident Stokes vector;  $t_j$  is the total optical distance along the path connecting the scattering point and sun<sub>j</sub>;  $w$  is a weight reflecting the probability that the photon has not been absorbed (including ground absorption for Lambertian regions encountered). There will be a different value for  $w$  for each Lambertian albedo map. Note that the above form assumes that  $\underline{I}_o$  represents initially unpolarized light. If the incident light from the sun were polarized, an additional rotation would be necessary.  $R_j$  has the form

$$R_j = \begin{pmatrix} 1 & 0 & 0 & 0 \\ 0 & \cos 2X & \sin 2X & 0 \\ 0 & -\sin 2X & \cos 2X & 0 \\ 0 & 0 & 0 & 1 \end{pmatrix} \quad (2.1.3)$$

where  $X$  is the rotation angle between the normal to the previous scattering plane (or the reference direction in the case of first scatterings) and the normal to the scattering plane for a scattering into the  $j^{\text{th}}$  solar direction.  $S_j$  has the general form

$$S_j = \frac{1}{4\pi} \begin{pmatrix} S_{11} & S_{12} & 0 & 0 \\ S_{12} & S_{22} & 0 & 0 \\ 0 & 0 & S_{33} & S_{34} \\ 0 & 0 & -S_{34} & S_{44} \end{pmatrix} \quad (2.1.4)$$

where  $S_{\ell,m}$  depends upon scattering angle. For Rayleigh scattering,  $S_{11} = S_{22} = \frac{3}{4} (1 + \cos^2 \beta_j)$

$$S_{12} = \frac{3}{4} (\cos^2 \beta_j - 1)$$

$$S_{33} = S_{44} = \frac{3}{2} \cos \beta_j$$

$$S_{34} = 0$$

where  $\beta_j$  is the scattering angle for a scattering into the  $j^{\text{th}}$  solar direction. For Lambertian scattering at the ground,  $S_{11} = 4 \cos \theta_j$ , where  $\theta_j$  is the zenith angle of the  $j^{\text{th}}$  sun and all other matrix elements are zero. Lambertian reflection thus is perfectly depolarizing.

Mie scattering and Fresnel scattering both have matrices with the form of Eq. (2.1.4). Mie elements are stored in tabular form and values for particular scattering angles are obtained by interpolation. The Fresnel matrix elements are given in the discussion of ground reflectance.

The next step after sampling is to accumulate a "real" scattering. Knowing the scatterer type, an appropriate scattering angle is found. If the scattering angle were chosen from a uniform distribution, and if the scattering matrix appropriate to the medium exhibited sharp peaks, then most photons would rapidly lose weight and large numbers of photon tracks would be necessary in order to achieve a reasonably small variance. To resolve this difficulty, we use the concept of importance sampling. We choose the scattering direction from a biased distribution designed to maximize the resultant contribution. The bias thus introduced is then removed by applying a weight. More concretely, we wish to fold in a scattering matrix

$$S = \begin{pmatrix} S_{11} & S_{12} & 0 & 0 \\ S_{12} & S_{22} & 0 & 0 \\ 0 & 0 & S_{33} & S_{34} \\ 0 & 0 & -S_{34} & S_{44} \end{pmatrix} \frac{dw}{4\pi}$$

$$= \frac{1}{f(\beta)} \begin{pmatrix} S_{11} & S_{12} & 0 & 0 \\ S_{12} & S_{22} & 0 & 0 \\ 0 & 0 & S_{33} & S_{34} \\ 0 & 0 & -S_{34} & S_{44} \end{pmatrix} \frac{f(\beta) \, dw}{4\pi} \quad (2.1.5)$$

Instead of choosing the scattering angle from a probability distribution corresponding to the probability density  $\frac{dw}{4\pi}$  (uniform), we use the distribution corresponding to the probability density  $\frac{f(\beta) \, dw}{4\pi}$ . The weight of the photon following the scattering can thus be maximized by choosing  $f(\beta)=S_{11}$  times a constant chosen so that the first matrix element is always unity. A real scattering is accumulated by multiplying into the cumulative scattering matrix first a rotation, and then the scattering matrix.

The process is repeated until either a designated maximum number of scatterings have been suffered, the photon leaves the atmosphere or its weight drops below the assigned threshold (due, for example, to atmospheric absorption).



## 2.2 ENCOUNTERS WITH CLOUDS

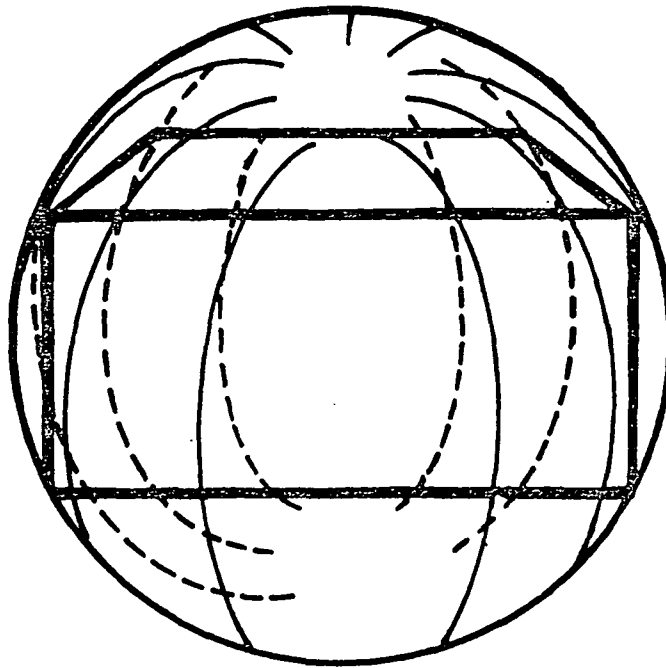
The presence of finite clouds complicates the evaluation of the fate of the path of the photon in that there is no simple way to determine if a given straight line in space enters a specified rectangular box. It was therefore necessary to undertake an analysis to find optimum procedures for evaluating the path as quickly as possible.

This analysis is applied in two areas of the program:

1. In evaluating the path of the "backward" photon to the "previous" scattering.
2. In computing the probability that a "forward" hypothetical photon would reach a given scattering point from the Sun without scattering.

The problem has been treated in two parts. First, we have found a quick and efficient method for eliminating clouds which could not possibly be entered by the photon path, and secondly, we have performed a detailed analysis to evaluate the uneliminated clouds.

There is a simple method for determining whether it is possible for a straight line to enter a given rectangular cloud. The approach is to circumscribe the cloud with a sphere, the center of which coincides with the center of mass of the cloud. The radius,  $r$ , of the sphere can be taken to be  $(a^2+b^2+c^2)^{1/2}$  where the lengths of the sides of the cloud are  $(2a, 2b, 2c)$ . In this case the eight corners of the box lie on the sphere as illustrated in Figure 2.2.1.



**FIGURE 2.2.1. ILLUSTRATION OF CIRCUMSCRIBING SPHERE CONCEPT**

Since the sphere completely contains the cloud then if a line cannot enter the sphere, it cannot enter the cloud. Thus, the first check should be to find if the path can enter any cloud circumscribing spheres. We shall present the analysis for a single cloud with the understanding that this must be repeated for all clouds in the program.

Suppose we have a line with direction cosines  $(c_x, c_y, c_z)$  leaving a point  $A(x_1, y_1, z_1)$ . The equation of the line is

$$\frac{x-x_1}{c_x} = \frac{y-y_1}{c_y} = \frac{z-z_1}{c_z} \quad (2.2.1)$$

The distance,  $R$ , of the point  $O (X, Y, Z)$  from  $A$  is

$$R = \{(X-x_1)^2 + (Y-y_1)^2 + (Z-z_1)^2\}^{1/2} \quad (2.2.2)$$

and the point of closest approach of the line to  $O$  is such that  $AP$  is perpendicular to  $OP$ , as illustrated in Figure 2.2.2. Now the cosine of the angle  $OAP$  is given by the dot product of the direction cosines of  $AP$  and  $AO$ ; i.e.,

$$\cos OAP = \frac{(X-x_1)c_x}{R} + \frac{(Y-y_1)c_y}{R} + \frac{(Z-z_1)c_z}{R} \quad (2.2.3)$$

But the distance  $AP$  is given by  $R \cos OAP$ ; i.e.,

$$AP = (X-x_1)c_x + (Y-y_1)c_y + (Z-z_1)c_z \quad (2.2.4)$$

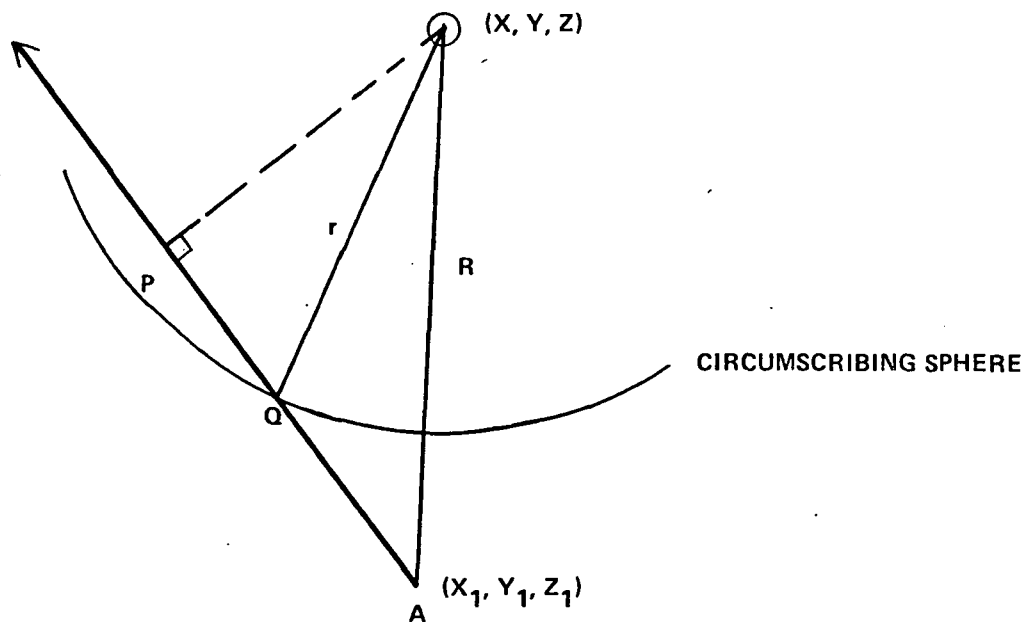


FIGURE 2.2.2. ILLUSTRATION OF POINT OF CLOSEST APPROACH OF A LINE TO A POINT



and by Pythagorus's theorem,

$$\begin{aligned} OP^2 &= R^2 - AP^2 \\ &= R^2 - \{(X-x_1)c_x + (Y-y_1)c_y + (Z-z_1)c_z\}^2 \end{aligned} \quad (2.2.5)$$

Now, if  $OP^2$  is greater than  $r^2$ , the squared radius of the circumscribing sphere, then the path cannot enter the sphere. Also, if the quantity in curly parentheses is negative, then again entry is impossible.

Note that  $OP^2$  can be computed in the general coordinate system and that no square roots or complicated functions are necessary for its evaluation.

If we are tracking the path of the backward photon then another check can be made. Although the point of closest approach may be inside the circumscribing sphere, it may be that the length,  $L$ , of the path is insufficient to reach the sphere. Suppose, in Figure 2.2.2 that the line reaches the sphere at  $Q$ . Then  $OQ$  has length  $r$ , the radius of the sphere. Now from (2.2.4) and (2.2.5) we are able to evaluate both  $OP$  and  $AP$  and by Pythagorus's theorem we have that

$$QP^2 = r^2 - OP^2 \quad (2.2.6)$$

Thus we are able to evaluate the distance to the sphere as

$$AQ = AP - QP \quad (2.2.7)$$

which may be evaluated by (2.2.4) and (2.2.6). Testing this value against  $L$  gives us another possible means of cloud elimination.

We have attempted to use the circumscribing sphere concept further, but we finally concluded that there are some dangers in its further application. For example, the sequence of distances along the path to a cloud need not be the same as the sequence of distances to the circumscribing spheres or the point of closest approach. An illustration of such a case is given in Figure 2.2.3. The reason for the difficulty is that the circumscribing sphere gives no information as to cloud orientation and can therefore mask orientation differences which may be important. For this reason we proceed in the program at this point to a completely general analysis.

The first step in treating an uneliminated cloud is to convert to the coordinate system of the cloud. Thus the location of the scattering point  $(x_1, y_1, z_1)$  is transformed to  $(x_{1c}, y_{1c}, z_{1c})$  using

$$\begin{aligned} x_{1c} &= (x_1 - X) \cos \theta_c + (y_1 - Y) \sin \theta_c \\ y_{1c} &= -(x_1 - X) \sin \theta_c + (y_1 - Y) \cos \theta_c \\ z_{1c} &= z_1 - Z \end{aligned} \tag{2.2.8}$$

where  $\theta_c$  is the orientation angle of the cloud and  $(X, Y, Z)$  are the coordinates of the center of mass of the cloud. The direction cosines of the line are transformed to the cloud system using

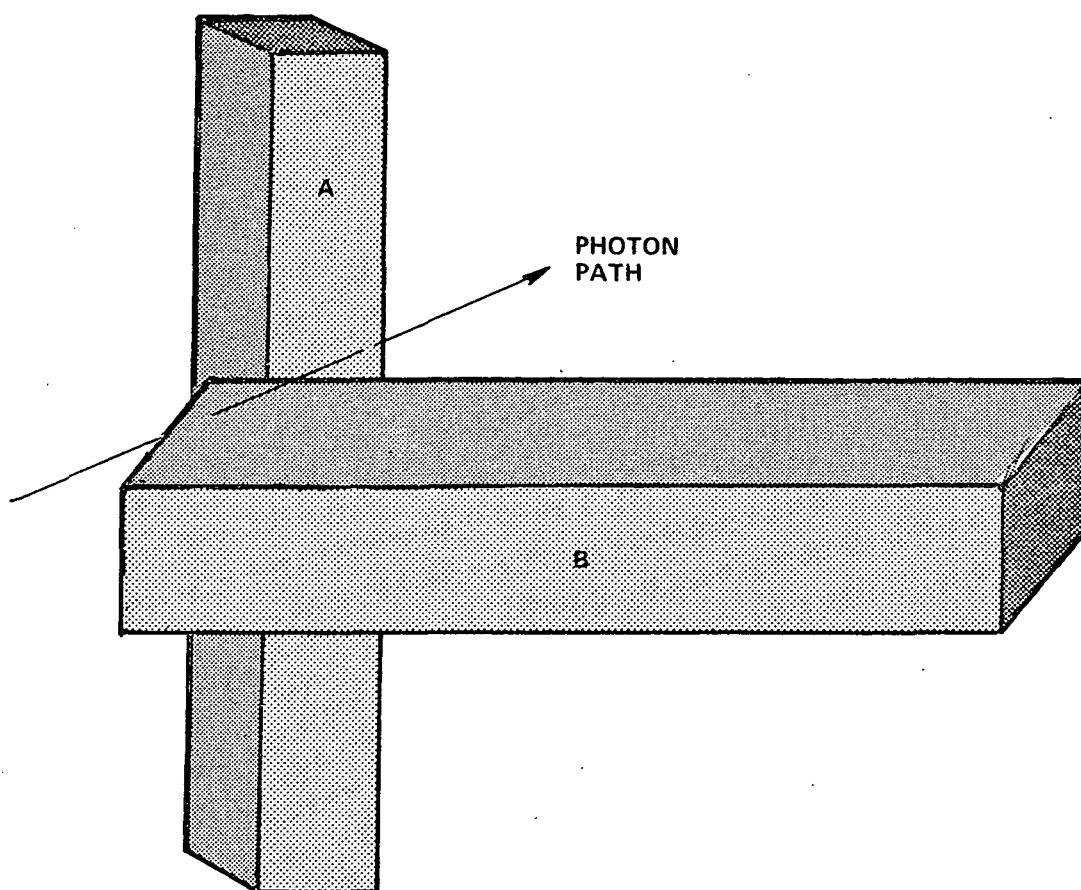


FIGURE 2.2.3. EXAMPLE OF SEQUENCING FAILURE OF CIRCUMSCRIBING SPHERES ALGORITHM

$$C_{cx} = C_x \cos\theta_c + C_y \sin\theta_c$$

$$C_{cy} = -C_x \sin\theta_c - C_y \cos\theta_c \quad (2.2.9)$$

$$C_{cz} = C_z$$

We shall present the analysis for determining if the photon enters a side perpendicular to the cloud x axis. In the computer program we index terms relating to the cloud x, y and z axes 1, 2 and 3, respectively. The analysis for the sides perpendicular to the y and the z axes can then be performed by merely rotating the ordered index set (1,2,3) to (2,3,1) and (3,1,2), respectively.

The following tests will be performed in sequence.

1. Is  $|x_{1c}| \leq a$ , the half length of the edges (2.2.10)  
parallel to the cloud x axis.

If this condition is satisfied, then the photon cannot possibly enter a face perpendicular to the cloud x axis.

2. If  $x_{1c} < -a$ , then the path can enter the face  $x_c = -a$ . In this case, set  $q = -a$ .

If  $x_{1c} > a$ , then the path can enter the face,  $x_c = a$ . In this case, set  $q = a$ .

3. Compute  $(x_{1c} - q) \cdot C_{cx}$ . If this is positive, then the photon is traveling away from the face,  $x_c = q$ , and will not enter the cloud.



4. Compute the  $(y_c, z_c)$  values of the point of intersection of the line with the plane,  $x_c=q$ . These are given by

$$\left. \begin{aligned} y_{cI} &= y_{1c} + C_{cy} \frac{q - x_{1c}}{C_{cx}} \\ z_{cI} &= z_{1c} + C_{cz} \frac{q - x_{1c}}{C_{cx}} \end{aligned} \right\} \quad (2.2.11)$$

5. Check to see if both the conditions (2.2.12) apply.

$$\left. \begin{aligned} |y_{cI}| &< b \\ |z_{cI}| &< c \end{aligned} \right\} \quad (2.2.12)$$

If these are both true, then the photon enters the cloud at the point  $(q, y_{cI}, z_{cI})$ . Otherwise, entry does not occur at the  $x=q$  plane.

When it is determined that a photon has entered a given cloud then the tracking mechanism from that point on will be performed in the cloud coordinate system.

If it is determined that a later scattering point  $(x_{1c}, y_{1c}, z_{1c})$  lies outside the cloud then we determine the exit point using steps (4) and (5) only.

For evaluating the track of the "forward" hypothetical photon from the Sun to a scattering center we will determine if the direction cosine  $C_{cxs}$  of the line from the scattering point to the Sun is positive or negative. (The solar direction cosines ( $C_{cxs}$ ,  $C_{cys}$ ,  $C_{czs}$ ) will be computed for each cloud prior to the simulation.) If  $C_{cxs}$  is positive, we set  $q=a$ , whereas if it is negative, we shall set  $q=-a$ . At this point steps (4) and (4) are employed to find the point of exit from the cloud.

### 2.3 GROUND SCATTERING

CTRANS has the capability to model reflections from a spatially inhomogeneous ground. In the present version of the code, the physical mechanism of reflection may be modeled as either Lambertian reflection or as Fresnel reflection from a rough surface and these modes may be intermixed in a patchwork fashion.

Reflectance type is basically controlled by a reflectance type map which dictates the reflectance character from point to point across the infinite ground plane. When a photon strikes the ground, its impact coordinates are computed and then used to decide whether the point of impact was within a Lambertian or a rough Fresnel region.

Since Lambertian reflection is not physically dependent upon the direction of incidence or reflection but only upon a scalar Lambertian albedo, CTRANS can model simultaneously the effect of several values (up to 50) of the albedo for each of the Lambertian regions. This is accomplished in the following way: A vector of scalar weights is maintained; one for each albedo map. When a Lambertian scattering occurs, the albedo at the point of impact is determined for each of the albedo maps and this is multiplied into the corresponding albedo weight to obtain a new weight for subsequent use. Upon sampling, each current albedo weight is folded into the sampled Stokes vector to obtain samples corresponding to each of the allowed albedo maps. If the impact point lies within a Fresnel region, however, the vector of albedo weights is left unchanged (since it represents the cumulative effects of only the Lambertian regions).

Symbolically, the entire reflection process is as follows: given an old cumulative scattering matrix  $S_o$ , the new one,  $S_N$ , is computed as:

$$S_N = S_o R s$$

where  $R$  is a rotation matrix and  $s$  depends upon the reflection type at the impact point:

$$\begin{array}{ll} \text{Lambertian} & s = \begin{pmatrix} \cos \theta & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \end{pmatrix} \\ \\ \text{Fresnel} & s = \begin{pmatrix} S_{11} & S_{12} & 0 & 0 \\ S_{12} & S_{11} & 0 & 0 \\ 0 & 0 & S_{33} & 0 \\ 0 & 0 & 0 & S_{33} \end{pmatrix} \end{array}$$

where  $S_{ij}$  represent Fresnel matrix elements:

$$S_{11} = (R_{11}^2 + R_1^2)/2$$

$$S_{12} = (R_{11}^2 - R_1^2)/2$$

$$S_{33} = R_{11} R_1$$

and

$$R_{11} = \frac{n \cos \chi_i - \cos \chi_t}{n \cos \chi_i + \cos \chi_t}$$

$$R_1 = \frac{\cos \chi_i - n \cos \chi_t}{\cos \chi_i + n \cos \chi_t}$$

$n$  = relative index of refraction of the surface

$\chi_i$  = angle of incidence

$\chi_t$  = angle of refraction, computed from  $\chi_i$  through Snell's law at the interface:  $n \sin \chi_t = \sin \chi_i$ .

The vector of scalar weights is renewed according to

$$A_i^{\text{new}} = A_i^{\text{old}} \times a_i(J; X, Y)$$

$X, Y$  = coordinates of impact point

$J=0$  = region is Lambertian and the values of  $a_i (i=1, 50)$  are determined from the Lambertian albedo maps according to the coordinates  $(X, Y)$

$J=1$  = region is Fresnel  $a_i = 1 (i=1, 50)$ .

The two kinds of ground maps (Lambertian albedo maps and the reflectance type map) are specified in CTRANS in two different ways.

The Lambertian albedo maps are specified in a fixed form by the subroutine ALBEDO. To change albedo map structures one version of ALBEDO is interchanged with another. The possible variety of maps is thus limited only by the imagination. ALBEDO, in addition to its function of providing specific values of the scalar weights at a specified point has the function of writing out text to describe the various maps.

The reflectance type map is specified by options read in by subroutine INPUT and is therefore less flexible than the albedo maps. As options, the following choices are presently available:

- 1) Uniform plane.
- 2) Adjoining half planes of different reflectance type bounded by a line parallel to the y-axis whose position is specifiable by its x-coordinate.
- 3) Non-overlapping rectangles set upon a uniform background (up to 20 such rectangles are allowed).

In all of the above, the background is specifiable as either Lambertian or rough Fresnel with inhomogeneities having either rough Fresnel or Lambertian character, respectively. The rectangles are specified by the (X,Y) coordinates of their centers and their X-Y edge lengths.

Text describing the chosen pattern is written out by INPUT. A cautionary note is in order here. Since the two types of maps are specified by unrelated means, care must be taken in the interpretation of results: The Albedo maps only apply to regions specified to have Lambertian character. Thus, using 50 variegated albedo maps and specifying the reflectance type map as a uniform rough Fresnel plane would produce identical results for all 50 albedo maps.

For rough Fresnel regions, the roughness is characterized as a distribution of randomly oriented sloping plane facets. The probability density for the distribution of slopes was chosen to have two-dimensional Gaussian form.  $p(Z_x, Z_y) \times \delta Z_x \delta Z_y$  is the fraction of a small horizontal unit area of surface for which the x,y components of the slope are within the limits  $Z_x \pm \frac{1}{2} \delta Z_x$  and  $Z_y \pm \frac{1}{2} \delta Z_y$ . We specify  $p(Z_x, Z_y)$  as:

$$p(Z_x, Z_y) = (\pi\sigma^2)^{-1} \exp [-(Z_x^2 + Z_y^2) / \sigma^2]$$

The variance,  $\sigma^2$  is specified either by three parameters W0, W1, W; or as a set value specified on input. When specified through parameters,  $\sigma^2$  is given as

$$\sigma^2 = W0 + W1 \times W$$

W represents wind speed (m/sec) in a model for the surface of the sea<sup>1)</sup> and W0, W1 have either their default values (W0 = .0015, W1 =  $2.54 \times 10^{-3}$ ) or values specified by card input. In the present code, all rough Fresnel regions share the same parametric values. This restriction could be relatively easily relaxed if desired.

The above form for  $p(Z_x, Z_y)$  represents that applicable for a photon incident from the vertical. For photons incident from some other direction, the distribution must be modified. Let the photon's direction be given by unit vector  $\hat{k}$ , the direction of the normal to a facet be  $\hat{n}$ , and the vertical direction be  $\hat{Z}$ . The probability of encounter will then be given by:

$$\frac{\hat{k} \cdot \hat{n}}{(\hat{n} \cdot \hat{Z})(\hat{k} \cdot \hat{Z})} p(\hat{n}) .$$

Having determined a slope at the photon impact point, the angle of incidence and, thence, the Fresnel matrix elements can be determined. If  $k$  and  $k'$  are the directions of propagation of the incident and reflected photons, their relation to  $n$  is

$$\frac{\hat{k}' - \hat{k}}{|\hat{k}' - \hat{k}|} = \hat{n} .$$

When sampling the contributions of unscattered photons from the Sun at a Fresnel scattering point, the direction of reflection is given by the solar direction and one merely evaluates the probability of having encountered a slope having the proper orientation. Note that in the present model the location of the Sun is given by a Dirac delta function (incoming plane waves) rather than being spread over a small angular region. The implied integration over the solar direction (or, equivalently, the change of variables within the delta function specifying the solar direction) introduces an additional factor of

$$.25 (\hat{n} \cdot \hat{Z})^{-3} (\hat{k} \cdot \hat{n})^{-1}$$



Our present formulation does not properly account for shadowing (waves whose surfaces are inaccessible due to their orientation) or for hiding (slopes inaccessible because of intervening higher waves). Thus, we expect some systematic bias, especially when either the sun or the receiver is low in the sky.

### SECTION 3.0

#### TESTING: CAPABILITIES AND LIMITATIONS OF CTRANS

CTTRANS has been tested and validated through comparison with the results of other calculations under a variety of conditions. Here, the results of representative cases will be presented and discussed.

The basic functional structure of the Monte Carlo code (backwards-tracking algorithm, Lambertian ground reflection, statistical normalizations, etc.) may be tested via calculations of radiative transfer through a pure Rayleigh atmosphere and comparison with the well established results of Coulson, Dave, and Sekera.<sup>2)</sup> Next, the atmosphere is made more complicated by adding layered structure and additional active atmospheric species. This provides a basic test of the algorithms for scatterer selection, the treatment of absorption, and the treatment of polydispersions. There may be special problems associated with optically thick atmospheres composed of strongly anisotropic scatterers so this case is of interest.

CTTRANS' capacity to handle horizontal inhomogeneities is basically evaluated by means of a calculation with a single cloud in the atmosphere and comparison with the results of McKee and Cox.<sup>3)</sup> In this test, some difficulties were detected which are associated with the calculation of flux (in optically thick clouds) by means of a backwards tracking code. These difficulties are partially resolved by using a specially adopted forwards-tracking code which will be briefly described.

CTRANS' capacities to treat horizontal ground reflection inhomogeneities are presented through test results. Absolute validation is difficult here in the absence of dependable analytical results, but having validated the microscopic reflection mechanism (through the inspection of results for uniform ground planes) only problems associated with the statistical density of sampling might be present. These statistical problems may be detected through the comparison of results from statistically independent runs.

### 3.1 HORIZONTALLY HOMOGENEOUS ATMOSPHERES

The first and most basic test case is that for a horizontally (and vertically) homogeneous Rayleigh atmosphere. Here CTRANS results may be compared with those of Coulson, Dave and Sekera <sup>2)</sup> who have tabulated values for the Stokes parameters and polarization for Rayleigh atmospheres with optical thicknesses ranging up to 1.0 and for uniform Lambertian ground planes with albedos from 0.0 to 0.8.

We have run tests over a range of optical thicknesses. Of these, the most stringent test is provided by the largest optical thickness ( $\tau = 1$ ). Since, in this case, single scattering, multiple scattering and ground reflection all are relatively important. Typical results for I, Q, U, and the polarization are shown in Figures 3.1.1 through 3.1.4. These results are for a receiver on the ground looking up with a zenith cosine angle of 0.4,  $60^\circ$  from the solar-vertical plane. As can be seen, agreement is excellent both for zero ground albedo and high ground albedo (0.8). Thus reflections at the ground are handled properly as is the basic transport through the atmosphere.

FIGURE 3.I.I.  
I VS. SOLAR ZENITH COSINE

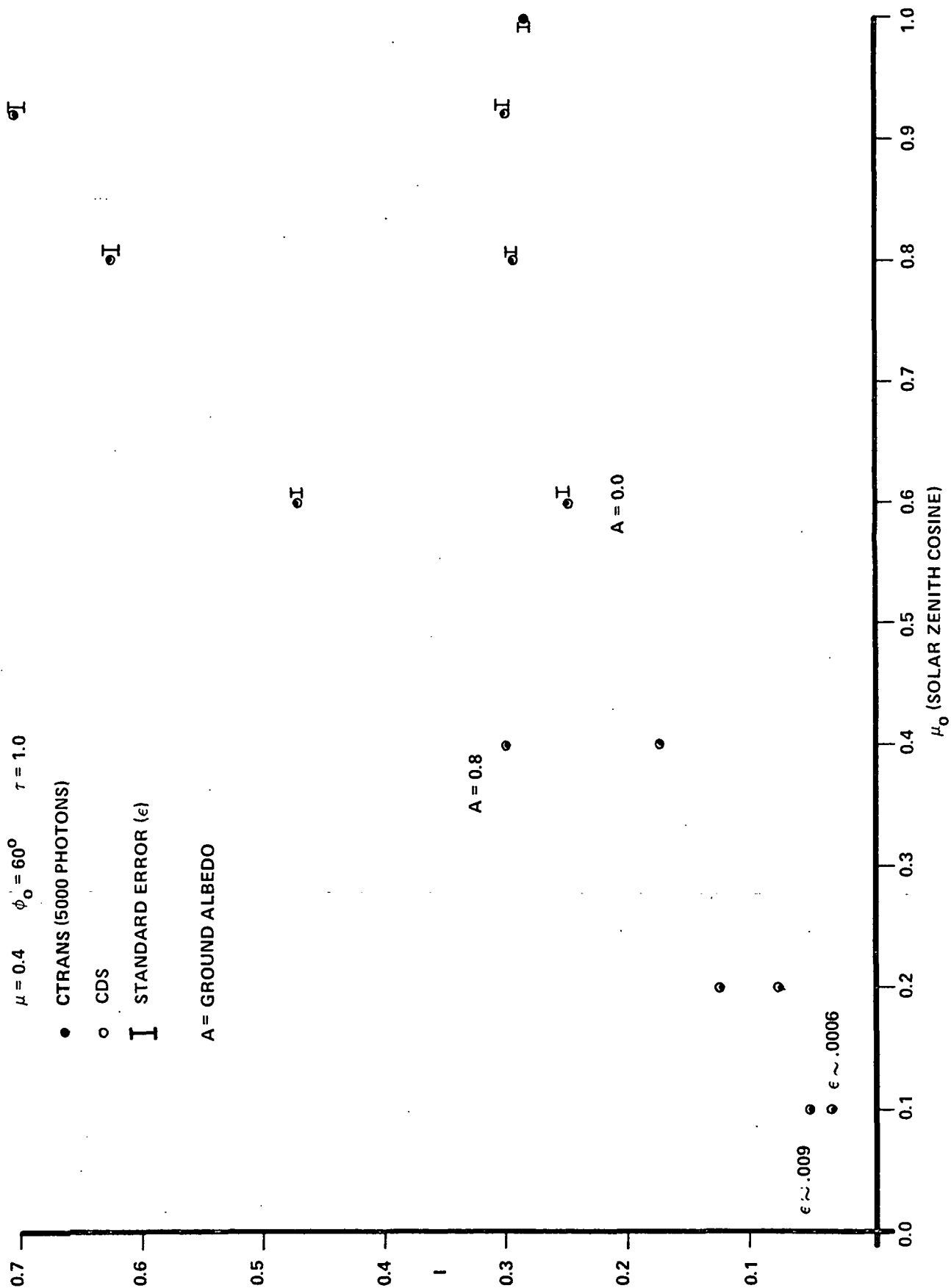


FIGURE 3.1.2.  
Q VS. SOLAR ZENITH COSINE

$\mu = 0.4$      $\phi = 60^\circ$

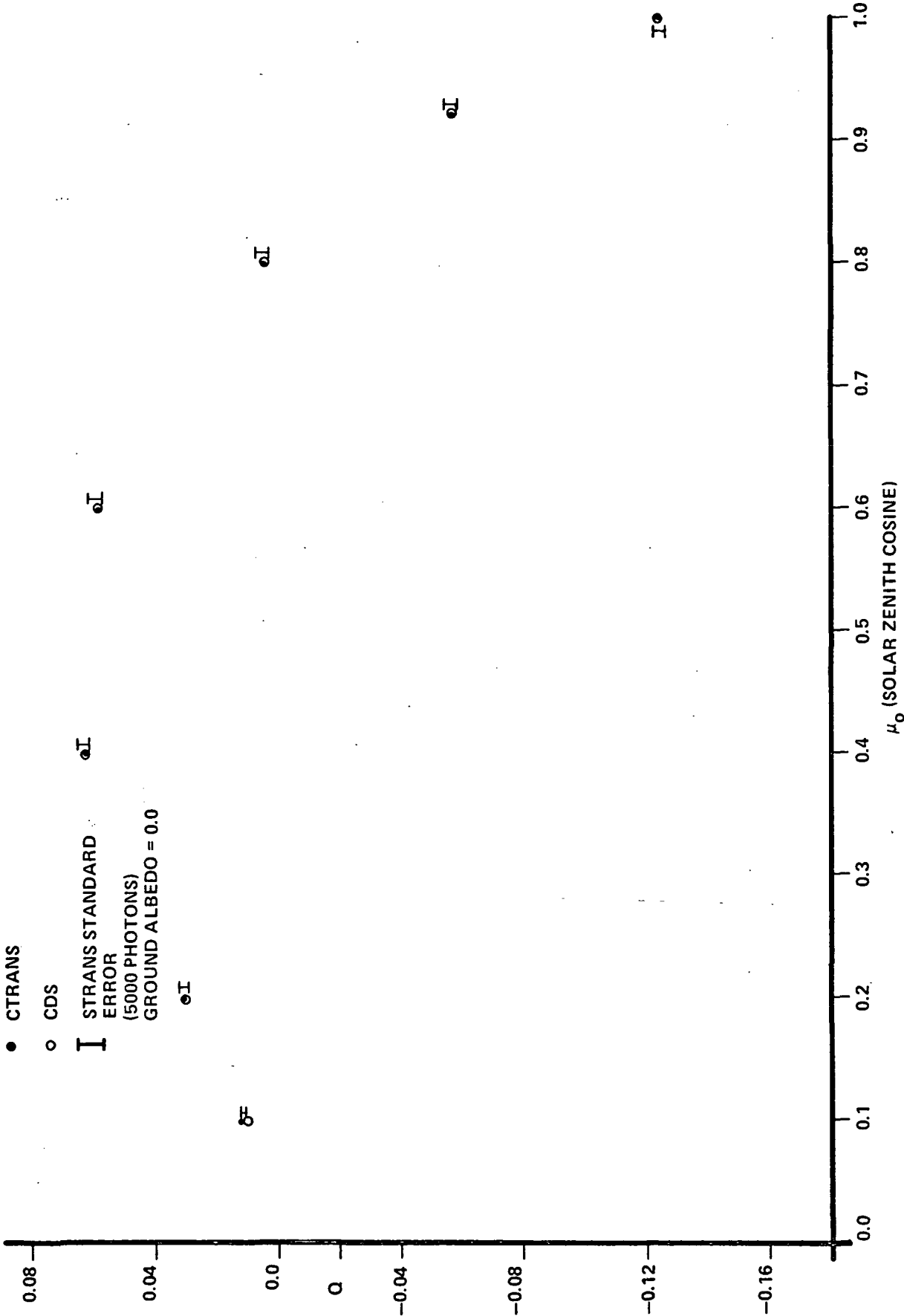


FIGURE 3.1.3  
 $\bar{U}$  VS. SOLAR ZENITH COSINE

• CTRANS  
 ○ CDS  
 I STRANS STANDARD ERROR  
 $\mu = 0.4 \quad \phi = 60^\circ$   
 $\tau = 1$  (5000 PHOTONS)  
 GROUND ALBEDO = 0.0

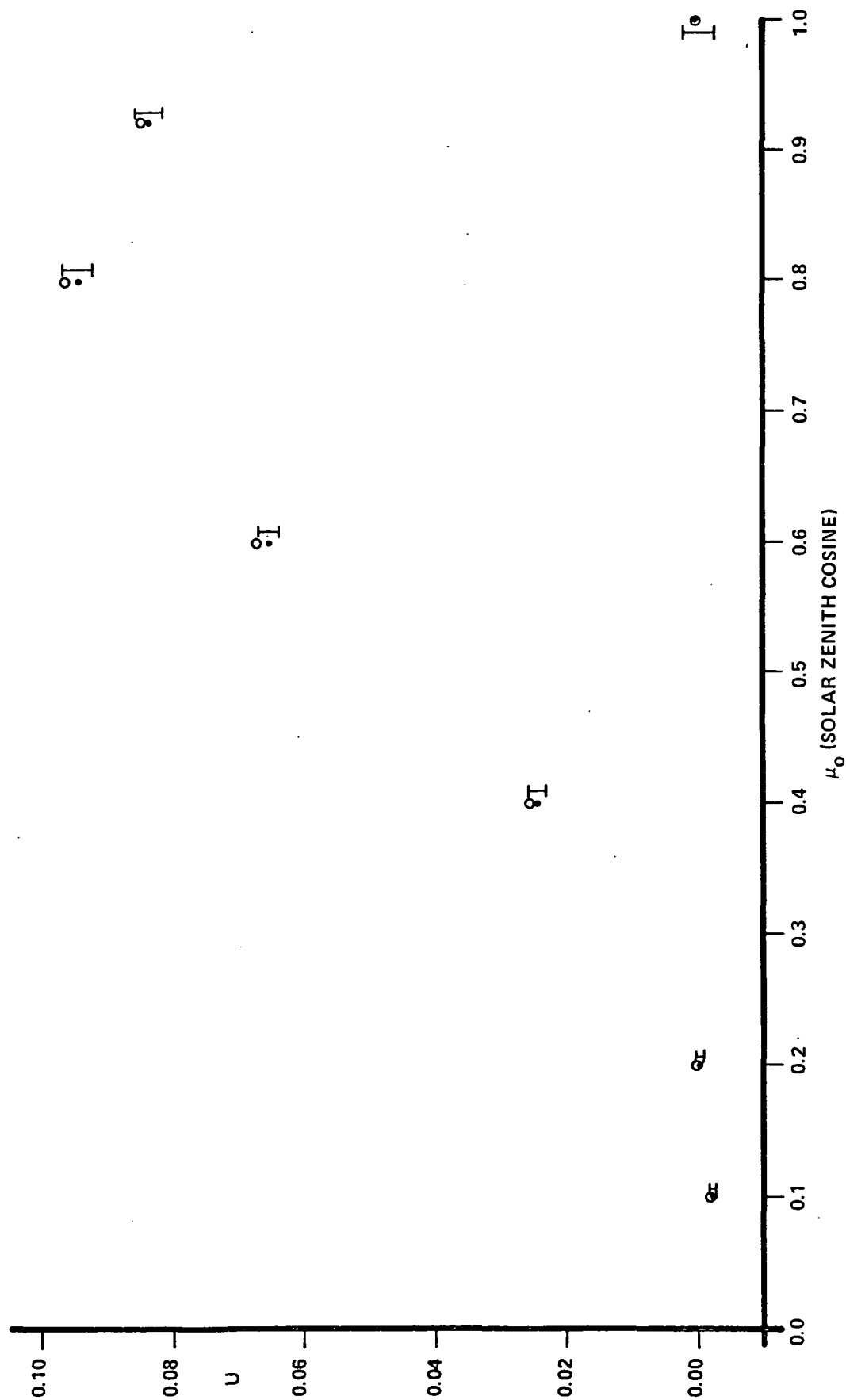
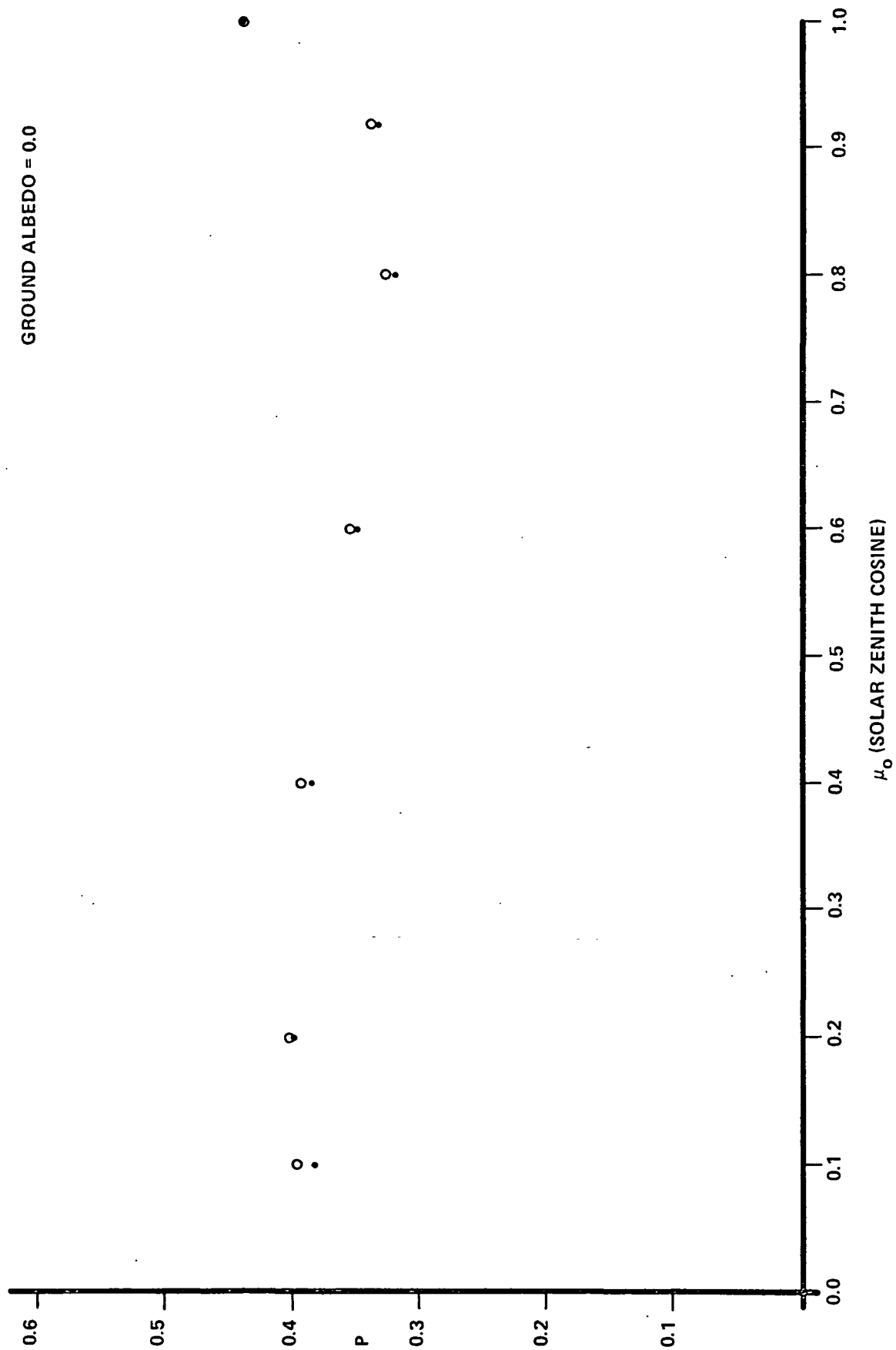


FIGURE 3.1.4.  
P VS. SOLAR ZENITH COSINE

$\mu = 0.4$      $\phi = 60^\circ$   
 $\tau = 1$  (5000 PHOTONS)  
 GROUND ALBEDO = 0.0

● CTRANS  
 ○ CDS



In the next test, we add vertical structure and a polydisperse aerosol in a fairly realistic model of a clear atmosphere. Since analytical results are unavailable for such an atmosphere, we compare CTRANS' computed values with two sets of results kindly provided by Dr. R.S. Fraser (computed by programs named RADTRAN and VPD). Results are presented in Tables 3.1.1 and 3.1.2 for the intensity and polarization at the bottom and the top of the atmosphere. As may be seen, CTRANS is in agreement with both routines to within the bounds expected from CTRANS' computed standard errors.

CTTRANS may encounter difficulty in handling optically thick atmospheres composed of scatterers having an extremely peaked phase function such as is provided by a Deirmendjian C1 polydispersion. The manifestation of the problem is a rather large variance especially evident when computing the radiance for a receiver looking down into the atmosphere. Tables 3.1.3 and 3.1.4 provide an illustration of the effect. Here we present a test case for a receiver pointing towards the nadir from the top of the atmosphere. The atmosphere is composed of pure Mie scatterers (C1 Deirmendjian haze:  $\alpha = 6.0$ ,  $\beta = 1.5$ ,  $\gamma = 1.0$ , index of refraction = 1.5). The wavelength is 0.825 microns. In the tables,  $I_c$  refers to CTRANS' results;  $I_k$  are results computed by a doubling method (provided by Mr. Lee Kyle); and  $SE_c$  denotes the standard error inherent in  $I_c$ . For this case, the ground albedo was zero and polarization was neglected. As may be seen, the agreement between  $I_c$  and  $I_k$  for the  $\tau = 0.1$  case is acceptable. However, when the optical thickness is increased to  $\tau = 10.0$ , the variance rises markedly (though no bias is detected). This variance is extremely difficult to reduce; particularly for the  $\tau = 10.0$  case. Here 2000 photons were tracked and up to 50 scatterings allowed per track, resulting in 39,422



Table 3.1.1.1. Realistic Clear Atmosphere Test: Intensity

RECEIVER		Height (Km)	CTRANS		RADTRAN $I_R$	$I_C - I_R$		VPD	
$\theta$	$\phi$		$I_C$	Std.Error (sec)		$\frac{I_C - I_R}{\text{sec}}$	$I_{VPD}$	$\frac{I_C - I_{VPD}}{\text{sec}}$	
60	0	0	.076158 ±	.00108	.07660	-.41	.07569	+.43	
60	180	0	.024003 ±	.000488	.02359	+.85	.02405	-.09	
36	0	0	.13846 ±	.002537	.13947	-.40	.1361	+.93	
36	180	0	.026063 ±	.000549	.02682	+.44	.02596	+.19	
60	0	70	.021629 ±	.000415	.02128	+.84	.02190	-.65	
60	180	70	.026991 ±	.000504	.02623	+1.52	.02735	-.70	
36	0	70	.014557 ±	.000362	.01396	+1.65	.01455	+.02	
36	100	70	.021593 ±	.000514	.02098	+1.19	.02180	-.40	

Wavelength  $\lambda = 0.55 \mu\text{m}$   
 Solar Zenith Angle =  $22^\circ$   
 Number of Atmospheric Layers = 34  
 Total Rayleigh Optical Thickness  $\tau_R = 0.098$   
 Total Aerosol Optical Thickness  $\tau_A = 0.19643$   
 Aerosol Index of Refraction  $m = 1.5$   
 Aerosol Size Distribution  $n(r) = 0$   
 Number of Photons per Receiver =  $10^4$   
 Maximum Scatterings per Photon Track = 20  
 Total Execution Time (CPU Time) = 2.66 min.

$r < .03$   
 $= C$   
 $= C r^{-4}$   
 $.03 < r < .2$   
 $.2 < r$

Table 3.1.2. Realistic Clear Atmosphere Test: Polarization

RECEIVER		CTRANS		RADTRAN	VPD	
$\theta$	$\phi$ Height (Km)	$P_C$	Std.Error (sec.)	$I_R$	$\frac{P_C - P_R}{\text{sec}}$	$\frac{P_C - P_{VPD}}{\text{sec}}$
60	0	0	0			
60	180	0	0			
36	0	0	0			
36	180	0	0			
60	0	70				
60	180	70				
36	0	70				
36	180	70				

Wavelength  $\lambda=0.55 \mu\text{m}$   
 Solar Zenith Angle=22°  
 Number of Atmospheric Layers=34  
 Total Rayleigh Optical Thickness  $\tau_R=0.098$   
 Total Aerosol Optical Thickness  $\tau_A=0.19643$   
 Aerosol Index of Refraction  $m=1.50$   
 Aerosol Size Distribution  $n(r)=0$   
 $=C$   
 $=C r^{-4}$   
 $r < .03 \mu\text{m}$   
 $0.03 < r < 0.2$   
 $.2 < r$

Number of Photons per Receiver=10<sup>4</sup>  
 Maximum Scatterings per Photon=20  
 Total Execution Time (CPU)=2.66 min.

Table 3.1.3. Uniform Aerosol Test  $\tau=0.10$

SOLAR ZENITH	CTTRANS	KYLE	PERCENT ERROR			
Angle $\theta_0$	Intensity $I_C$	Std.Error $SE_C$	Intensity $I_K$	$\frac{I_C - I_K}{SE_C} \times 100\%$	$\frac{I_C - I_K}{I_K} \times 100\%$	
0	.00660 +	.00014	.00699	-2.77	2.1	-5.6
4	.01398 +	.00024	.01415	-.59	2.1	-1.2
12	.00467 +	.00017	.00472	-.32	3.1	-1.1
15	.00620 +	.00084	.00534	+1.02	13.6	+16.0
30	.000818 +	.000034	.000812	+.17		+0.7
45	.000368 +	.000020	.0003726	+.21		+1.1
60	.000360 +	.000017	.0004017	-2.47		-10.5

36

Atmosphere: Uniform Aerosol 5 Km Thick

Aerosol Size Distribution: Deirmendjian C1

$\alpha=6.0$ ,  $\beta=1.5$ ,  $\gamma=1.0$

Aerosol Index of Refraction  $m=1.5$

Total Vertical Optical Thickness  $\tau=0.10$

Wavelength  $\lambda=0.825 \mu m$

Receiver Nadir Angle= $0^\circ$

Receiver Altitude = 5 Km

(Top of  
Atmosphere)

Number of Photon Track = 22000

CPU Time = 1.51 min.

Table 3.1.4. Uniform Aerosol Test  $\tau=10.0$ 

SOLAR ZENITH		CTRANS		KYLE		PERCENT ERROR	
Angle	Intensity $I_C$	Std.Error $SE_C$	Intensity $I_K$	$\frac{I_C - I_K}{sec}$	$\frac{SE_C}{I_C} \times 100\%$	$\frac{I_C - I_K}{I_K} \times 100\%$	
$\theta_0$							
0	.28179	+ .07461	.2434	.51	26.5	15.8	
4	.26818	+ .03061	.2858	-.58	11.4	-6.2	
12	.18665	+ .02554	.2067	-.79	13.7	-9.7	
15	.17177	+ .01998	.2076	-1.79	11.6	-17.3	
30	.15409	+ .03187	.1459	+.26	20.7	5.6	
45	.12780	+ .05169	.1132	+.28	40.4	12.9	
60	.07365	+ .01862	.07631	-.14	25.3	-3.5	

Atmosphere: Uniform Aerosol 5 Km Thick

Aerosol Size Distribution:Deirmendjian C1

 $(\alpha=6.0, \beta=1.5, \gamma=1.0)$ Aerosol Index of Refraction  $m=1.5$ Total Vertical Optical Thickness  $\tau=10.0$ Wavelength  $\lambda=0.825 \text{ }\mu\text{m}$ 

Receiver Nadir Angle = 0°

Receiver Altitude = 5 Km

(Top of Atmosphere)

Number of Photon Tracks = 2000

Maximum Scatterings per  
Photon = 50

CPU Time = 5.10 min.

scattering events (19.71 scatterings per photon track on the average). Tracking 2000 photons in this thick atmosphere required 5.10 minutes of CPU time. The variance might be reduced by increasing the number of photon tracks, but in general this would be very expensive. There are two effects operating in the  $\tau = 10$ . Case: 1) Since the atmosphere is thick, photons must scatter many times before wandering out of the atmosphere. 2) The fact that the scattering phase function is extremely peaked in the forward direction means that most photons will not contribute importantly to the sample; i.e., only a few photons which, by chance, are traveling nearly toward the sampling direction provide large contributions to the sample while all others contribute small amounts. The backwards tracking code is thus statistically inefficient in this case. This inefficiency may be unimportant in optically thin atmospheres (or in absorbing atmospheres) since it may be economically overcome by increasing the number of photon tracks.

In an attempt to improve the efficiency of the code, a number of alternate importance sampling schemes were implemented. In all of these, it was found that any substantial reduction in variance was accompanied by the introduction of bias. These alternate schemes have, thus, been abandoned.

### 3.2 HORIZONTAL ATMOSPHERIC INHOMOGENEITIES (CLOUDS)

In order to validate CTRANS' capacity to handle finite clouds, we may compare with the results of McKee and Cox.<sup>3)</sup> Their computation utilized a Monte Carlo method to calculate the flux emerging from the faces of a finite cloud of cubic shape. Their model ignored scattering outside the cloud and neglected polarization effects. Accordingly, we used no ambient atmosphere and restricted the ground to zero albedo.

McKee and Cox obtained results for clouds composed of an aerosol having a Deirmendjian haze  $Cl^{5)}$  size distribution and optical thickness per kilometer equal to 4.9 and 73.5. The wavelength is  $0.45 \mu m$ .

The scattering phase function for this case contains a very narrow, strong forward peak. Our previous considerations would lead us to expect that these clouds would provide a very severe test of CTRANS. Optically thick clouds entail many scatterings per photon track and a sharply peaked phase function requires many independent photon tracks to achieve satisfactory variance. On this account, we have restricted the test to a cloud with an optical thickness of 4.9 per kilometer.

The basic geometry of the test is illustrated in Figure 3.2.1. Light is incident upon the cloud from zenith angles of  $0^\circ$ ,  $30^\circ$ , and  $60^\circ$ . The incident flux is normalized to  $1 \text{ watt/km}^2$  normal to the beam.

In order to compare with McKee and Cox, CTRANS (using backward tracking) initiates photons from a chosen face of the cloud, distributing them uniformly over the face and distributing their initial flight directions over  $2\pi$  steradians. In so doing, CTRANS might be expected to incur additional variance since some regions of the cloud will be brighter than others and some exit directions will be more important. This, then, will represent an additional source of difficulty for the backwards tracking method. For this test, separate computations are performed for each face. This means that flux will not be automatically conserved and the degree to which flux is conserved will be a test of the program.

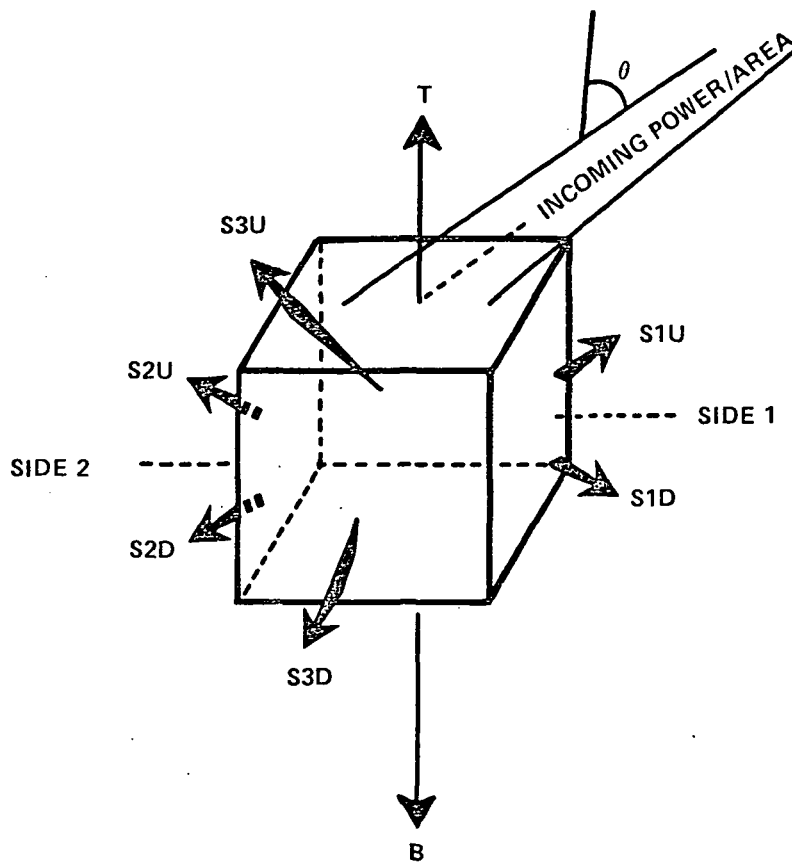


FIGURE 3.2.1. GEOMETRY OF THE COX-McKEE TEST CLOUD

When photons are initiated on a face, they are segregated according to whether the (forward) photon would be emerging upwards or downwards. CTRANS' results for the fraction of incident flux emerging from each face upwards or downwards are compared with those of McKee and Cox in Table 3.2.1 for each face for upward-emerging and downward-emerging photons. Results for all three solar zenith angles are computed simultaneously so that there will be some correlation between results for different suns; suns at  $30^\circ$  and  $60^\circ$  correlate most strongly.

From the results of Table 3.2.1, the conservation of flux can be checked: for solar zenith angles,  $0^\circ$ ,  $30^\circ$ , and  $60^\circ$ , the total emerging flux is  $.946 \pm .12$ ,  $.98 \pm .14$ , and  $1.29 \pm .25$ . In each case, the difference from 1.0 is not statistically significant.

Overall, the results for individual faces tend not to be as accurate as might be desired. For a number of faces, the difference between CTRANS' results and those of McKee and Cox is large compared with the computed standard error and in most of these instances, CTRANS' results are low. This may be caused indirectly by photons escaping from the cloud before they have added their full proper contributions to the flux. Two possibilities exist for correcting this: keep the photons in the cloud and accumulate the probability that they would have escaped; or run many more photons. The first method precludes interaction with the atmosphere surrounding the cloud and with other clouds and is therefore generally undesirable for CTRANS. The second method will only be feasible for optically thin clouds. One other possibility exists which has not yet been fully explored: distribute the photons non-uniformly over the cloud face initially.



TABLE 3.2.1. FLUX EMERGING FROM THE FACES OF A CUBIC CLOUD

CLOUD VERTICAL OPTICAL THICKNESS = 4.9      WAVELENGTH  $\lambda = 0.45 \mu\text{m}$       NUMBER OF PHOTONS TRACKED = 4000/FACE  
 CLOUD COMPOSITION: C1 DEIRMENDJIAN      NO AMBIENT ATMOSPHERE  
 $[n(r) \sim r^6 \exp(-1.5r)]$       GROUND ALBEDO = 0.0

$\theta_o$       T      S1U      S2U      S3U      TOTAL UP      B      S1D      S2D      S3D      TOTAL DOWN

INCIDENT	1.00									
DIRECT (CTRANS)						.0074566				
(EXACT)						.0074650				
0° SCATTERED (CTRANS)	.0561 + .003	.0163 + .003	.0165 + .003	.0167 + .003	.120 + .006	.2747 + .028	.1972 + .112	.0873 + .012	.1282 + .028	.816 + .13
(COX-McKEE)	.08	.02	.02	.02	.17	.41	.10	.10	.10	.82
INCIDENT	.63	.37								
DIRECT (CTRANS)						.06618 + .002				
(EXACT)						.06543				
30° SCATTERED (CTRANS)	.041 + .002	.0187 + .002	.0162 + .002	.0122 + .002	.101 + .005	.430 + .135	.0252 + .002	.1801 + .030	.0560 + .004	.748 + .14
(COX-McKEE)	.05	.02	.02	.02	.13	.33	.03	.25	.07	.74
INCIDENT	.37	.63								
DIRECT (CTRANS)						.06494 + .0013				
(EXACT)						.064497				
60° SCATTERED (CTRANS)	.0428 + .002	.0227 + .002	.201 + .109	.0211 + .003	.309 + .11	.4351 + .212	.0234 + .008	.2939 + .094	.0459 + .003	.844 + .23
(COX-McKEE)	.05	.03	.05	.02	.19	.26	.02	.27	.06	.68

This is tricky, however, as great care must be employed to avoid introducing bias in the final result. Further, a suitable non-uniform distribution would be expected to depend upon the solar zenith angle, thus limiting runs to a single sun. The logical extension of this concept would be to attempt to distribute photons both in position and direction according to their importance in the final results. Initial effort along this line were not notably successful and have not been pursued.

### 3.3 FLUX COMPUTATIONS FOR A FINITE CLOUD COMPUTED BY A FORWARD TRACKING PROGRAM

Our experience in applying the backward tracking Monte Carlo program to the evaluation of fluxes emanating through the faces of finite clouds demonstrated that there is considerable difficulty in establishing relevant importance functions which provide unbiased solutions with low variance. A more natural procedure for evaluating the fluxes through the faces of a single cloud is to use the forward tracking procedure of Cox and McKee.

In order to provide a means of testing flux results generated by the backwards code we modified an existing forward tracking code for a plane parallel atmosphere using subroutines developed for the backtracking code. The code was tested by regenerating some of the results of Cox and McKee.

The flux evaluation code, FLX, provides a capability in simulation capacity that exceeds that of the Cox and McKee code. The salient features of the simulation are as follows:

1. Only one box-shaped cloud can be treated. Its interactions with the surrounding atmosphere, other clouds and the ground are neglected. The cloud must have its upper and lower surfaces parallel to the ground. Its shape need not be cubic.
2. The cloud can have arbitrary azimuthal orientation, i.e., it is not necessary for there to be a pair of faces parallel to the solar zenith plane.
3. Vertical inhomogeneities within the cloud are allowed. Up to 100 vertical layers may be defined with up to 5 scattering species.
4. Polarization is treated using the Mueller scattering algebra.

In brief, the photon tracking and sampling algorithm is as follows:

A photon enters a face of the cloud in a random location. The face of entry is selected on the basis of the area of the face projected perpendicular to the solar direction. At each scattering we compute the face towards which the photon is travelling using the subroutine CLOUT described elsewhere in this report and evaluate the optical thickness  $\tau_i$  to the face. We then sample the quantity

$$S_i = w_i I_i e^{-\tau_i}$$

where  $w_i$  = weight of the photon at the  $i$ th scattering

and  $I_i$  = intensity component of Stokes vector at  $i$ th scattering as the contribution to the appropriate flux.

The photon weight is then reduced by a fraction  $(1 - e^{-\tau_i})$ , i.e.,

$$w_{i+1} = w_i (1 - e^{-\tau_i})$$

and the photon is forced to make its next scattering prior to exit from the cloud. If  $\tau_{i_s}$  is the actual optical distance to the next scattering then  $\tau_{i_s}$  is distributed as  $e^{-\tau}$  but with the constraint that  $\tau_{i_s} < \tau_i$ .

The sampled fluxes from the sides of the cloud are discriminated in terms of up-welling and down-welling photons. Obviously, only upwelling photons contribute to the flux from the upper face of the cloud and only downwelling photons contribute to the flux from the lower cloud face. By treating the point of entry to the cloud as a scattering point we are able to properly evaluate the flux contribution of attenuated but unscattered solar radiation contributing to the flux.

Each photon is tracked until its weight is reduced to an arbitrary threshold. Typically we have set the threshold at  $10^{-5}$ . A typical simulation would involve 1000 to 10000 incident photons and standard errors in the fluxes range from 1 to 5 percent.

θ	τ	TINF	T	S1U	S2U	S3U	TOTAL	BINF	B	S1D	S2D	S3D	TOTAL
							UP						DOWN
INCIDENT													
			1.0	0									
0	4.9	.222	.066	.026	.026	.026	.171	.771	.395	.108	.108	.108	.829
		+ .012	+ .007	+ .004	+ .004	+ .004	+ .010	+ .012	+ .009	+ .009	+ .009	+ .009	+ .010
	73.5	.877	.512	.051	.051	.051	.716	.118	.016	.068	.068	.068	.287
		+ .019	+ .022	+ .009	+ .009	+ .009	+ .020	+ .016	+ .006	+ .010	+ .010	+ .010	+ .018
SCATTERED													

INCIDENT													

INCIDENT													
			.36	.63									
SCATTERED	4.9	.470	.056	.033	.058	.032	.212	.530	.238	.026	.264	.065	.788
		+ .015	+ .006	+ .005	+ .006	+ .004	+ .011	+ .015	+ .013	+ .004	+ .013	+ .007	+ .011
	73.5	.915	.286	.164	.021	.047	.565	.089	.106	.191	.035	.058	.447
		+ .016	+ .020	+ .015	+ .007	+ .008	+ .021	+ .016	+ .014	+ .016	+ .008	+ .010	+ .021
60													
46													

Table 3.3.1 presents a comparison of the flux fractions emanating from the various faces of the cloud. Contributions from unscattered light have been added into the diffuse contribution in computing the total downwelling flux. TINF and BINF refer to corresponding results for a cloud layer of infinite horizontal extent. Apart from these differences, Table 3.3.1 is similar in format to Table 3.2.1 and permits comparisons among the results from CTRANS, FLX, and McKee and Cox.

### 3.4 GROUND PLANE REFLECTIONS

The basic mechanism for handling Lambertian reflection has been tested implicitly in the Rayleigh atmosphere tests reported in Section 3.1. The capacity of CTRANS to handle inhomogeneous Lambertian ground patterns may be illustrated by a test example but specifically comparable independent calculations do not appear to be available.

As a suitable test example, the basic ground patterns were chosen as half planes of differing albedo with boundaries parallel to the y-axis and x-axis intersections at a number of points along the axis. The receiver was above the top of the atmosphere (704 km) centered at  $(X_k^R, Y_k^R) = (0,0)$  and looking towards the nadir. The receiver field of view was 85.2  $\mu$ rad yielding a 60 m diameter footprint on the ground. The atmosphere was composed of Rayleigh and haze C aerosol scatterers with total optical thicknesses of .098 and .19643, respectively. The wavelength employed was  $\lambda = 0.55 \mu\text{m}$ . The albedo pairs employed were (.6, 0), (.5, .1), (.4, .2), (.3, .3) with boundaries intersecting the x-axis at  $X = \pm 2.0, \pm 1.0, \pm 0.5, \pm 0.25, \pm 0.05, 0.0$  km. In addition to the half-planes, results for uniform Lambertian ground planes

with albedos .6, .5, .4, .3, .2, .1, and 0.0 were obtained. All results were, of course, obtained simultaneously. These results are shown in Figure 3.4.1. Since all computed values depend upon the same set of photon tracks, relative values are computed more accurately than absolute values. This feature is of great importance when CTRANS is used, for example, to determine the distinguishability of surface features as seen from a satellite.

The ground plane reflection characteristics may be modified in yet another way: the reflectance type may be changed from Lambertian to rough Fresnel, useful for sea surface modeling. Several independent calculations exist against which CTRANS' results may be validated. We chose the following parameters to specify a suitable test case: solar zenith angle,  $\theta_0 = 57^\circ$ ; wind speed = 5 m/sec (yields a wave slope variance  $\sigma^2 = 0.0286$ ); wavelength,  $\lambda = 0.70 \mu\text{m}$ ; Rayleigh optical thickness  $\tau_R = 0.037$ ; aerosol optical thickness  $\tau_M = 0.214$ ; the field of view of the receiver was taken to be zero. These parameter values were chosen so as to be able to compare our results with those computed independently by RADTRAN. These model parameters are also similar to (but not identical with) those used by Kattawar and Plass.<sup>4)</sup> Figure 3.4.2 presents the results of CTRANS as well as those of RADTRAN and Kattawar and Plass. As may be seen, all three calculations are in agreement to within 1.4 times the computed standard error.

INTENSITY  
(ster<sup>-1</sup>)

ALBEDO BOUNDARY EFFECTS

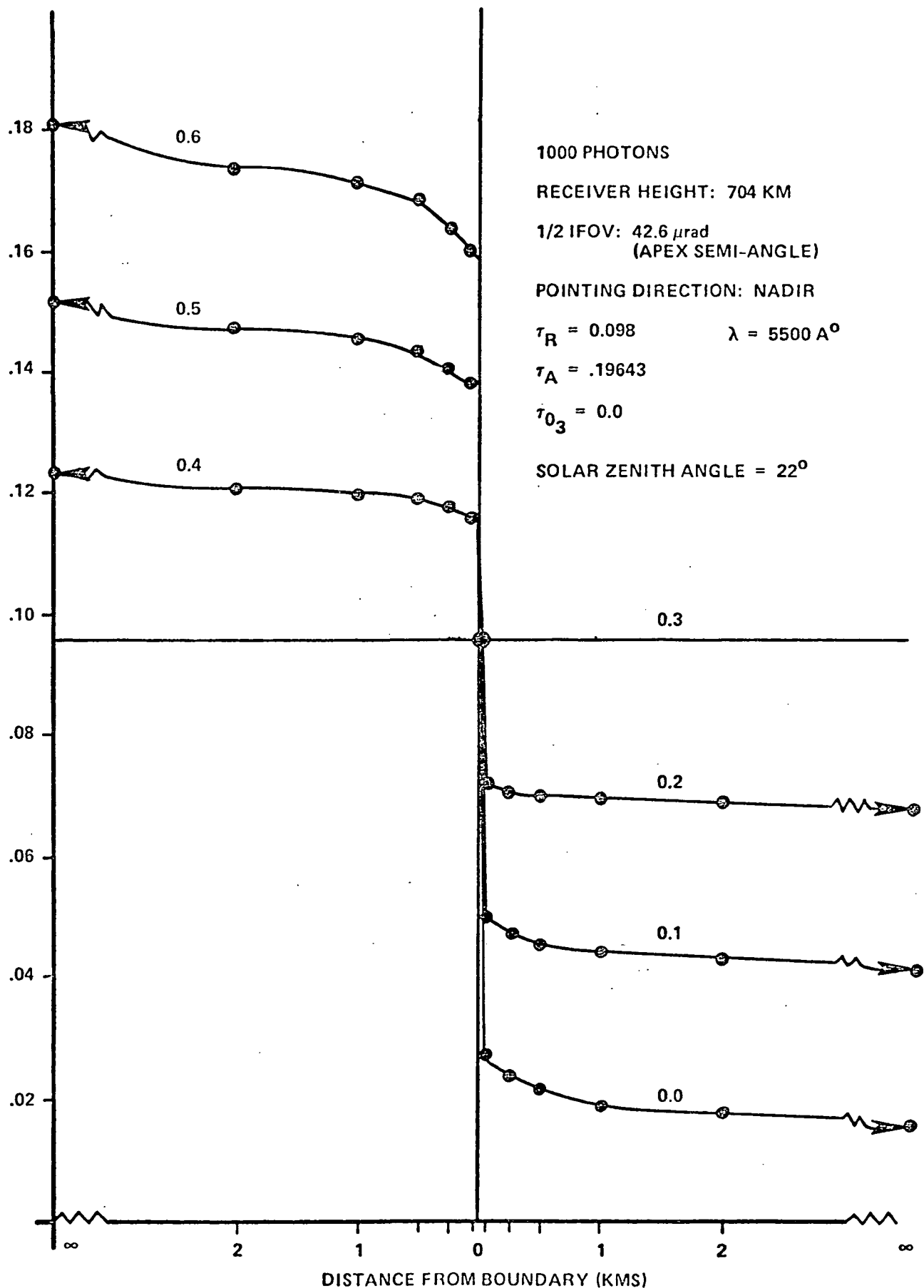


FIGURE 3.4.1.



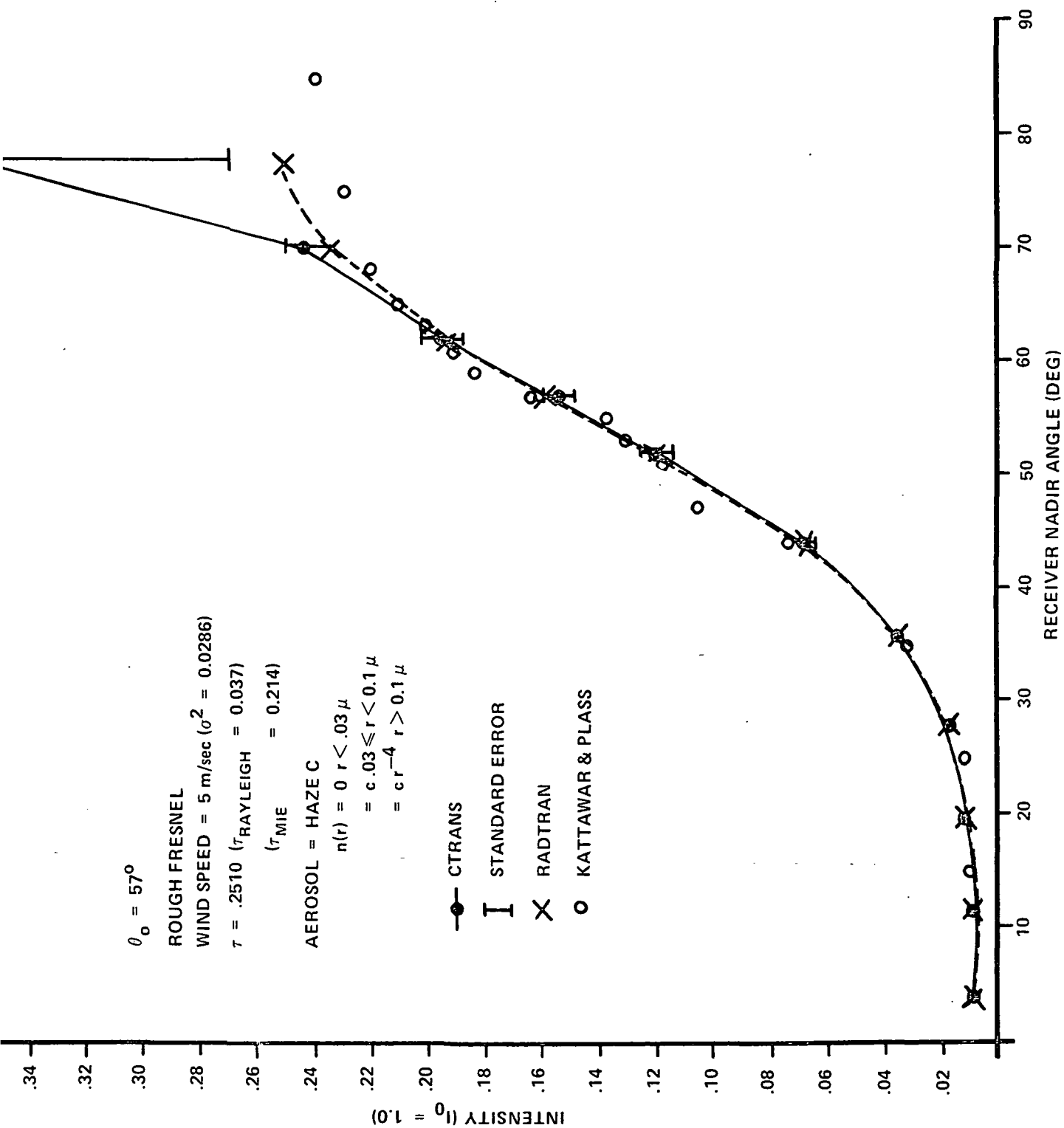


FIGURE 3.4.2.

SECTION 4.0  
SUBROUTINES: DESCRIPTIVE OUTLINES

In its present version, CTRANS is composed of a MAIN control routine and 34 supporting subroutines. In the following, we outline the main functions of each of these.

MAIN

MAJOR FUNCTION: Main control routine

INPUTS: 1. Initial random number  
2. IND,IST,ISKY,INFLUX,WAV

OUTPUTS: 1. Contribution maps  
2. Timing information, number of photons tracked

ACTIONS: 1. Set up constants, initiate random number sequence, clear storage.  
2. Read major control card: IND,IST,...  
(STOP if IND=0)  
3. Call INPUT - Input model specification, write out descriptive text  
4. Loop over photon tracks  
4.1 Initialize photon at receiver  
4.2 Sample direct sun contribution (use SEESOL)  
4.3 Loop over allowed number of scatterings  
4.3.1 Determine distance to scattering, propagate photon along path (TRACK)  
4.3.2 Determine scattering species  
4.3.3 Sample hypothetical photon from each sun (SAMPLE)

- 4.3.4 Determine scattering angle and direction (ANGLEM and JIM; or GNDREF)
- 4.3.5 Update cumulative scattering matrix following a real scattering (RENEW)
- 4.4 Clump, collect statistical measures
- 4.5 Check time remaining (terminate if insufficient)
- 5. Write contribution maps (if finite receiver field of view)
- 6. Normalize samples
- 7. Output results (OUTPUT)
- 8. Output statistics (TAB)
- 9. Return to Step 2.

## INPUT

MAJOR FUNCTION: Read in model specification parameters, compute and fill reference tables, write text describing model and input quantities.

INPUTS: 1. Atmosphere description cards  
2. Sun specifications  
3. Size distribution parameters  
4. Phase matrix elements (cards or tape)  
5. Atmospheric layer heights, temperatures  
6. Atmospheric layer heights, component densities  
7. Cloud input specifications (CLINP)  
8. Receiver specifications  
9. Ground reflectance type map specifications

OUTPUTS: 1. Main title  
2. Simulation parameters  
3. Receiver description  
4. Solar array description  
5. Ground description  
    5.1 Reflectance type map  
    5.2 Lambertian albedo maps  
6. Atmosphere description  
    6.1 Characteristics of each type of scatterer in entire atmosphere  
    6.2 Phase functions  
    6.3 Ambient atmospheric densities, cross section  
    6.4 Average scattering angle  
    6.5 Cloud specifications

## SAMPLE

MAJOR FUNCTION: Accumulates a sample for hypothetical photons arriving from each Sun. Reads no cards. Writes no text.

- ACTIONS:
1. Set up photon co-ordinates (if in a cloud) (TRANS 1)
  2. Loop over Suns
    - 2.1 Compute scattering angle and/or direction for scattering into Sun
    - 2.2 Determine scattering plane, normal to scattering plane, rotation angle (FIXALL)
    - 2.3 Multiply rotation into cumulative scattering matrix (ROTATE)
    - 2.4 Obtain matrix elements for scattering other than Rayleigh (ELEMTS or GENGND)
    - 2.5 Multiply scattering matrix into cumulative scattering matrix (SCATMI, SCATRA or GENSCA)
    - 2.6 Compute optical path length to Sun (SEESOL) and, thence, the attenuation factor
    - 2.7 Fold in other applicable weights
    - 2.8 Accumulate sample into sampling matrix, VSAMP

## SEESOL

MAJOR FUNCTION: Determines optical path length to the Sun. Assumes that CLCORD and COORD contain position and path direction cosines for photons in a cloud or not in a cloud, respectively.

- ACTIONS:
1. Determine distance out of cloud (if in a cloud) (CLOUT)
  2. Compute contribution of overlying ambient atmospheric layers
  3. Compute contribution of present ambient atmospheric layer
  4. Compute contribution of other clouds entered along path
    - 4.1 Check cloud spheres entered along path (CLENTR)
    - 4.2 For each sphere entered, check entries in detail; get distance to entry and distance to exit for each cloud entered (SDIST,CLOUT)
  5. Compute total optical distance to Sun (along the direction indicated by COORD and/or CLCORD)

## TRACK

- MAJOR FUNCTIONS:
1. Determines optical path length to be traversed
  2. Propagate photon along its current direction until chosen optical path length is traversed
  3. Update co-ordinate systems at boundary (cloud) crossings
  4. Set IOUT=1 for photons exiting top of atmosphere
  5. Set ISCAT=1 for photons hitting earth, compute coordinates of impact

- ACTIONS:
1. Choose optical path length to be traversed  
 $\tau = -\ln(P)$  ( $P$ =uniformly distributed random number)
  2. Set up boundaries
    - 2.1 Boundary of present cloud (if in a cloud)
    - 2.2 If not in a cloud, boundary of any cloud along extended path - use CLENT, TDIST- or, atmospheric boundaries if no clouds can be entered
    - 2.3 Determine type of boundary
  3. Successively accumulate increments in distance traversed and traversed optical path length until either the chosen optical path is exhausted or until a boundary is encountered.
  4. Boundary encounter
    - 4.1 If boundary is top of atmosphere, set IOUT=1, exit
    - 4.2 If boundary is ground, set ISCAT=1, compute coordinates of impact, CG.
    - 4.3 If boundary is a cloud boundary, update coordinates and resume tracking
  5. Update photon position

TRANS  
TRANS1  
TRANS2

FUNCTIONS: These closely related and similar routines transform coordinate positions and/or photon flight direction cosines into and out of the cloud coordinate systems.

If  $XC_i$  = photon position coordinate in the cloud  $i=1,3$

$X_i$  = photon position in fixed coordinate system  $i=1,3$

$XC_i$  = photon flight direction cosines in the cloud  $i=4,6$

$X_i$  = photon flight direction cosines in the fixed coordinate system  $i=4,6$

and  $XCL_i$  = C.M coordinates of the cloud in the fixed system  $i=1,3$

$\theta$  = orientation angle of the cloud

$\underline{XC} = \underline{R}(\underline{X} - \underline{XCL}) \quad i=1,3$

$\underline{XC} = \underline{R}(\underline{X}) \quad i=4,6$

$\underline{X} = \underline{XCL} + \tilde{\underline{R}} \underline{XC} \quad i=1,3$

$\underline{X} = \tilde{\underline{R}} \underline{XC} \quad i=4,6$

$\underline{R} = \begin{pmatrix} \cos\theta & \sin\theta & 0 \\ -\sin\theta & \cos\theta & 0 \\ 0 & 0 & 1 \end{pmatrix}$

$\tilde{\underline{R}}$  = transpose of  $\underline{R}$



## CLOUT(I,NOUT,CDIST,EXT)

FUNCTION: Determines the point of exit from a cloud and the distance along the photon path to this point

PARAMETERS: I = Cloud index  
NOUT = 1 if exit point is found  
CDIST(I) = distance to exit point  
EXT(I,J), J=1,2,3 = exit point coordinates for cloud I

METHOD: Let  $C_i, C_j, C_k$  = exit coordinates in cloud system  
 $X_i, X_j, X_k$  = present photon coordinates in cloud system  
 $V_i, V_j, V_k$  = direction cosines of photon flight path in cloud system  
 $A_i, A_j, A_k$  = cloud half edge lengths  
all where i,J,K may be a permutation of X,Y,Z.

1.  $C_i = |V_i| * A_i$   
 $C_j = X_j + (C_i - X_i) V_j / V_i$   
 $C_k = X_k + (C_i - X_i) V_k / V_i$   
if  $C_j$  and  $C_k$  are within the cloud boundaries then the exit point is  $(C_i, C_j, C_k)$  i if not, cycle through values of (i,j,k)
2. Compute distance to exit point

## CLINP

FUNCTIONS: Reads in cloud input parameters, transforms these and computes auxilliary descriptive parameters.

ACTIONS:

1. Read number of clouds N CLOUD
2. Return if N CLOUD=0
3. For each cloud read  
HC, AC, BL, CC, XCL, YCL, THETAC, INC, CLDEN  
where  
HC=Altitude of base of Cloud (in km.)  
AC, BC, CC=Linear dimension of cloud (km.)  
XCL, YCL =X, Y coordinates of center of  
mass of the cloud in the fixed  
coordinate system  
THETAC =Orientation angle of the cloud  
measured clockwise looking up  
(in degrees)  
INC =Indicator of scatterer type  
composing cloud  
CLDEN =Density of scatterers of type  
INC ( $\text{cm}^{-3}$ ).
4. Computes sines and cosines of THETAC,  
cloud edge half-lengths, radii of cloud  
circumscribing spheres and puts all  
information into the descriptive vector  
CLOUD(10,10):  
CLOUD(I,J) : I=Cloud pointer  
J=1,2,3 : C.M. coordinates of the cloud  
J=4,5,6 : Half dimensions of each side  
of the cloud  
J=7,8 : cos (THETAC) , sin (THETAC)  
J=9 : Radius, R, of the circumscribing  
sphere  
J=10 :  $R^2$

## CLINTR

FUNCTIONS: Checks whether the photon can penetrate any of the cloud circumscribing spheres and orders the sequence of entry.

ACTIONS: 1. Computes square of distance to a cloud, length between point of closest approach and present photon position, and square of distance of closest approach along the extended path.

2. Orders entries by entry sequence

## SDIST

FUNCTIONS: Tests which plane of the cloud photon entered, calculates distance to intersection, and orders them by entry sequence

ACTIONS: 1. For each uneliminated cloud computes point of entry and distance to that point (PLANE)  
2. Orders by entry sequence (length from present position to entry point).

## TDIST

FUNCTION: Calculates distance to the cloud photon can enter in TRACK

ACTION: Uses PLANE to compute distance to the first cloud entry

PLANE(I, INDC, ENT, NPLANE, DIST)

FUNCTION:      Calculates the coordinates of the point of entry of a photon into a cloud and determines the distance to this point from the photon's present position

PARAMETERS:    I            = Cloud index  
                  INDC        = Parameter controlling the transformation into/out of cloud coordinate system  
                  ENT(I,J) J=1,2,3 = Coordinates of point of entry into cloud I  
                  NPLANE    = 1 if entry can occur  
                                 = 0 otherwise  
                  DIST(I) = Distance to point of entry into cloud I

METHOD:      Let  $C_i, C_j, C_k$  = Entry coordinates in cloud system  
                   $X_i, X_j, X_k$  = Present photon position coordinates in cloud system  
                   $V_i, V_j, V_k$  = Direction cosines of photon flight path in cloud system  
                   $A_i, A_j, A_k$  = Cloud half-edge lengths  
                                 all where  $i, j, k$  are a permutation of  $X, Y, Z$ .

1. If  $|X_i| \leq A_i$       try another permutation
2. If  $X_i < A_i$        $C_i = -A_i$   
                   $X_i > A_i$        $C_i = A_i$
3. If  $(X_i - C_i)A_i > 0$       }  
                  or  $V_i = 0$ .      }      Try another permutation
4.  $C_j = X_j + (V_j/V_i) (C_i - X_i)$   
           $C_k = X_k + (V_k/V_i) (C_i - X_i)$

5. If  $C_j$  and  $C_k$  lie within the cloud boundaries, exit point is  $(C_1, C_2, C_3)$   
If not, try another permutation
6. Calculate distance to entry point,  
set  $NPLANE=1$
7. If no entry point has been found after  
three permutations, set  $NPLANE=0$

FIXALL (UX,UY,UZ,CX,CY,CZ,UN,VN,WN,ANGLE,A,B,C,)

FUNCTIONS: Determines normal to the scattering plane  
and the angle through which the Stokes  
vector must be rotated

PARAMETERS: U = UX,UY,UZ Direction cosines of post-  
scattering photon  
C = CX,CY,CZ Direction cosines of pre-  
scattering photon  
N = UN,VN,WN Direction cosines of normal  
to previous scattering plane  
ANGLE Necessary angle of rotation  
M = A,B,C Direction cosines of normal  
to new scattering plane

ACTIONS:

1. Checks (UX,UY,UZ) and CX,CY,CZ) for  
parallelism if parallel, return with  
(A,B,C)=(UN,VN,WN),ANGLE=0.
2. Computes direction cosines of normal to  
scattering plane, (A,B,C) via NORMAL
3. Computes dot product N•M and thence  
the rotation angle magnitude
4. Sets ANGLE=-ANGLE IF  $C \cdot (M \times N) < 0$ .

NORMAL (CX1,CY1,CZ1,CX2,CY2,CZ2,CX,CY,CZ)

FUNCTION: Computes direction cosines of unit vector  
normal to the plane defined by two vectors

PARAMETERS:

V1 = (CX1,CY1,CZ1) Direction cosines of one  
vector defining plane

V2 = (CX2,CY2,CZ2) Direction cosines of other  
vector defining planes

N = (CX,CY,CZ) Direction cosines of NORMAL

ACTION: 1. Computes  $N = \underline{V1} \times \underline{V2}$   
2. Normalizes N to unit magnitude

$$\text{i.e. } N = \frac{\underline{V1} \times \underline{V2}}{|\underline{V1} \times \underline{V2}|}$$



JIM (COUT,CIN,CP,SP,CB,SB)

FUNCTION: Computes photon direction cosines after scattering given the direction cosines prior to scattering and the polar and azimuthal scattering angles

PARAMETERS: COUT(J) J=1,3 Photon position coordinates  
J=4,6 Post-scattering direction cosines  
CIN(J) J=1,3 Photon position coordinates  
J=4,6 Pre-scattering direction cosines  
CP,SP Cosine and sine of azimuthal scattering angle  
CB,SB Cosine and sin of polar scattering angle

ACTION: Let  $\theta, \phi$  = polar coordinates of CIN(J), J=4,6  
then  
$$\text{COUT}(4) = \text{CB} * \text{CIN}(4) - \text{SB} * \text{SP} * \text{SIN}(\phi) + \text{SB} * \text{CP} * \text{CIN}(6) * \text{COS}(\phi)$$
$$\text{COUT}(5) = \text{CB} * \text{CIN}(5) + \text{SB} * \text{SP} * \text{COS}(\phi) + \text{SB} * \text{CP} * \text{CIN}(6) * \text{SIN}(\phi)$$
$$\text{COUT}(6) = \text{CB} * \text{CIN}(6) - \text{SB} * \text{CP} * \text{SIN}(\theta)$$

XSECTM

XS2

FUNCTION: These essentially similar routines perform table look-up and interpolation of the phase function given a value for the scattering angle,  $B$ . XSECTM operates only on  $S_{11}$  and XS2 operates on general phase matrix elements.

METHOD: Three point Newton's method - see for example R.W. Hamming, Numerical Methods for Scientists and Engineers, McGraw-Hill, New York, 1962; p 99.

## ANGLEM

FUNCTION: Given a rectangularly distributed random number, and the scattering species index, chooses a scattering angle by table look-up. Uses the scattering angle distribution function formed from  $S_{11}$  for the indicated species.

PARAMETERS: Where JK points to the scattering species

$X1(JK,100)$  = Table of scattering angles for species JK

$Y1(JK,100)$  = Probability distribution function for the angles listed by  $X1$  computed from  $S_{11}$ .

METHOD: 2 or 3-point Newton's method

## ELEMTS (BETA,S,K)

FUNCTION: Computes all the scattering matrix elements (for an atmospheric scattering) for a specified scattering angle BETA.

PARAMETERS: BETA = Scattering angle  
S(I) = Result value of I<sup>th</sup> matrix element  
S(1) =  $S_{11}$   
S(2) =  $S_{12}$   
S(3) =  $S_{33}$   
S(4) =  $S_{34}$   
S(5) =  $S_{22}$   
S(6) =  $S_{44}$

ACTIONS: Use XSECTM to obtain S(1) for hypothetical scattering (S(1)=1 for real scattering).  
Use XS2 for remaining matrix elements.

RENEW (COUT,BETA,CB)

FUNCTION: Updates the cumulative scattering matrix following a real scattering

PARAMETERS: COUT = Six-vector describing post-scattering photon  
BETA = Scattering angle  
CB =  $\cos(\text{BETA})$

- ACTIONS:
1. Determine normal to new scattering plane and the angle between it and the normal to the previous scattering plane (or reference direction) using FIXALL
    - 1.1 Update scattering plane normal
  2. Post-multiply a rotation into the cumulative scattering matrix
  3. Obtain scattering matrix elements and accumulate a scattering by post-multiplication
    - 3.1 For ground scattering obtain matrix elements from LAMBRT (Lambertian scattering) or from GENGND (rough Fresnel scattering) and use GENSCA to accumulate the scattering.
    - 3.2 For atmospheric scattering, obtain Mie or generalized scattering matrix elements from ELEMTS. Accumulate the scattering using SCATRA (Rayleigh scattering-matrix elements computed), GENSCA (general scattering), or SCATMI (Mie scattering).
  4. Update CIN to the values contained in COUT.

FUNCT (A1,B1,C1,D1,IDIST,D)

FUNCTION: Computes the value of the particle diameter probability density function for a given particle diameter.

```

PARAMETERS:  A1,B1,C1  =  distribution function parameters
              D1       =  Normalization factor
              IDIST     Specifies type of distribution
                      =  1  Junge
                      =  2  Deirmendjian
                      =  3  Log-normal
                      =  4  Haze-C (Junge with pedestal)
              D         =  Particle diameter

```

USE:        FUNCT is called as a function

```

ACTIONS:      IDIST=1  FUNCT = D1*D-B1      D>A1
               = 0.    D<A1

               IDIST=2  FUNCT = D1*DA1 exp (-B1*DC1)

               IDIST=3  FUNCT = 0.              D<C1
               =  $\frac{D1}{D-C1} \exp\{-[A1*\ln(\frac{D-C1}{B1-C1})]^2\}$ 

               IDIST=4  FUNCT = 0              D<C1
               = D1      C1<D<A1
               = D1( $\frac{A1}{D}$ )B1      D>A1

```

GENSCA (SSIN,SOUT,SK,K)

SCATMI (SSIN,SOUT,S,K)

SCATRA (SSIN,SOUT,CB,K)

FUNCTIONS: These similar routines accumulate a new scattering by post-multiplying the scattering phase matrix into the cumulative scattering matrix for real or hypothetical (sampling) scattering.

PARAMETERS: SSIN = 16-element vector containing the elements of the 4x4 cumulative scattering matrix arrayed column-wise.

SOUT = 16-element vector of elements of cumulative scattering matrix after scattering.

S = 6-element vector of matrix element values

K = 1 Compute only first column of SOUT (i.e., first 4 elements) for hypothetical (sampling) scattering. All elements are not needed for unpolarized incident light.

K = 2 Compute all elements of SOUT.

CB = Cosine of scattering angle used by SCATRA to compute scattering matrix elements.

ACTIONS: If  $\underline{\underline{S_o}}$ , is the output matrix,  $\underline{\underline{S_I}}$  is the input matrix

$$\underline{\underline{S_o}} = \underline{\underline{S_I}} \times \begin{pmatrix} S_{11} & S_{12} & 0 & 0 \\ S_{12} & S_{22} & 0 & 0 \\ 0 & 0 & S_{33} & S_{34} \\ 0 & 0 & -S_{34} & S_{44} \end{pmatrix}$$

SPECIALIZATION: SCATMI Assumes that  $S_{33}=S_{44}$  and  $S_{11}=S_{22}$

Assumes that  $S_{11}=1$  if  $K=2$

SCATRA Computes  $S_{11}=\frac{3}{4} (1+(CB)^2)=S_{22}$

$$S_{12}=\frac{3}{4} ((CB)^2-1)$$

$$S_{33}=\frac{3}{2} \quad CB=S_{44}$$

$$S_{34}=0.$$

Takes  $S_{11}=1$  and normalizes other  
matrix elements by  
dividing by  $\frac{3}{4}(1+(CB)^2)$   
if  $K=2$ .



## ROTATE (SSIN,SOUT,PHI)

FUNCTION: Folds a rotation into the cumulative scattering matrix by post-multiplication.

PARAMETERS: SSIN = 16-element vector containing column-wise ordered elements of the cumulative scattering matrix

SOUT = 16-element vector containing elements of the cumulative scattering matrix after rotation.

PHI = Rotation angle

ACTIONS:  $\underline{\underline{S_o}}$  is the cumulative scattering matrix after rotation

$\underline{\underline{S_I}}$  is the cumulative scattering matrix before rotation

$\phi$  = rotation angle

$$\underline{\underline{S_o}} = \underline{\underline{S_I}} \times \begin{pmatrix} 1 & 0 & 0 & 0 \\ 0 & \cos 2\phi & \sin 2\phi & 0 \\ 0 & -\sin 2\phi & \cos 2\phi & 0 \\ 0 & 0 & 0 & 1 \end{pmatrix}$$

## REFLOC (CG,IRCOD)

FUNCTION: Returns a value of IRCOD indicating the reflectance type at a point indicated by CG corresponding to the map choice fixed by INPUT.

PARAMETERS: CG(1),CG(2) = X-Y location of point of impact of photon on the ground  
IRCOD = Reflectance type code  
          = 0 Lambertian  
          = 1 Rough Fresnel

ACTIONS:

1. If ground is uniform plane (i.e., IRPAT=0) IRCOD=IRBGD
2. If map is half-planes |IRPAT|=1  
then  
    for IRPAT=+1 and X>XBND IRCOD=IRSPOT  
    for IRPAT=-1 and X<XBND IRCOD=IRSPOT  
    with  
        IRCOD=IRBGD otherwise
3. If map consists of rectangles differing from background (IRPAT=2)  
then  
    IRCOD=IRSPOT if |X-CNTRX| $\leq$ EDGEEX/2  
                  and |Y-CNTRY| $\leq$ EDGEY/2  
    IRCOD=IRBGD otherwise

## LAMBRT (COUT,S,K)

FUNCTION:     Constructs matrix elements appropriate to  
              Lambertian scattering

PARAMETERS:   COUT = Descriptor vector for scattered photon  
                      COUT(6)=zenith cosine  
              S     = 6-vector of matrix elements  
              K     = 1 Indicates hypothetical scattering  
              K     = 2 Indicates real scattering

ACTIONS:     S(1) = 2\*COUT(6)     K=2  
              S(1) = 4\*COUT(6)     K=1  
              S(J) = 0     J=2,6

GNDREF (COUT,CIN,XTH,XPH,IRCOD)

FUNCTION: Generates a reflection direction from the ground

PARAMETERS: COUT = Post-scattering photon descriptor  
CIN = Pre-scattering photon descriptor  
XTH,XPH = Uniformly distributed random numbers  
IRCOD = Reflectance type indicator  
= 0 Lambertian  
= 1 Rough Fresnel

ACTIONS:

1. For Lambertian reflection
$$\phi = 2\pi * XPH$$
$$\text{Cos}(\theta) = XTH$$
$$COUT(4) = \text{SIN}\theta \text{ COS}\phi$$
$$COUT(5) = \text{SIN}\theta \text{ SIN}\phi$$
$$COUT(6) = \text{COS}\theta$$
$$COUT(J) = CIN(J), \quad J=1,3$$
2. For rough Fresnel reflection
  - 2.1 Find slope X,Y components from Gaussian distribution through GAUSS (standard deviation=WSIG, mean=0.)
  - 2.2 Compute normal to slope (direction cosines labeled WNG(I), I=1,3)
  - 2.3 Check to see if slope is visible to incident photon (visible if
$$G = \sum_{J=1}^3 CIN(J) * WNG(J) \leq 0.$$
)
  - 2.4  $COUT(J+3) = -2G * WNG(J) + CIN(J+3)$  forms the direction cosine of reflection direction

GENGND (COUT,CIN,IRCOD,S,K)

FUNCTION: Computes Fresnel matrix elements multiplied by statistical factors

PARAMETERS: COUT,CIN = Scattered and unscattered photon descriptors, respectively

IRCOD = Not used

S = 6-vector of matrix elements

K = 1 Hypothetical (sampling) scattering

= 2 Real scattering

ACTIONS: Let  $\underline{V}_o$  and  $\underline{V}_i$  be the (unit) photon propagation vectors following and prior to reflection, respectively and  $\underline{n}$  be the normal to the surface facet.

1. Compute cosine of angle of incidence:

$$\cos X = \sqrt{\frac{1 - \underline{V}_o \cdot \underline{V}_i}{2}}$$

2. Compute factor to account for non-vertical incidence of photon (modification to probability of encounter for a chosen facet slope)

$$\text{FACTR} = \cos X / [(\hat{n} \cdot \hat{Z}) (-\hat{Z} \cdot \underline{V}_i)]$$

3. Compute cosine of angle of refraction

$$\cos \theta_t = \sqrt{1 - \frac{1}{f^2} (1 - \cos^2 X)} \quad f = \text{Index of refraction}$$

4. Compute Fresnel factors

$$R_{11} = \frac{f \cos X - \cos \theta_t}{f \cos X + \cos \theta_t} ; R_1 = \frac{\cos X - f \cos \theta_t}{\cos X + f \cos \theta_t}$$

5. Compute matrix elements

$$S_{11} = (R_{11}^2 + R_1^2)/2 = S_{22}$$

$$S_{12} = (R_{11}^2 - R_1^2)/2$$

$$S_{33} = S_{44} = R_1 R_{11}$$

$$S_{34} = 0$$

6. If  $K=1$ , compute probability of encountering proper slope; FEXP

7. Fold all auxilliary factors into matrix elements.

TAB (VSAMP2,VSAMP3,XMC,XX,IND,IFL)

FUNCTION: Compute and display mean, variance, standard deviation, and standard error for each sun, each Lambertian albedo pattern, and each Stokes' parameter (I,Q,U,V) for single scattering, multiple scattering and total. Compute correlation coefficients amongst suns.

PARAMETERS: VSAMP2 = Sample matrix VSAMP2(IQUV,ISUN,IS,1,IALB)  
where  
IQUV Points to Stokes' parameters  
ISUN Designates the sun  
IS Designates direct sun contribution,  
single scattering, and higher order  
scattering.  
VSAMP3 = Sample matrix of squares of clumps  
XMC = Number of clumps  
XX = Factor used to normalize results to  
the number of photons actually tracked  
(when this varies from NMAX).  
IND = 5 or 6 display results only for zero  
albedo  
IFL = Indicator designating whether answers  
are for flux or intensity

ACTIONS: 1. Compute normalization factors  
 $f = (\text{solar const.}) / 4\pi$   
2. Compute and write means and standard  
deviations  
$$\text{std. dev.} = \sqrt{\frac{XMC}{XMC-1} [VSAMP3 * f^2 * XMC - (\text{MEAN})^2]}$$
  
3. Compute variance =  $(\text{std. dev.})^2 = \sigma^2$   
and standard error =  $\sqrt{\sigma^2 / XMC}$   
4. Compute correlation coefficient matrix  
for results for each solar direction.

## OUTPUT (VSAMP,IND,FACT)

FUNCTION:      Normalize results, write out intensity or flux results labeled by Lambertian albedo pattern. If appropriate, compute effective albedo evaluated from regression on uniform albedo patterns and modulation transfer functions.

PARAMETERS:   VSAMP = Sample matrix  
                 IND    = Not used  
                 FACT   = Normalization adjustment factor  
                         (normally FACT=.25)

- ACTIONS:
1. Compute normalization factor  
 $f = (\text{solar const.}) * \text{FACT} / \pi$ . If receiver is the face of a cloud, normalize to unit flux incident on the cloud (Cox-McKee normalization).
  2. Write out results (normalized) for intensity or flux. For intensity, results are direct sun contribution, single scattering, higher order scattering, and total intensity. For flux, results are direct solar contribution, upward flux, downward flux, total flux.
  3. If the Lambertian albedo patterns contain uniform planes with  $A=0$ . and at least two others (and if the reflectance type map is uniformly Lambertian) perform a regression analysis: find AL,BL in the expression

$$[I(A) - I(0)] / A = AL + BL * [I(A) - I(0)]$$

where A refers to the albedo and I(A) is the result for albedo=A. Use AREG. Also computed are the effective albedos for other albedo patterns.



4. If appropriate (IMTF=1, set by ALBEDO)  
compute percent contrast from pairs of  
results both for intensity and effective  
albedo.

ALBEDO (IALB,ALBPT)

FUNCTION:     Write titles or compute the albedo at the  
                 point specified by CG.

ACTIONS:    1. IALB = -J   Write out description (50 character maximum width) of albedo pattern J.  
                 IALB = +J   Compute albedo at the point  
                             X=CG(1), Y=CG(2) and return this  
                             value as ALBPT.

2. If this pattern is for computing MTF's, set  
   IMTF=1.

AREG (NALB,AL,BL)

FUNCTION: Perform albedo regression analysis assuming  
FTOT (NALB) is the value corresponding to a  
uniform zero albedo plane.

PARAMETERS: NALB = Total number of albedo patterns  
NUNIF = Number of uniform plane albedo  
patterns  
AL,BL = Regression coefficients

ACTIONS: 1. Use LINFIT to compute albedo regression  
coefficients AL,BL

Regression Form:  $[I(A) - I(A=0.)] / A = AL + BL * [I(A) - I(A=0.)]$

2. Compute effective albedo (AEFF(I), I=1,NALB-1):

$$AEFF(I) = \frac{I(J) - I(NALB)}{AL + BL * (I(J) - I(NALB))}$$

$$AEFF(NALB) = 0.$$

LINFIT (N,Y,X,A,B)

FUNCTION: Performs linear regression, finding the parameters A,B which best fit the form  $Y=A+B*X$  where  $Y(N),X(N)$  are vectors of length N.

METHOD:

$$B = \frac{N \sum_{i=1}^N X_i Y_i - \sum_{i=1}^N X_i \sum_{i=1}^N Y_i}{N \sum_{i=1}^N X_i^2 - \left( \sum_{i=1}^N X_i \right)^2}$$

$$A = \frac{1}{N} \left( \sum_{i=1}^N Y_i - B \sum_{i=1}^N X_i \right)$$

## SECTION 5.0

### INPUT PARAMETERS

The input parameters are listed below, together with a concise description of their use, meaning, and default values (if applicable). The order of appearance is that of a proper data deck.

Initial random number (may be blank, default value = 65549)

(I7)

IND,IST,ISKY,INFLUX,WAV

(4I1,F8.5)

IND = Calculation extent indicator

= 0 Stop calculation

= 2 Input new clouds and receivers only

= 4 Normal start

= 5 Omit polarization, set scattering matrix

$S_{ij}=0$  for  $i,j \neq 1$

= 6 Calculate only for completely absorbing ground

= 7 Completely absorbing ground + no polarization

IST = New atmosphere indicator

= 1 Read in new atmosphere

= 0 Use one already read in

ISKY = Sun indicator

= 0 User specified suns (maximum of 5)

= 1 Suns at  $\theta=0^\circ, 30^\circ, 60^\circ; \phi=0$

= 2 Suns at  $\theta=0^\circ, 30^\circ, 60^\circ; \phi=\pi/4$

= 3 Suns at  $\theta=0^\circ, 30^\circ, 60^\circ; \phi=\pi/2$

INFLUX = Indicator specifying whether flux or intensity is to be calculated.

= 0 Calculate flux at receiver

= 1 Calculate intensity at receiver

WAV = Wavelength of radiation (in micrometers).

INDIC(5), IDIST(5), NLAYER, NSOL, NMAX, NSCA, NALB, IUNIT(5), NTOT(5)  
(10I1, 2I3, I6, 7I2, 5I3)

INDIC(k) = Indicator for type of  $k^{\text{th}}$  species.

$\geq 5$  If species is not present

= 0 For Rayleigh (matrix elements computed)

= 1 For monodisperse Mie (matrix elements  
read from binary tape)

= 2 For polydisperse Mie (matrix elements  
computed while reading from binary tape)

= 3 For experimental data (matrix elements  
read from cards)

= 4 For ozone (absorption only)

IDIST(k) = Particle diameter distribution indicator  
for  $k^{\text{th}}$  species.

= 1 For Junge distribution

= 2 For Deirmendjian's Haze model

= 3 For log-normal distribution

= 4 For Haze C (Junge with pedestal)

NLAYER = Number of plane parallel layers in ambient  
atmosphere.

NSOL = Number of solar zenith angles to be con-  
sidered.

NMAX = Number of photons to be tracked

NSCA = Maximum number of scatterings allowed per  
photon track

NALB = Number of Lambertian albedo maps

IUNIT(k) = Indicator of (tape) unit from which matrix  
elements of  $k^{\text{th}}$  species is to be read.

NTOT(k) = Number of diameter steps to be read for  
the  $k^{\text{th}}$  (polydisperse) scattering species.

INDICA(5)

(5I1)

INDICA(k) = Indicator similar to INDIC(k) but applicable to ambient atmosphere (not clouds).

Note - Any species appearing in INDICA must also appear in INDIC.

SCALE(5)

(5E11.6)

SCALE(k) = 0. Use cross section as otherwise read in and/or computed for species k.

>0. Scale cross section of ambient atmosphere component k so that the total vertical optical thickness of component k=SCALE(k).

AR,BR

(2F8.6)

AR and BR specify the Rayleigh cross section  $\sigma_R$ :

$\sigma_R = AR \times 10^{-28} \times \lambda^{-BR}$ , where  $\lambda$  is the wavelength.

ADEF,EXPFAC

(2F8.5)

ADEF = Ozone cross section

$$\sigma_{03} = ADEF / 2.687 \times 10^{19}$$

EXPFAC = Scale height adjustment parameter for molecular species. If H is the effective scale height computed from densities as read from cards, the adjusted scale height  $H' = H / (1 - H * EXPFAC)$ .

INDOZ,INDCOZ

(2I1)

INDOZ        = Ozone input units specification  
             = 0 Ozone densities  $\text{cm}^{-3}$  are read in  
              $\neq 0$  Ozone partial pressures are read in  
             = 1 Ozone densities computed from partial  
                 pressures are temperature corrected.  
INDCOZ       Inactive parameter, no function ascribed  
             for it in this version.

SOLC

(F10.6)

SOLC        = Solar constant assumed for normalization  
             = 0. (or blank) on input, a value of 1.0  
                 is adopted.  
              $\neq 0$ . Use the specified value of SOLC.

If ISKY=0, solar directions must be read in as follows:

THETA(1),PHI(1)

(F7.4,F7.2)

:

THETA(NSOL),PHI(NSOL)

THETA(I)    = Solar zenith angle for  $I^{\text{th}}$  sun (in degrees)

PHI(I)      = Solar azimuth from  $I^{\text{th}}$  sun (in degrees)

NK(1),STEP(1),A1(1),B1(1),C1(1),ITAPE(1)

(I3,4F8.3,I1)

:



[When the  $K^{\text{th}}$  species' matrix elements are to be read from cards, they appear as follows:]

NK(K), STEP(K), ...

CSECT(K), ASECT(K)

(2E11.4)

XA, S11(1,K), S12(1,K), S22(1,K), S33(1,K), S34(1,K), S44(1,K)

(F6.1, 6E12.5)

XA, S11(NK,K), S12(NK,K), ...

⋮

NK(KMAX), STEP(KMAX), A1(KMAX), ... (Where KMAX is the maximum  
total number of atmospheric  
species present)

NK(K) = Number of angles for which the matrix elements  
of the  $K^{\text{th}}$  species are to be read from tape  
or cards.

STEP(K) = Step size in  $x$  ( $x = \pi D/\lambda$ ) for polydispersions  
( $K^{\text{th}}$  species)  
= Value of  $x$  for monodispersions ( $K^{\text{th}}$  species)

A1(J), B1(J), C1(J) are the parameters entering into the  
particle size distribution function  
for the  $J^{\text{th}}$  scatterer type.

For IDIST(J) = 1, the diameter distribution is

$$F = D1 D^{-B1} \quad D \geq A1$$

where  $D1 = (B1-1) A1^{(B1-1)}$

For IDIST(J)=2

$$F = D1 D^{A1} \exp(-BB1 * D^{C1})$$

$$\text{where } D1 = \frac{C1 B1^{(A1+1)/C1}}{(2^{A1+1}) \Gamma(\frac{A1+1}{C1})}$$

$$BB1 = B1 * 2^{-C1}$$

For IDIST(J)=3

$$F = \frac{D1}{D-C1} \exp \left\{ - \left[ A1 \log \left( \frac{D-C1}{B1-C1} \right) \right]^2 \right\}, D > C1$$

$$= 0. \quad D \leq C1$$

$$\text{where } D1 = A1/\sqrt{\pi}$$

For IDIST(J)=4

$$F = 0. \quad D < C1$$

$$F = D1 \quad C1 \leq D < A1$$

$$F = D1 \left( \frac{A1}{D} \right)^{B1} \quad A1 \leq D$$

$$\text{where } D1 = \frac{B1-1}{(B1-1)(A1-C1)+A1}$$

ITAPE(J) = 0 Use NTOT(J) and STEP(J) as read from cards.  
 = 1 Read NTOT(J) and STEP(J) from Mie tape.

XH(1),TEMP(1)

(F3.0,2X,F3.0)

⋮

XH(NLAYER),TEMP(NLAYER)

XH(J) = Layer top height of J<sup>th</sup> ambient atmospheric  
 layer (in km.)

TEMP(J) = Temperature of J<sup>th</sup> layer (in °K)

XH(1),DENS(1,1)

(F3.0,2X,E9.3)

⋮

XH(NLAYER),DENS(1,NLAYER)

XH(1),DENS(2,1)

⋮

XH(NLAYER),DENS(KMAX,NLAYER)

XH(J) = Layer top height of J<sup>th</sup> ambient atmospheric  
layer (in km.)

DENS(K,J) = Density of K<sup>th</sup> species in J<sup>th</sup> layer (cm<sup>-3</sup>)

NCLOUD

(I3)

NCLOUD = Number of clouds to be considered.

\*\*\* The following are read in if NCLOUD>0

HC(1),AC(1),BC(1),CC(1),XCL(1),YCL(1),THETAC(1),INC(1),CLDEN(1)  
(F8.5,5F8.3,F8.5,I3,E9.3)

⋮

HC(NCLOUD),AC(NCLOUD),...

HC(I) = Altitude of bottom surface of I<sup>th</sup>  
cloud (in km.)

AC(I),BC(I),CC(I) = Edge lengths of I<sup>th</sup> cloud (in km.)

THETAC(I) = Angle between the x-axis of the  
cloud and that of the general  
co-ordinate system (measured  
clockwise in degrees looking up  
from the ground).

INC(J) = Indicator of the atmospheric con-  
stituent appropriate to I<sup>th</sup> cloud  
[e.g., INC(1)=3 states that cloud  
number 1 is composed of the species  
specified by INDIC(3)].

CLDEN(I) = Density of cloud-specific scatters  
of the type labeled by INC(I) (in cm<sup>-3</sup>).

IRCLD, IREC, RECANG, HR, CZO, RPHI, RX, RY, SZO, IAPAT, NCON  
(2I2, 7E10.4, 2I2)

IRCLD = Receiver extent indicator  
= 0 Receiver with infinitesimal area  
= J>0 Receiver extends over an entire face of cloud J.

IREC Specifies which face of the cloud is to be the receiver.  
= 1 + X Face of cloud IRCLD  
= 2 - X Face of cloud IRCLD  
= 3 + Y Face of the cloud IRCLD  
= 4 - Y Face of cloud IRCLD  
= 5 + Z Face of cloud IRCLD  
= 6 - Z Face of Cloud IRCLD  
< 0 Receiver points out of cloud IRCLD.  
|IREC| specifies which face as above.

RECANG = Apex angle of cone of receiver field of view in milliradians.

HR = Height of receiver (ignored if receiver is a cloud face)

CZO = Zenith cosine of receiver pointing direction (ignored if receiver is a cloud face)

RPHI = Azimuthal angle of plane containing receiver field of view and the vertical (ignored if receiver is a cloud face)

RX, RY = X, Y co-ordinates of receiver (ignored if receiver is a cloud face)

SZO = Sine of receiver zenith angle  
= 0. or blank - SZO is computed from CZO  
≠ 0. CZO,, computed from SZO (ignored if receiver is a cloud face)

IAPAT = Index of albedo pattern for which the intensity is to be mapped within the receiver field of view.  
DEFAULT VALUE-IAPAT=1 (Max=50)

NCON = Number of THETA BINS=Number of PHI bins for mapping of response within the receiver field of view.  
DEFAULT=20 (Max=20)

IRPAT,IRBGD,XBND,FN,WSPD,WC0,WC1,WSIG2

(2I2,6E11.4)

IRPAT = Specification of reflectance type map  
= 0 Uniform plane (= Background)  
=+1 Plane differs from background for  $X > XBND$   
=-1 Plane differs from background for  $X < XBND$   
= 2 Inhomogeneties are rectangles set upon  
uniform background plane.

IRBGD = Specification of character of background  
= 0 Background is Lambertian  
= 1 Background is rough Fresnel

XBND = Boundary line for half-plane pattern  
= X-co-ordinate of line parallel to Y-axis

FN = Index of refraction for Fresnel reflectance  
DEFAULT=1.338

WSPD = Wind speed (m/sec.) for rough Fresnel

WC0,WC1 = Parameters used to construct variance, WSIG2  
If both = 0 (or Blank), use default values:  
WC0= .0015  
WC1=2.54E-03

WSIG2 = Variance for Gaussian slope distribution for  
rough Fresnel reflectance  
Non-zero or non-blank entry takes precedence  
over value computed from WC0,WC1, and WSPD.

If IRPAT=2, the following cards are required.

NSPOT

(I2)

NSPOT = Number of non-overlapping rectangular inhomo-  
geneities (maximum NSPOT=20)

CNTRX(1),CNTRY(1),EDGEEX(1),EDGEY(1)

(4E11.4)

:

CNTRX(NSPOT),CNTRY(NSPOT),...

CNTRX(J),CNTRY(J) = X-Y co-ordinates of rectangle J

EDGEEX(J),EDGEY(J) = X,Y edge lengths of rectangle J

# MIE TAPE FORMATS

## MONODISPERSE

$$I=1,n \left\{ \begin{array}{l} \text{REFACT}, \text{ALPHA}, \text{QSCA}, \text{COSBAR}, \text{QEXT} \\ J=1, \text{NK}(K) \{ \text{XA}, \text{AA1}, \text{AA2}, \text{S33}(J,K,1), \text{S34}(J,K,1), \text{S11}(J,K), \text{S12}(J,K,1) \} \end{array} \right.$$

where

$n$  is computed from  $A1(K)$  and  $STEP(K)$  read in on cards:

$n = \text{INT}(A1(K) \cdot (STEP(K) + .5))$

$\text{REFACT} = \text{complex index of refraction}$

$\text{ALPHA} = \text{size parameter } \alpha = \pi d / \lambda, d = \text{diameter},$   
 $\lambda = \text{wavelength}$

$\text{QSCA} = \text{scattering cross section normalized by geometric cross section}$

$\text{QEXT} = \text{extinction cross section normalized by geometric cross section}$

$$\text{eg } \sigma_{\text{SCA}}(\text{cm}^2) = Q_{\text{SCA}} \times \pi \frac{d^2}{4} \times 10^{-8}$$

with  $d$  in micrometers

$\text{COSBAR} - \text{not used}$

$\text{NK}(K) = \text{number of scattering angles for species } k$

$\text{XA} = \text{scattering angle (degrees)}$

C-2

$$\left. \begin{array}{l} S33 \\ S11 \\ S12 \end{array} \right\} \begin{array}{l} \text{Scattering matrix elements for Jth scattering} \\ \text{angle kth species} \end{array}$$

S34 = -S34 as used by this code

### POLYDISPERSE

NT, ST [Read only if ITAPE≠0; for ITAPE=0, values are taken from card input.]

$$I=1, NT \left\{ \begin{array}{l} \text{REFACT, ALPHA, QSCA, COSBAR, QEXT} \\ J=1, NK(K) \{ XA, AA, BB, XX3, XX4, YY, XX2 \} \end{array} \right.$$

NT = number of steps in size

ST = dimensionless step size =  $\frac{\pi}{\lambda} \times \delta d$  where  $\delta d$  is the step size in diameter (microns)

REFACT, ALPHA, QSCA, COSBAR, QEXT as described under MONODISPERSE input

XA = scattering angle (degrees)

AA, BB - not used

$$\left. \begin{array}{l} XX3 = S33 \\ XX4 = -S34 \\ YY = S11 \\ XX2 = S12 \end{array} \right\} \begin{array}{l} \text{Scattering matrix elements for size} \\ \text{parameter ALPHA, scattering angle XA} \end{array}$$

SECTION 6.0  
CTrans PROGRAM LISTING



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TORT(I) = DIRECTION OF TOP OF ITH LAYER MEASURED AS
          FOR FORWARD PASS
COS(J).*(J)= DIRECTION COSINES OF THE SOLAR ANGLES
              TO BE CONSIDERED
VSAMP = SAMPLE MATRIX
VSLN = IN-CLOUD SOLAR DIRECTIONS
TCARDS = INITIAL RANDOM NUMBER (MAY BE BLANK)

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(17)
IRCLD,151,15SKY,INFLUX,NAV
(41,F9.5)
INDIC(5),101ST(5),N1AYER,NSCL,NMAX,NSCA,NALB,IUNIT(5),NTCT(5)
(1311,1515,10,712,515)
INDICATE(F)
(211)
SCALE(5)
(211)
AR,BA
(258,6)
AUCF,EXPFC
(258,4)
INDCZ,INDCZ
(211)
SOLC (F10,6)
(IF 15KYEC)
THETA(1),PHI(1)
(F7,4,F7,2)
.
.
.
THETA(NSCL),PHI(NSCL)
NK(1),STEP(1),AI(1),BI(1),CI(1),ITAPE(1)
(12,4F8,3,11)
.
.
.
NK(KMAX),STEP(KMAX),AI(KMAX),...
XH(1),TEMP(1)
(F3,6,2X,F3,6)
.
.
.
XH(NLAYER),TEMP(NLAYER)
XH(1),DENS(1,1)
(F3,6,2X,E9,3)
.
.
.
XH(NLAYER),DENS(1,NLAYER)
.
.
.
XH(NLAYER),DENS(KMAX,NLAYER)
NCLUD
(13)
HC(1),AC(1),BC(1),CC(1),XCL(1),YCL(1),THETAC(1),INC(1),CLDEN(1)
(F9,5,5F8,3,F8,5,13,E5,3)
.
.
.
HC(NCLUD),AC(NCLJUD),...
IRCLD,152,15CANG,NR,CZ,NPHI,FX,FY,S20,IAPAT,NCCN
(212,7E10,4,212)
IRPAT,IRPCD,XUND,FN,MSFD,WCD,WCI,MSIG2
(212,CE11,4)
THE FOLLOWING ARE REQUIRED IF IRPAT = 2
NSPT (12)
CNTRY(1),CNTRY(1),EDGEY(1)
(4E11,4)
.
.
.
CNTRY(NSPT),...
****
*****
DIMENSION DSUNT(13),DSUNP(15),ETA(15),TSUN(15),PSUN(15)
DIMENSION LCSNUM(20,20)
.
.
.
DIMENSION NUMAP(1,20),CONMAP(20,20,15),PHMAP(20),THMAP(20)
DIMENSION
1522(100,5,2),S33(100,5,2),S34(100,5,2),S12(100,5,2),
3X1(5,100),Y1(5,100)
DIMENSION CDF(5,100)
DIMENSION CULT(0)
.
.
.
15N C004
15N C005
.
.
.
15N C006
15N C007
```



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```
112 CONTINUE
DO 55 ITH=1,20
  PRVAP(ITH)=0.
  THAP(ITH)=0.
  DO 55 JTH=1,2
    LUSUM(ITH,JTH)=0
    NLVAP(ITH,JTH)=0
  DO 55 ISN=1,15
    CNVAP(ITH,JTH,ISN)=0.
  55 CONTINUE
  KK=1
  DO 40 ISCA=1,200
    NURSCA(1SCA)=0
  40 CONTINUE

C READ LINE PAIR DESIGNATION UNDER STUDY
C AND ATMOSPHERE CHARACTERISTICS. COMPUTE PARAMETERS REQUIRED
C LATER
C
  IRAND=IX
  CALL INPUT(KK,ISKY)
  OTHC=RECANG/FLCAT(NCON)
  SPHC=2*PI/FLCAT(NCON)
  DO 50 ITH=1,NCON
    PRVAP(ITH)=FLCAT(ITH)*DFHC
    THAP(ITH)=FLCAT(ITH)*JTHC
  50 CONTINUE
  NPSTR=SQRT(TFSSR)
  IIRCC(KK)=0
  IMPJ=20
  IF(IIRCC.NE.0) IIRCC(KK)=IIRCC
  70 CONTINUE

C LOOP OVER NUMBER OF PHOTONS TO BE TRACKED
C
  IMOD=MOD(NMAX,NCLUMP)
  IF(IMOD.NE.0) NMAX=NMAX+1-NCLUMP-IMOD
  ADENSE=FLCAT(NMAX)
  DO 20 I=1,NMAX
    20 CONTINUE

C INITIALIZE PHOTON
C
  IMOD=MOD(1,NCLUMP)
  FCLUMP=1.
  ECLUMP=1.
  SWATE=1.
  CIRATE=1.
  INCLD=0
  IF(IIRCLD.EC.0) GO TO 420

C START ON A CLOUD FACE
C
  X2=1.
  Y2=1.
  CALL RANDU(IX,IY,X2)
  IX=IY
  IY=IY
  CALL RANDU(IX,IY,Y2)
  IY=IY
  410 CINC(1)=CLOC(IIRCLD,IFC1+3)*FAC1R
  CINC(2)=CLOC(IIRCLD,IFC2+3)*(X2-.5)*2.
  CINC(3)=CLOC(IIRCLD,IFC3+3)*(Y2-.5)*2.
  SWATE=4*CLOC(IIRCLD,IFC2+3)+CLOC(IIRCLD,IFC3+3)
  DO 415 J=1,10
    DO 415 IJ=1,6
      415 CINC(IJ)=CINC(IJ)
      IF(IIRCLD.LT.0) GO TO 412
      INCLD=IIRCLD
      CPT=CLOC(IIRCLD,3)
      GO TO 421
    412 IIRCLD=0
    DO 415 IJ=1,6
      415 CINC(IJ)=CINC(IJ)
      INCLD=1
      CALL TRANS(IIRCLD,INCLD)
      DO 415 IJ=1,6
        415 CINC(IJ)=CINC(IJ)
      415 CINC(IJ)=CINC(IJ)
      GO TO 421
    420 DO 421 IJ=1,6
      421 IJ=1,6
  C
```

1111

103



ISN 0209 425 CONTINUE

```

ISN 0211 CALL JIM(COUT,CIN,CP,SP,C3,SB)
ISN 0212 DO 423 IJ=4,6
ISN 0213 423 CINTIJ=CCUT(IJ)
ISN 0214 424 CONTINUE
ISN 0215 DO 425 J=1,NLAYER
ISN 0216 JF=J
ISN 0217 425 IF(CXH(J).GE.(CMT+CIN(3)))GC TC 426
ISN 0218 426 CONTINUE
ISN 0219 IUPDN=C

```

```

C IF INITIAL CIN(6).GT.0 FCRAIRS TRACKED PHOTON WOULD BE
C GCING DOWN WHEN IT ENTERED RECEIVER
C

```

```

ISN 0220 IF(CIN(6).GT.0.)IUPDN=1
ISN 0221 WEIGHT=1.
ISN 0222 WEIGHT=WEIGHT*SBWT
ISN 0223 WTIME=WEIGHT
ISN 0224

```

```

C INITIALIZE CUMULATIVE SCATTERING MATRIX
C

```

```

ISN 0225 DO 21 J=2,10
ISN 0226 21 SCUT(J)=C.
ISN 0227 DO 211 J=1,15,5
ISN 0228 211 SCUT(J)=1.

```

```

C INITIALIZE GROUND SCATTERING COUNTER (IGND)
C

```

```

ISN 0229 IGND=C

```

```

C SAMPLE DIRECT SUN
C

```

```

ISN 0230 DO 551 ISUN=1,NSUL
ISN 0231 ICLENCLDI
ISN 0232 IF(INCLC.NE.2)ICL=INCLD
ISN 0233 CUSAN=WSUN(ICL,ISUN,1)*CINR(4)*SUN(ICL,ISUN,2)*CINR(5)*SUN(ICL,ISUN,3)*CINR(6)
ISN 0234 551 CUSAN=LT.CFEC)GU TC 551
ISN 0235 IF(INCLC.EU.2)GU TU 552
ISN 0236 DO 553 IJ=1,3
ISN 0237 IJ2=IJ+3
ISN 0238 CUCUD(IJ)=CIN(IJ)
ISN 0239 CUCUD(IJ2)=WSUN(ICL,ISUN,IJ)
ISN 0240 553 INCL=1
ISN 0241 CALL TRANS(INCLD,INCL)
ISN 0242 GO TO 554
ISN 0243 DO 552 IJ=1,3
ISN 0244 IJ2=IJ+3
ISN 0245 CUCUD(IJ)=CIN(IJ)
ISN 0246 CUCUD(IJ2)=WSUN(ICL,ISUN,IJ)
ISN 0247 554 CONTINUE
ISN 0248 CALL SER SOL(TAUJ)
ISN 0249 IF(CUSAN.EU.C)GU TO 551
ISN 0250 IF(TAUS.JT.15.)TAUS=150.
ISN 0251 DSAMP=EXP(-TAUS)*CUSAN*4.*PI/ADEN
ISN 0252 IF(INFLUX.CC.1)DSAMP=DSAMP/CCSAN
ISN 0253 DSAMP=DSAMP*DTIMAT
ISN 0254 DO 556 IALB=1,NALB
ISN 0255 VSAMP(1,ISUN,1,KK,IALB)=VSAMP(1,ISUN,1,KK,IALB)+DSAMP
ISN 0256 556 CONTINUE
ISN 0257 551 MSCAT=1

```

```

C INITIALIZE ALBEDO TRACK STORAGE
C

```

```

ISN 0264 DO 60 IALB=1,NALB
ISN 0265 60 ALB(IALB)=1.
C LOOP OVER ALBEDO NUMBER OF SCATTERINGS
C

```

```

ISN 0266 ICNDF=1
ISN 0267 DO 22 ISCA=1,NSCA
ISN 0268 IMP=IMP
ISN 0269 IF(IMP.EQ.2.AND.(SCA.GE.2))IMPEX=C
ISN 0270 IF(IMP.EQ.3.AND.(ISCA.LT.IMPJ))IMPEX=C
ISN 0271 IF(ISCA.EQ.1.AND.(INFLUX.EQ.1))IUPDN=C
ISN 0272 IF(ISCA.GT.1.AND.(INFLUX.EQ.1))IUPDN=1
ISN 0273

```

```

C ICUT=0
C

```

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DETERMINE DISTANCE TRAVELED BY PARTICLE BETWEEN SCATT.

PAGE 009

```

15N 0278      ISCAT=0
15N 0279      CALL TIME(ITK1)

15N 0280      INN=0
15N 0281      INX=0
15N 0282      ITEST=0
15N 0283      IF(I.LE.INX.AND.I.GE.IMN) ITEST=1
15N 0284      CALL TRACK(ITOT,ISCAT,IX)
15N 0285      CALL TIME(ITK2)
15N 0286      ITKTIME=ITK1+ITK2-ITK1
15N 0287      C
15N 0288      C****
15N 0289      C
15N 0290      TEST PRINT SECTION *****
15N 0291      IF(IITEST.EQ.0) GO TO 600
15N 0292      WRITE(6,201) I, IOUT, ISCAT, IGND, WEIGHT, INCLD, UN, VN, WN
15N 0293      WRITE(6,202) ISCA
15N 0294      WRITE(6,203) (CIN(IPR), IPR=1,6)
15N 0295      *WRITE(6,204) (CUCOR(IPR), IPR=1,6)
15N 0296      *WRITE(6,205) (CUCOR(IPR), IPR=1,6)
15N 0297      IF(ISCAT.NE.0) WRITE(6,206) (CG(IPR), IPR=1,2)
15N 0298      600 FORMAT(1H, 'I=', I5.2X, 'IOUT=', I5.2X, 'ISCAT=', I5.2X, 'IGND=', I5.2X,
15N 0299      *WEIGHT=', E12.6X, 'INCLD=', I5.2X, 'UN=', E12.6X, 'VN=', E12.6X,
15N 0300      *WN=', E12.6X)
15N 0301      602 FORMAT(1H, 'IX=', I5.2X, 'CIN=', E14.7)
15N 0302      603 FORMAT(1H, 'IX=', I5.2X, 'CUCOR=', E14.7)
15N 0303      604 FORMAT(1H, 'IX=', I5.2X, 'CUCOR=', E14.7)
15N 0304      605 FORMAT(1H, 'IX=', I5.2X, 'CG=', E14.7)
15N 0305      600 CONTINUE
15N 0306      C*****
15N 0307      C
15N 0308      IF((ICUT.NE.0).AND.(ISCA.EQ.1)).AND.(IMAP.EQ.1))
15N 0309      *LCSNUM(ITHC,IPHC)=LCSNUM(ITPC,IFPC)+1
15N 0310      IF(IOUT.NE.0) GO TO 30
15N 0311      GROUND SCATTERING
15N 0312      UPDATE COUNTERS, DETERMINE TYPE OF REFLECTANCE, UPDATE
15N 0313      LAMBERTIAN ALBEDO WEIGHTS (IF LAMJERTIAN), AND GO TO
15N 0314      SAMPLING SECTION
15N 0315      IF(ISCAT.EQ.0) GO TO 310
15N 0316      IF(IND.EQ.6.CH.IND.EQ.7) GO TO 30
15N 0317      MSCAT=ISCA
15N 0318      IGND=IGND+1
15N 0319      CALL REFLOC(CG,IRGCD)
15N 0320      IF(IRCLOC.NE.0) GO TO 62
15N 0321      DO 61 LABEL,NALG
15N 0322      CALL ALBEDO(ALB,ALGPT)
15N 0323      61 ALB=(ALB)*ALPT*ALG
15N 0324      62 CONTINUE
15N 0325      IF((ISCA.EQ.1.AND.ISCAT.EQ.1).AND.(INFLUX.EQ.1)) IUPCN=-1
15N 0326      IF(ISCAT.NE.0) GO TO 25
15N 0327      310 CONTINUE
15N 0328      C
15N 0329      C
15N 0330      DETERMINE SCATTERING SPECIES
15N 0331      TOLDR=
15N 0332      IF((INCLD.GT.0)) ILL=ILL+INCLD
15N 0333      SIGCT=ICL(JJ)+TCLD
15N 0334      SIGCT=ICL(JJ)+TCLD
15N 0335      SIGCT=ICL(JJ)+TCLD
15N 0336      SIGCT=ICL(JJ)+TCLD
15N 0337      CALL RANDU(IX,IY,XX)
15N 0338      IXEY=
15N 0339      IF(XX.LE.SIGCT) GO TO 411
15N 0340      SCATTERER=IS A CLOUD-PARTICLE
15N 0341      C
15N 0342      C
15N 0343      JK=INC(INCLD)
15N 0344      WEIGHT=WEIGHT*(1.-ACLD(INCLD))
15N 0345      GO TO 24
15N 0346      411 CONTINUE
15N 0347      C
15N 0348      C
15N 0349      SCATTERER IS AN AMBIANT ATMOSPHERE PARTICLE
15N 0350      XX=XX/SIGCTM
15N 0351      WN=1.-CDF(1,XX)
15N 0352      WEIGHT=WEIGHT*WN
15N 0353      XX=CDF(1,XX)+XX*WN

```

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```

1SN 0402 VSAMP(11,12,KK)=VSAMP(11,12,KK)+(VSAMP(11,12,i,KK,1)+VSAMP(11,12,
1SN 0403 *12,KK,1)+VSAMP(11,12,i,KK,1))#2
1SN 0404 IGV#2
1SN 0405 CALL OVERFL(IGV)
IF (IGV.NE.2)WRITE(6,555)IGV,11,12,MSCA,
1,IGV,
1SN 0407 VSAMP(11,12,1,1,1).VSAMP(11,12,2,1,1).VSAMP(11,12,3,1,1)
999 FORMAT(1H,IGV=,11,IGV=,11,ISUN=,12,MSCA=,13,2X,
*PHOT=,16,IGV=,12,
*VSAMP(1,2,ANDJ)=,3(14,7,2X))

```

PAGE 011

```

1SN 0408 203 CONTINUE
1SN 0409 DC 203 12=1,2
1SN 0410 DC 203 15=1,NALB
1SN 0411 VSAMP2(11,12,13,KK,15)=VSAMP2(11,12,13,KK,15)*FCLUMP+VSAMP(11,12,1
1SN 0412 *3,KK,15)*FCLUMP
VSAMP3(11,12,13,KK,15)=VSAMP3(11,12,13,KK,15)+VSAMP(11,12,13,KK,15
1SN 0413 *1)*VSAMP(11,12,13,KK,15)
1SN 0414 206 CONTINUE
1SN 0415 DC 206 11=1,4
1SN 0416 DC 204 12=1,NSUL
1SN 0417 DC 204 13=1,3
1SN 0418 DC 204 15=1,NALB
1SN 0419 VSAMP(11,12,13,KK,15)=C,
1SN 0420 CALL REATIM(ISTOP,IGTIM)
1SN 0421 NLP#1
1SN 0422 IF(ISTOP.LE.ITLIM)GO TO 502
1SN 0423 201 CONTINUE
1SN 0424 C
1SN 0425 C
1SN 0426 C
1SN 0427 C
1SN 0428 C
1SN 0429 C
1SN 0430 C
1SN 0431 C
1SN 0432 C
1SN 0433 C
1SN 0434 C
1SN 0435 C
1SN 0436 C
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1SN 0459 C
1SN 0460 C

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**PAGE 014**

\*\*\*\*\*TRAN CACS REFERENCE LISTING\*\*\*\*\*

SYMBOL	INTERNAL STATEMENT NUMBERS
1	1
2	2
3	3
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100	100

SYMBOL	INTERNAL	SYMBOL	INTERNAL
S22	0308	S22	0312
S33	0308	S33	0312
S34	0308	S34	0312
S44	0308	S44	0312
TAU	0308	TAU	0312
TOL	0329	TOL	0329
TUR	0329	TUR	0329
TPI	0342	TPI	0342
UNR	0142	UNR	0142
VNR	0142	VNR	0142
VSA	0354	VSA	0354
WAV	0354	WAV	0354
WNR	0354	WNR	0354
XMC	0354	XMC	0354

XPH	0150	0165	0185	0186	0376	0280
XTH	0145	0486				
ACLO	0127	0372				
ADEN	0122	0234	0234			
DETA	0124	0234	0234			
CIN2	0124	0234	0234			
CUU	0124	0234	0234			
CREC	0124	0234	0234			
DPFC	0124	0234	0234			
DTFC	0124	0234	0234			
FALF	0124	0234	0234			
ICUN	0124	0234	0234			
IFC1	0124	0234	0234			
IFC2	0124	0234	0234			
IFC3	0124	0234	0234			
IGN3	0124	0234	0234			
IMAP	0124	0234	0234			
IMCO	0124	0234	0234			
IMPJ	0124	0234	0234			
IMPX	0124	0234	0234			
INCC	0124	0234	0234			
IOLU	0124	0234	0234			
IPRT	0124	0234	0234			
IOUV	0124	0234	0234			
ISCA	0124	0234	0234			
ISKY	0124	0234	0234			
ISNI	0124	0234	0234			
ISM2	0124	0234	0234			
ISME	0124	0234	0234			
ITFC	0124	0234	0234			
ITK1	0124	0234	0234			
ITK2	0124	0234	0234			
JCCN	0124	0234	0234			
JNUN	0124	0234	0234			
KMAX	0124	0234	0234			
MSCA	0124	0234	0234			
MTUT	0124	0234	0234			
NALJ	0124	0234	0234			
NCUN	0124	0234	0234			
NMAK	0124	0234	0234			
NOPH	0124	0234	0234			
NSCA	0124	0234	0234			
NSCL	0124	0234	0234			
NUMA	0124	0234	0234			
PHIN	0124	0234	0234			
PSUN	0124	0234	0234			
SD*F	0124	0234	0234			
SDTH	0124	0234	0234			
SOUT	0124	0234	0234			
SOHT	0124	0234	0234			
SREC	0124	0234	0234			
TAUS	0124	0234	0234			
TCLD	0124	0234	0234			
THIN	0124	0234	0234			
TIME	0124	0234	0234			

\*\*\*\*\*F O H T M A N C R C S S R E F E R E N C E L I S T I N G\*\*\*\*\*

SYMBOL INTERNAL STATEMENT NUMBERS

TORT	0224
TSUN	0224
WSON	0224
WTEF	0224
WTIN	0224
XPHI	0157
ALPH	0157
ARCJS	0157
ATAN2	0157
AVSCA	0157

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0120 0248 0253  
0255 0256 0257  
0257 0257 0259 0261

0118 0251 0252 0102 0430 0430 0485 0485 0494 0494 0495 0455  
0259 0392 0392  
0394 0396  
0399 0127 0130 0232 0232 0237 0244 0290 0327 0327 0336 0337

0415  
0266 0110 0116 0119 0120 0121 0121 0127 0128 0134 0152  
0314 0315 0380  
0278 0280 0285 0308 0321 0323 0360  
0358 0358 0481  
0421 0478 0482  
0282 0289

0432 0432  
0297 0450  
0478 0482  
0273 0275 0356  
0251 0455 0495 0501

0441 0443 0450 0452 0464  
0441 0441 0443 0450 0452 0464  
0445 0447 0454 0456 0468  
0445 0447 0456 0468  
0279 0172 0172 0234 0443 0443 0447  
0275 0291 0165 0270 0441 0445 0450 0376 0378  
0110 0148 0150 0352 0360 0363 0366

0160 0172 0174  
0276 0292 0165 0155 0443 0447 0452 0456 0464 0468  
0353  
0461

0244 0251 0261 0356 0392 0392 0392 0395 0395 0399 0399 0402 0402 0405 0405  
0358 0412 0418

0122 0241 0242 0294  
0381 0392 0464 0464 0468  
0411

0411  
0254 0257 0257 0273 0275 0321 0458  
0482 0482  
0482 0304 0304 0452 0452 0456

0259 0100 0104 0494 0495  
0214  
0385 0387 0387 0425 0429 0478  
0434

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\*\*\*\*\*F O R T R A N C I R C S S R E F E R E N C E L I S T I N G \*\*\*\*\*

INTERNAL STATEMENT NUMBERS

0250 0250  
0250 0250 0154 0154 0184  
0419  
0234 0340

SYMBOL

POINTN  
RELANC  
REFLUC  
REMTIM  
SAMPLE  
SEESUL  
SIGAIM



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\*\*\*\*\* F O R T M A N C R C S S R E F E R E N C E L I S T I N G \*\*\*\*\*

LABEL DEFINED REFERENCES

1	0004	0003
2	0004	0103
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100	0004	0207



[illegible][illegible]

VAR.	NAME	REL.	ADDR.	VAR.	NAME	TYPE	REL.	ADDR.	VAR.	NAME	TYPE	REL.	ADDR.
S11	M#4	N#4	N.F.	S12	R#4	R#4	N.R.	N.R.	S33	R#4	R#4	N.R.	N.R.
S14	M#4	M#4	N.F.	S44	R#4	R#4	N.R.	N.R.	X1	M#4	M#4	N.R.	N.R.
Y1	M#4	N.F.	N.F.	CDF	F#4	F#4	N.R.	N.R.					
								CJ6DEQ					

[illegible]

VAR.	NAME	TYPE	REL.	ADDR.	VAR.	NAME	TYPE	REL.	ADDR.	VAR.	NAME	TYPE	REL.	ADDR.
IMP	IMP	I*4	COCOC3		IMPJ	IMPJ	I*4	COCOC4		TAMSLN	TAMSLN	R*4	N.R.	
TSBK	TSBK	R*4	COCOC10		SOIH	SOIH	R*4			N.F.				

NAME OF COMMON BLOCK	*SPLIT*	SIZE OF BLOCK	CCCC004 HEXADECIMAL BYTES
COMMON BLOCK 1	1	100	00000000
COMMON BLOCK 2	2	200	00000000
COMMON BLOCK 3	3	300	00000000
COMMON BLOCK 4	4	400	00000000
COMMON BLOCK 5	5	500	00000000
COMMON BLOCK 6	6	600	00000000
COMMON BLOCK 7	7	700	00000000
COMMON BLOCK 8	8	800	00000000
COMMON BLOCK 9	9	900	00000000
COMMON BLOCK 10	10	1000	00000000
COMMON BLOCK 11	11	1100	00000000
COMMON BLOCK 12	12	1200	00000000
COMMON BLOCK 13	13	1300	00000000
COMMON BLOCK 14	14	1400	00000000
COMMON BLOCK 15	15	1500	00000000
COMMON BLOCK 16	16	1600	00000000
COMMON BLOCK 17	17	1700	00000000
COMMON BLOCK 18	18	1800	00000000
COMMON BLOCK 19	19	1900	00000000
COMMON BLOCK 20	20	2000	00000000
COMMON BLOCK 21	21	2100	00000000
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COMMON BLOCK 25	25	2500	00000000
COMMON BLOCK 26	26	2600	00000000
COMMON BLOCK 27	27	2700	00000000
COMMON BLOCK 28	28	2800	00000000
COMMON BLOCK 29	29	2900	00000000
COMMON BLOCK 30	30	3000	00000000
COMMON BLOCK 31	31	3100	00000000
COMMON BLOCK 32	32	3200	00000000
COMMON BLOCK 33	33	3300	00000000
COMMON BLOCK 34	34	3400	00000000
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COMMON BLOCK 36	36	3600	00000000
COMMON BLOCK 37	37	3700	00000000
COMMON BLOCK 38	38	3800	00000000
COMMON BLOCK 39	39	3900	00000000
COMMON BLOCK 40	40	4000	00000000
COMMON BLOCK 41	41	4100	00000000
COMMON BLOCK 42	42	4200	00000000
COMMON BLOCK 43	43	4300	00000000
COMMON BLOCK 44	44	4400	00000000
COMMON BLOCK 45	45	4500	00000000
COMMON BLOCK 46	46	4600	00000000
COMMON BLOCK 47	47	4700	00000000
COMMON BLOCK 48	48	4800	00000000
COMMON BLOCK 49	49	4900	00000000
COMMON BLOCK 50	50	5000	00000000
COMMON BLOCK 51	51	5100	00000000
COMMON BLOCK 52	52	5200	00000000
COMMON BLOCK 53	53	5300	00000000
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COMMON BLOCK 56	56	5600	00000000
COMMON BLOCK 57	57	5700	00000000
COMMON BLOCK 58	58	5800	00000000
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COMMON BLOCK 62	62	6200	00000000
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COMMON BLOCK 69	69	6900	00000000
COMMON BLOCK 70	70	7000	00000000
COMMON BLOCK 71	71	7100	00000000
COMMON BLOCK 72	72	7200	00000000
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COMMON BLOCK 74	74	7400	00000000
COMMON BLOCK 75	75	7500	00000000
COMMON BLOCK 76	76	7600	00000000
COMMON BLOCK 77	77	7700	00000000
COMMON BLOCK 78	78	7800	00000000
COMMON BLOCK 79	79	7900	00000000
COMMON BLOCK 80	80	8000	00000000
COMMON BLOCK 81	81	8100	00000000
COMMON BLOCK			

VAR.	NAME	TYPE	REL.	ADDR.	VAR.	NAME	TYPE	REL.	ADDR.	VAR.	NAME	TYPE	REL.	ADDR.
N.R.														
R#4														
TYPE														

NAME OF COMMON BLOCK *	TST*	SIZE OF BLOCK	000004 HEXADECIMAL BYTES

VAR. NAME	REL. ADDR.	VAR. NAME	REL. ADDR.	VAR. NAME	REL. ADDR.
TEST	000000				
I#4					

NAME--(F--COMMON--LOCK--\*--CTAB#--SIZE--IF--SLOCK-----COIEUCHEXADESIMAL--BYTES--

VAR.	NAME	REL.	ADDR.	VAR.	NAME	TYPE	REL.	ADDR.	VAR.	NAME	TYPE	REL.	ADDR.
VSAMP4	R#4	C0000		VSAMP5	R#4	C01C20							

NAME OF COMMON BLOCK	*SCROLL*	SIZE OF BLOCK	HEXADECIMAL BYTES
COMMON BLOCK	1	100	000004

[illegible][illegible][illegible]

NAME OF COMMON BLOCK	* * * * *	PHOT*	-----	SIZE	OF	BLOCK	HEXADECIMAL BYTES
				C0006C			

[illegible][illegible][illegible]

NLAYER	1*4	CC2000	TCR	R*4	N.F.	TURF	R*4	N.R.	TCL	R*4	CC0324
XH	R*4	CC0404	DX	R*4	N.F.						
NAME OF COMMON BLOCK * SEAT* SIZE OF BLOCK CC0020 HEXADECIMAL BYTES											
VAR. NAME	TYPE	REL. ADDR.	VAR. NAME	TYPE	REL. ADDR.	VAR. NAME	TYPE	REL. ADDR.	VAR. NAME	TYPE	REL. ADDR.
N	1*4	CC0000	INDIC	1*4	N.F.	JK	1*4	CC0018	IGND	1*4	CC001C
NAME OF COMMON BLOCK * PARAM* SIZE OF BLOCK CC0048 HEXADECIMAL BYTES											
VAR. NAME	TYPE	REL. ADDR.	VAR. NAME	TYPE	REL. ADDR.	VAR. NAME	TYPE	REL. ADDR.	VAR. NAME	TYPE	REL. ADDR.
INO	1*4	CC0000	NSCA	1*4	CC0004	NK	1*4	CC0008	NUMK	1*4	N.R.
KMAX	1*4	CC0030	IST	1*4	CC0034	WAV	R*4	CC0038	FACTOR	R*4	N.R.
NM	1*4	N.R.	NMAX	1*4	CC0044						
NAME OF COMMON BLOCK * ACC* SIZE OF BLOCK CC00CC HEXADECIMAL BYTES											
VAR. NAME	TYPE	REL. ADDR.	VAR. NAME	TYPE	REL. ADDR.	VAR. NAME	TYPE	REL. ADDR.	VAR. NAME	TYPE	REL. ADDR.
AC1	R*4	CC0000	AC2	R*4	CC0004	AC3	R*4	CC0008			
NAME OF COMMON BLOCK * GND* SIZE OF BLOCK CC0004 HEXADECIMAL BYTES											
VAR. NAME	TYPE	REL. ADDR.	VAR. NAME	TYPE	REL. ADDR.	VAR. NAME	TYPE	REL. ADDR.	VAR. NAME	TYPE	REL. ADDR.
NAL3	1*4	CC0000	ALB	R*4	CC0004	CG	R*4	CC000C			
NAME OF COMMON BLOCK * FIL* SIZE OF BLOCK CC0004 HEXADECIMAL BYTES											
VAR. NAME	TYPE	REL. ADDR.	VAR. NAME	TYPE	REL. ADDR.	VAR. NAME	TYPE	REL. ADDR.	VAR. NAME	TYPE	REL. ADDR.
ACEN	R*4	CC0000									
NAME OF COMMON BLOCK * *I* SIZE OF BLOCK CC0004 HEXADECIMAL BYTES											
VAR. NAME	TYPE	REL. ADDR.	VAR. NAME	TYPE	REL. ADDR.	VAR. NAME	TYPE	REL. ADDR.	VAR. NAME	TYPE	REL. ADDR.
EIGHT	R*4	CC0000									
NAME OF COMMON BLOCK * CLPAR* SIZE OF BLOCK CC0198 HEXADECIMAL BYTES											
VAR. NAME	TYPE	REL. ADDR.	VAR. NAME	TYPE	REL. ADDR.	VAR. NAME	TYPE	REL. ADDR.	VAR. NAME	TYPE	REL. ADDR.
NCL00	1*4	N.R.	NCL01	1*4	CC0004	CLOUD	R*4	CC0008			
NAME OF COMMON BLOCK * *UPDATE* SIZE OF BLOCK CC0030 HEXADECIMAL BYTES											
VAR. NAME	TYPE	REL. ADDR.	VAR. NAME	TYPE	REL. ADDR.	VAR. NAME	TYPE	REL. ADDR.	VAR. NAME	TYPE	REL. ADDR.
CC00	R*4	CC0000	CLC00	R*4	CC0018						
NAME OF COMMON BLOCK * CLDAT* SIZE OF BLOCK CC0078 HEXADECIMAL BYTES											
VAR. NAME	TYPE	REL. ADDR.	VAR. NAME	TYPE	REL. ADDR.	VAR. NAME	TYPE	REL. ADDR.	VAR. NAME	TYPE	REL. ADDR.
INC	1*4	CC0000	TULCLO	R*4	CC0008	ACLO	R*4	CC0050			
NAME OF COMMON BLOCK * RCVR* SIZE OF BLOCK CC005C HEXADECIMAL BYTES											
VAR. NAME	TYPE	REL. ADDR.	VAR. NAME	TYPE	REL. ADDR.	VAR. NAME	TYPE	REL. ADDR.	VAR. NAME	TYPE	REL. ADDR.
IRCLD	1*4	CC0000	IREC	1*4	CC0004	RECAFG	R*4	CC0008	CREC	R*4	CC000C
HL	R*4	N.R.	ALJ	R*4	N.R.	IFCI	1*4	CC0018	IFC2	1*4	CC001C
IFC3	1*4	CC0020	CLNK	R*4	CC0024	UNR	R*4	CC003C	VNR	R*4	CC0040
*N4	R*4	CC0044	FACTOR	R*4	CC0048	PCINTR	R*4	N.R.	CHT	R*4	CC0050
INFLX	1*4	CC0054	SZU	R*4	N.R.						
NAME OF COMMON BLOCK * CCNST* SIZE OF BLOCK CC0008 HEXADECIMAL BYTES											
VAR. NAME	TYPE	REL. ADDR.	VAR. NAME	TYPE	REL. ADDR.	VAR. NAME	TYPE	REL. ADDR.	VAR. NAME	TYPE	REL. ADDR.
PI	R*4	CC0000	TFI	R*4	CC0004						

NAME OF COMMON BLOCK \* INCUIT\* SIZE OF BLOCK 000008 HEXADECIMAL BYTES

VAR. NAME TYPE REL. ADDR. VAR. NAME TYPE REL. ADDR. VAR. NAME TYPE REL. ADDR. VAR. NAME TYPE REL. ADDR.

NAME OF COMMON BLOCK \*MAPCOM\* SIZE OF BLOCK 000008 HEXADECIMAL BYTES

VAR. NAME TYPE REL. ADDR. VAR. NAME TYPE REL. ADDR. VAR. NAME TYPE REL. ADDR. VAR. NAME TYPE REL. ADDR.

NAME OF COMMON BLOCK \*GNMHT\* SIZE OF BLOCK 000008 HEXADECIMAL BYTES

VAR. NAME TYPE REL. ADDR. VAR. NAME TYPE REL. ADDR. VAR. NAME TYPE REL. ADDR. VAR. NAME TYPE REL. ADDR.

NAME OF COMMON BLOCK \*GNMHT\* SIZE OF BLOCK 000008 HEXADECIMAL BYTES

VAR. NAME TYPE REL. ADDR. VAR. NAME TYPE REL. ADDR. VAR. NAME TYPE REL. ADDR. VAR. NAME TYPE REL. ADDR.

NAME OF COMMON BLOCK \*GNMHT\* SIZE OF BLOCK 000008 HEXADECIMAL BYTES

VAR. NAME TYPE REL. ADDR. VAR. NAME TYPE REL. ADDR. VAR. NAME TYPE REL. ADDR. VAR. NAME TYPE REL. ADDR.

NAME OF COMMON BLOCK \*GNMHT\* SIZE OF BLOCK 000008 HEXADECIMAL BYTES

VAR. NAME TYPE REL. ADDR. VAR. NAME TYPE REL. ADDR. VAR. NAME TYPE REL. ADDR. VAR. NAME TYPE REL. ADDR.

NAME OF COMMON BLOCK \*GNMHT\* SIZE OF BLOCK 000008 HEXADECIMAL BYTES

VAR. NAME TYPE REL. ADDR. VAR. NAME TYPE REL. ADDR. VAR. NAME TYPE REL. ADDR. VAR. NAME TYPE REL. ADDR.

NAME OF COMMON BLOCK \*GNMHT\* SIZE OF BLOCK 000008 HEXADECIMAL BYTES

VAR. NAME TYPE REL. ADDR. VAR. NAME TYPE REL. ADDR. VAR. NAME TYPE REL. ADDR. VAR. NAME TYPE REL. ADDR.

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14 CONTINUE
DO 151 ISUN=1,NSUL
  READ(5,1,7)SILT,SPHI
  SUE=SI(SILT*RAUCUN)
  CUE=SU(SILT*RAUCUN)
  SPE=SI(SPHI*RAUCUN)
  CPE=CU(SPHI*RAUCUN)
  SCLDIR(1,ISUN,1)=SUE*CP
  SCLDIR(1,ISUN,2)=SPE*SP
  SCLDIR(1,ISUN,3)=CUE
  CUE(1,ISUN)=SCLDIR(1,ISUN,1)
  CPE(1,ISUN)=SCLDIR(1,ISUN,2)
  CUE(1,ISUN)=SCLDIR(1,ISUN,3)
151 CONTINUE
200 IF(IMP*GE.1.AND.1ST.EC.CIGU TC 1005
  DO 1 KET,MAXX
    IF(INDIC(K).GE.5) GO TO 1
    IC=UNIT(K)
    IF(1C.GT.5) REWIND IC
    IF(K*EC.2.CRA1ST.EC.0) GO TO 201
  C HEAD IN COMPONENT SIZE DISTRIBUTION PARAMETERS
  C
  READ(5,10)NK(K),STEP(K),AI(K),EI(K),CI(K),ITAPE(K)
  NUNK(K)=(NK(K)-1)/2
  NUNENLAK(K)
  NENK(K)
  IF(K*GT.1.AND.INDIC(N).GE.5)GO TC 1111
  IF(INDIC(N).EQ.1.OR.INDIC(K).EC.2)STEP(K)=WAV/PI
  IF(DIST(K).EQ.1)DI(K)=(CI(K)-1.)+AI(K)*(BI(K)-1.)
  IF(DIST(K).EQ.3)DI(K)=AI(K)/SCRT(PI)
  IF(DIST(K).EC.4)DI(K)=(BI(K)-1.)/((EI(K)-1.)*(AI(K)-CI(K))+AI(K)
  )
  IF(DIST(K).NE.2)GO TC 2
  IT=1
  IT=(AI(K)+1.)/DI(K)+0.5
  DO J=1,3,11
    IT=IT*(1-1)
    OI(K)=CI(K)*EI(K)*11/PLCAT(11)
    DI(K)=CI(K)*2.*(AI(K)-1.)
    BI(K)=BI(K)*2.*(CI(K)-1)
    IF(INDIC(K)+1
  C SET UP EXTINCTION CROSS SECTIONS (CSECT), ABSORPTION CROSS
  C SECTIONS (ASCT), SCATTERING ANGLES (X), AND S11 FOR
  C ALLOWED TYPES OF SCATTERERS
  C GO TO(4,5,6,7,8),II
  C RAYLEIGH
  C
  4 CONTINUE
  CSECT(K)=AR*WAV**(-BR)
  ASCT(K)=C.
  XA=RAUCUN*100./PLCAT(N-1)
  DO 18 I=1,N
    X(K,I)=XA*PLCAT(1-1)
    CA=CU(X(K,I))
    S11(1,K)=C.75*(1.+CA*CA)
    GO TO 20
  18 S11(1,K)=C.75*(1.+CA*CA)
  1111 DO 1112 I=1,NLAYER
  1112 CDF(N,I)=CDF(N-1,I)
  GO TO 1
  C MUNCODIPERSE MIE
  C
  C
  5 NL=INT(AI(K)/STEP(K))+C.5)
  DO 5 I=1,NL
    READ(10,1)REFACT,ALPHA,CSCA,CCSEAR,CEXT
    MN(K)=REFACT
    DO 9 J=1,N
      READ(10,1)XA*RAUCUN
      X(K,J)=XA*RAUCUN
      S11(J,K,I)=S11(J,K)S12(J,K,I)
  9 CONTINUE
  S14(J,K,I)=-S34(J,K,I)
  D=WAV*ALPHA/PI
```

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WRITE(6.563)  
IF(IRPAT.NE.0)GO TO 130

WRITE(6.562)  
IF(IRSGO.EQ.0)\*WRITE(6.563)  
IF(IRLGO.EQ.1)\*WRITE(6.564)  
IF(IAP3(IRPAT).NE.1)GO TO 131

WRITE(6.565)XND  
LUCE=IRCUF\*(IRPAT+1)/2+1  
IF(LUCC=2)\*2

IF(ILUCC.EQ.ILUC)\*WRITE(6.566)  
IF(ILUCC.NE.ILUC)\*WRITE(6.567)  
\*WRITE(6.568)XND

IF(IRPAT.NE.0)GO TO 132  
\*WRITE(6.569)  
IF(IRSGO.EQ.0)\*WRITE(6.570)  
IF(IRLGO.EQ.1)\*WRITE(6.571)

IF(IRHGO.EQ.1)\*WRITE(6.572)  
\*WRITE(6.573)  
DO 132 IPRE1,NSPOT

WRITE(6.574)CNTRY(IPR),CNTRY(IPR),EDGEY(IPR)  
IF(IRLGO.EQ.0)XAND,IRSPOT,EG,0)GO TO 134  
WRITE(6.575)XAND,IRSPOT,EG,0)GO TO 134

IF(IWSIZE.NE.0)GO TO 134  
\*WRITE(6.576)XAND,IRSPOT,EG,0)GO TO 134  
CONTINUE

WRITE(6.577)XAND,IRSPOT,EG,0)GO TO 134  
DO 442 IALD=1,IALD  
\*WRITE(6.578)XAND,IRSPOT,EG,0)GO TO 134  
CONTINUE

CALL ALGDCU(MAL9,ALBPT)  
\*WRITE(6.579)XAND,IRSPOT,EG,0)GO TO 134  
CONTINUE

WRITE(6.580)  
IF(IRSGO.EQ.0)\*WRITE(6.581)  
IF(IRLGO.EQ.1)\*WRITE(6.582)  
IF(IAP3(IRPAT).NE.1)GO TO 131

WRITE(6.583)XND  
LUCE=IRCUF\*(IRPAT+1)/2+1  
IF(LUCC=2)\*2

IF(ILUCC.EQ.ILUC)\*WRITE(6.584)  
IF(ILUCC.NE.ILUC)\*WRITE(6.585)  
\*WRITE(6.586)XND

IF(IRPAT.NE.0)GO TO 132  
\*WRITE(6.587)  
IF(IRSGO.EQ.0)\*WRITE(6.588)  
IF(IRLGO.EQ.1)\*WRITE(6.589)

IF(IRHGO.EQ.1)\*WRITE(6.590)  
\*WRITE(6.591)  
DO 132 IPRE1,NSPOT

WRITE(6.592)CNTRY(IPR),CNTRY(IPR),EDGEY(IPR)  
IF(IRLGO.EQ.0)XAND,IRSPOT,EG,0)GO TO 134  
WRITE(6.593)XAND,IRSPOT,EG,0)GO TO 134

IF(IWSIZE.NE.0)GO TO 134  
\*WRITE(6.594)XAND,IRSPOT,EG,0)GO TO 134  
CONTINUE

WRITE(6.595)XAND,IRSPOT,EG,0)GO TO 134  
DO 442 IALD=1,IALD  
\*WRITE(6.596)XAND,IRSPOT,EG,0)GO TO 134  
CONTINUE

CALL ALGDCU(MAL9,ALBPT)  
\*WRITE(6.597)XAND,IRSPOT,EG,0)GO TO 134  
CONTINUE

WRITE(6.598)  
IF(IRSGO.EQ.0)\*WRITE(6.599)  
IF(IRLGO.EQ.1)\*WRITE(6.600)  
IF(IAP3(IRPAT).NE.1)GO TO 131

WRITE(6.601)XND  
LUCE=IRCUF\*(IRPAT+1)/2+1  
IF(LUCC=2)\*2

IF(ILUCC.EQ.ILUC)\*WRITE(6.602)  
IF(ILUCC.NE.ILUC)\*WRITE(6.603)  
\*WRITE(6.604)XND

WRITE(6.605)  
IF(IRPAT.NE.0)GO TO 130

WRITE(6.606)  
IF(IRSGO.EQ.0)\*WRITE(6.607)  
IF(IRLGO.EQ.1)\*WRITE(6.608)  
IF(IAP3(IRPAT).NE.1)GO TO 131

WRITE(6.609)XND  
LUCE=IRCUF\*(IRPAT+1)/2+1  
IF(LUCC=2)\*2

IF(ILUCC.EQ.ILUC)\*WRITE(6.610)  
IF(ILUCC.NE.ILUC)\*WRITE(6.611)  
\*WRITE(6.612)XND

IF(IRPAT.NE.0)GO TO 132  
\*WRITE(6.613)  
IF(IRSGO.EQ.0)\*WRITE(6.614)  
IF(IRLGO.EQ.1)\*WRITE(6.615)

IF(IRHGO.EQ.1)\*WRITE(6.616)  
\*WRITE(6.617)  
DO 132 IPRE1,NSPOT

WRITE(6.618)CNTRY(IPR),CNTRY(IPR),EDGEY(IPR)  
IF(IRLGO.EQ.0)XAND,IRSPOT,EG,0)GO TO 134  
WRITE(6.619)XAND,IRSPOT,EG,0)GO TO 134

IF(IWSIZE.NE.0)GO TO 134  
\*WRITE(6.620)XAND,IRSPOT,EG,0)GO TO 134  
CONTINUE

WRITE(6.621)XAND,IRSPOT,EG,0)GO TO 134  
DO 442 IALD=1,IALD  
\*WRITE(6.622)XAND,IRSPOT,EG,0)GO TO 134  
CONTINUE

CALL ALGDCU(MAL9,ALBPT)  
\*WRITE(6.623)XAND,IRSPOT,EG,0)GO TO 134  
CONTINUE

WRITE(6.624)  
IF(IRSGO.EQ.0)\*WRITE(6.625)  
IF(IRLGO.EQ.1)\*WRITE(6.626)  
IF(IAP3(IRPAT).NE.1)GO TO 131

WRITE(6.627)XND  
LUCE=IRCUF\*(IRPAT+1)/2+1  
IF(LUCC=2)\*2

IF(ILUCC.EQ.ILUC)\*WRITE(6.628)  
IF(ILUCC.NE.ILUC)\*WRITE(6.629)  
\*WRITE(6.630)XND

IF(IRPAT.NE.0)GO TO 132  
\*WRITE(6.631)  
IF(IRSGO.EQ.0)\*WRITE(6.632)  
IF(IRLGO.EQ.1)\*WRITE(6.633)

IF(IRHGO.EQ.1)\*WRITE(6.634)  
\*WRITE(6.635)  
DO 132 IPRE1,NSPOT

WRITE(6.636)CNTRY(IPR),CNTRY(IPR),EDGEY(IPR)  
IF(IRLGO.EQ.0)XAND,IRSPOT,EG,0)GO TO 134  
WRITE(6.637)XAND,IRSPOT,EG,0)GO TO 134

IF(IWSIZE.NE.0)GO TO 134  
\*WRITE(6.638)XAND,IRSPOT,EG,0)GO TO 134  
CONTINUE

WRITE(6.639)XAND,IRSPOT,EG,0)GO TO 134  
DO 442 IALD=1,IALD  
\*WRITE(6.640)XAND,IRSPOT,EG,0)GO TO 134  
CONTINUE

CALL ALGDCU(MAL9,ALBPT)  
\*WRITE(6.641)XAND,IRSPOT,EG,0)GO TO 134  
CONTINUE

WRITE(6.642)  
IF(IRSGO.EQ.0)\*WRITE(6.643)  
IF(IRLGO.EQ.1)\*WRITE(6.644)  
IF(IAP3(IRPAT).NE.1)GO TO 131

WRITE(6.645)XND  
LUCE=IRCUF\*(IRPAT+1)/2+1  
IF(LUCC=2)\*2

IF(ILUCC.EQ.ILUC)\*WRITE(6.646)  
IF(ILUCC.NE.ILUC)\*WRITE(6.647)  
\*WRITE(6.648)XND





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L I S T I N G \*\*\*\*\*

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0349	0358	0369	0379	0389	0399	0409	0419	0429	0439	0449	0459	0469	0479	0489	0499	0509	0519	0529	0539	0549	0559	0569	0579	0589	0599	0609	0619	0629	0639	0649	0659	0669	0679	0689	0699	0709	0719	0729	0739	0749	0759	0769	0779	0789	0799	0809	0819	0829	0839	0849	0859	0869	0879	0889	0899	0909	0919	0929	0939	0949	0959	0969	0979	0989	0999																																																																																																																																																																																																																																																																																																																																		
0172	0173	0174	0175	0176	0177	0178	0179	0180	0181	0182	0183	0184	0185	0186	0187	0188	0189	0190	0191	0192	0193	0194	0195	0196	0197	0198	0199	0200	0201	0202	0203	0204	0205	0206	0207	0208	0209	0210	0211	0212	0213	0214	0215	0216	0217	0218	0219	0220	0221	0222	0223	0224	0225	0226	0227	0228	0229	0230	0231	0232	0233	0234	0235	0236	0237	0238	0239	0240	0241	0242	0243	0244	0245	0246	0247	0248	0249	0250	0251	0252	0253	0254	0255	0256	0257	0258	0259	0260	0261	0262	0263	0264	0265	0266	0267	0268	0269	0270	0271	0272	0273	0274	0275	0276	0277	0278	0279	0280	0281	0282	0283	0284	0285	0286	0287	0288	0289	0290	0291	0292	0293	0294	0295	0296	0297	0298	0299	0300	0301	0302	0303	0304	0305	0306	0307	0308	0309	0310	0311	0312	0313	0314	0315	0316	0317	0318	0319	0320	0321	0322	0323	0324	0325	0326	0327	0328	0329	0330	0331	0332	0333	0334	0335	0336	0337	0338	0339	0340	0341	0342	0343	0344	0345	0346	0347	0348	0349	0350	0351	0352	0353	0354	0355	0356	0357	0358	0359	0360	0361	0362	0363	0364	0365	0366	0367	0368	0369	0370	0371	0372	0373	0374	0375	0376	0377	0378	0379	0380	0381	0382	0383	0384	0385	0386	0387	0388	0389	0390	0391	0392	0393	0394	0395	0396	0397	0398	0399	0400	0401	0402	0403	0404	0405	0406	0407	0408	0409	0410	0411	0412	0413	0414	0415	0416	0417	0418	0419	0420	0421	0422	0423	0424	0425	0426	0427	0428	0429	0430	0431	0432	0433	0434	0435	0436	0437	0438	0439	0440	0441	0442	0443	0444	0445	0446	0447	0448	0449	0450	0451	0452	0453	0454	0455	0456	0457	0458	0459	0460	0461	0462	0463	0464	0465	0466	0467	0468	0469	0470	0471	0472	0473	0474	0475	0476	0477	0478	0479	0480	0481	0482	0483	0484	0485	0486	0487	0488	0489	0490	0491	0492	0493	0494	0495	0496	0497	0498	0499	0500	0501	0502	0503	0504	0505	0506	0507	0508	0509	0510	0511	0512	0513	0514	0515	0516	0517	0518	0519	0520	0521	0522	0523	0524	0525	0526	0527	0528	0529	0530	0531	0532	0533	0534	0535	0536	0537	0538	0539	0540	0541	0542	0543	0544	0545	0546	0547	0548	0549	0550	0551	0552	0553	0554	0555	0556	0557	0558	0559

SYMBOL		INTERNAL STATEMENT NUMBERS														
WS	0313	0329	0355													
W1	0353	0354	0355													
W2	0353	0354	0355													
W3	0353	0354	0355													
XA	0270	0282	0293	0315	0316	0320	0327									
XH	0270	0282	0293	0406	0413	0418	0419	0422	0430	0432	0432	0444	0444	0447	0462	0466
X1	0311	0321	0345	0761												
Y1	0317	0321	0350	0363	0702											
Y2	0321	0337	0353	0353	0353											
ZX	0322	0337	0353	0353	0353											
ZY	0322	0337	0353	0353	0353											
AUS	0327															
ACL	0324															
ALU	0324															
BCL	0324															
CCL	0324															
CDL	0324															
CHI	0324															
CIN	0324															
COS	0324															
CZO	0324															
EXP	0324															
FFF	0324															
MCL	0324															
ICL	0324															
IPL	0324															
IMP	0324															
INC	0324															
IND	0324															
INT	0324															
IPR	0324															
IST	0324															
IST	0324															
MDD	0324															
NNK	0324															
NSP	0324															
NUM	0324															
PHI	0324															
RZA	0324															
SIN	0324															
SUM	0324															
S20	0324															
S11	0324															
S12	0324															
S22	0324															
S33	0324															
S34	0324															
S44	0324															
TEN	0324															
TOL	0324															
TOT	0324															
TPI	0324															
T41	0324															
UNR	0324															
VNR	0324															
VAV	0324															
WCO	0324															
WCI	0324															
WNG	0324															
WNR	0324															
XCL	0324															
XX2	0324															
XX3	0324															
XX4	0324															
YCL	0324															
ACLU	0324															
ADEF	0324															
ALUG	0324															
CINR	0324															
CNR5	0324															
CRUC	0324															
CX21	0324															
CX31	0324															
CX32	0324															



[illegible][illegible]

**PAGE 017**

\*\*\*\*\*  
TRANSCROSS REFERENCE LISTING\*\*\*\*\*

LAUEL	DEFINED	REFERENCES	C276	0334	0364
1	0366	0232			
2	0233	0254			
3	0235	0259			
4	0236	0264			
5	0237	0264			
6	0238	0264			
7	0239	0264			
8	0240	0264			
9	0241	0270			
10	0242	0270			
11	0243	0270			

LABEL	DEFINED	REFERENCES
301	0.242	6239
302	0.198	6191
400	0.267	6609
401	0.266	6637
402	0.265	6632
403	0.275	6635

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\*\*\*\*\*  
CROSS REFERENCE LISTING\*\*\*\*\*

LAJEL	DEFINED	REFERENCES
521	0755	C773
522	0757	C775
523	0756	C774







VAR.	NAME	TYPE	REL.	ADDR.	VAR.	NAME	TYPE	REL.	ADDR.	VAR.	NAME	TYPE	REL.	ADDR.
THEAT		R#4	000000											
NAME OF COMMON BLOCK * SUL# SIZE OF BLOCK 000E74 HEXADECIMAL BYTES														
VAR.	NAME	TYPE	REL.	ADDR.	VAR.	NAME	TYPE	REL.	ADDR.	VAR.	NAME	TYPE	REL.	ADDR.
NSCL		R#4	000000											
AS		R#4	000E38											
NAME OF COMMON BLOCK * PHOT# SIZE OF BLOCK 00006C HEXADECIMAL BYTES														
VAR.	NAME	TYPE	REL.	ADDR.	VAR.	NAME	TYPE	REL.	ADDR.	VAR.	NAME	TYPE	REL.	ADDR.
CIN		R#4	N.R.											
JJ		R#4	N.R.											
NAME OF COMMON BLOCK * ATM# SIZE OF BLOCK 0007D4 HEXADECIMAL BYTES														
VAR.	NAME	TYPE	REL.	ADDR.	VAR.	NAME	TYPE	REL.	ADDR.	VAR.	NAME	TYPE	REL.	ADDR.
NLAYER		R#4	000000											
XH		R#4	0004A4											
NAME OF COMMON BLOCK * SCAT# SIZE OF BLOCK 000020 HEXADECIMAL BYTES														
VAR.	NAME	TYPE	REL.	ADDR.	VAR.	NAME	TYPE	REL.	ADDR.	VAR.	NAME	TYPE	REL.	ADDR.
N		R#4	000000											
NAME OF COMMON BLOCK * PARAM# SIZE OF BLOCK 000048 HEXADECIMAL BYTES														
VAR.	NAME	TYPE	REL.	ADDR.	VAR.	NAME	TYPE	REL.	ADDR.	VAR.	NAME	TYPE	REL.	ADDR.
IND		R#4	000000											
MAX		R#4	00003C											
NM		R#4	N.R.											
NAME OF COMMON BLOCK * GND# SIZE OF BLOCK 0000D4 HEXADECIMAL BYTES														
VAR.	NAME	TYPE	REL.	ADDR.	VAR.	NAME	TYPE	REL.	ADDR.	VAR.	NAME	TYPE	REL.	ADDR.
NALJ		R#4	000000											
NAME OF COMMON BLOCK * CLPAR# SIZE OF BLOCK 000198 HEXADECIMAL BYTES														
VAR.	NAME	TYPE	REL.	ADDR.	VAR.	NAME	TYPE	REL.	ADDR.	VAR.	NAME	TYPE	REL.	ADDR.
NCLCUJ		R#4	000000											
NAME OF COMMON BLOCK * CLEAIN# SIZE OF BLOCK 000078 HEXADECIMAL BYTES														
VAR.	NAME	TYPE	REL.	ADDR.	VAR.	NAME	TYPE	REL.	ADDR.	VAR.	NAME	TYPE	REL.	ADDR.
INC		R#4	000000											
NAME OF COMMON BLOCK * CREAD# SIZE OF BLOCK 000140 HEXADECIMAL BYTES														
VAR.	NAME	TYPE	REL.	ADDR.	VAR.	NAME	TYPE	REL.	ADDR.	VAR.	NAME	TYPE	REL.	ADDR.
FCL		R#4	000000											
XCL		R#4	000000											
NAME OF COMMON BLOCK * RCVR# SIZE OF BLOCK 00005C HEXADECIMAL BYTES														
VAR.	NAME	TYPE	REL.	ADDR.	VAR.	NAME	TYPE	REL.	ADDR.	VAR.	NAME	TYPE	REL.	ADDR.
IRCLD		R#4	000000											
PR		R#4	000010											
IFCJ		R#4	000020											
WNR		R#4	000044											
JWELLY		R#4	N.R.											

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ORIGINAL PAGE IS  
OF POOR QUALITY

```

131 0007 IF (IPCCO.EQ.0) CALL LAPM1(CCLT,S,1)
134 0008 IF (IPCCO.NE.0) CALL GENSCA(CCLT,CIN,IRCOO,S,1)
135 0009 CALL GENSCA(SSIN,S,S,1)
136 0010 GO TO 31
137 0011 CONTINUE SCATTERING
138 0012 C RAYLEIGH SCATTERING
139 0013 C
140 0014 IF (INDIC(JK).NE.0) GO TO 2
141 0015 CUECUSAN
142 0016 C
143 0017 COMPUTE TRANSFORMED SCATT. MATRIX FOR RAYLEIGH SCATT.
144 0018 C
145 0019 CALL SCATRA(SSIN,S,CE,1)
146 0020 GO TO 32
147 0021 COMPUTE SCATTERING MATRIX ELEMENTS FOR OTHER TYPES OF SCATT.
148 0022 C
149 0023 2 CALL ELEMIS(BETA,S,1)
150 0024 C
151 0025 TRANSFORM SCATT. MATRIX
152 0026 C
153 0027 MIR SCATTERING
154 0028 IF (INDIC(JK).NE.0) CALL SCATMI(SSIN,SS,S,1)
155 0029 C
156 0030 OTHER TYPES OF SCATT.
157 0031 C
158 0032 IF (INDIC(JK).EQ.0) CALL GENSCA(SSIN,SS,S,1)
159 0033 C
160 0034 COMPUTE ATTENUATION ALONG PATH IC SUN
161 0035 FIRST, GET CRITICAL PATH LENGTH IC SUN
162 0036 C
163 0037 30 CONTINUE
164 0038 CALL SEFSOL(TAUS)
165 0039 IF (TAUS.GT.1E-07) TAUS=1E-07
166 0040 TAU=TAUS
167 0041 RP=EXP(-TAUS)
168 0042 FR=FR+RIGHT
169 0043 DO 3 L=1,4
170 0044 DC 3 L=L+1,4
171 0045 C
172 0046 SAMPLE
173 0047 C
174 0048 ST(L)=SS(L)
175 0049 ST(L)=ST(L)+FF(IALJ)
176 0050 VSAMP(L,I,IS,KK,IALJ)=VSAMP(L,I,IS,KK,IALJ)+FR*ST(L)/ADEN
177 0051 2 CONTINUE
178 0052 RETURN
179 0053 END

```

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\*\*\*\*\* LISTING \*\*\*\*\*

SYMBOL	INTERNAL STATEMENT NUMBERS	CRCS	REFERENCE	LISTING
I	0017	0034	0039	0039
L	0016	0034	0039	0039
N	0020	0081	0081	0082
S	0011	0056	0056	0057
A1	0047			
U1	0047			
CG	0012			
CI	0042			
FI	0072			
FR	0076	0082	0082	0082
IJ	0024	0026	0026	0026
IS	0020	0026	0026	0026
JJ	0010			
JK	0021	0067	0067	0067
KK	0022	0067	0067	0067
SS	0014	0067	0067	0067
ST	0047	0081	0081	0082
UN	0010			
UN	0010			
VN	0010			
VS	0010			
WN	0010			
WS	0010			
ALB	0010	0026	0026	0026
CIN	0010	0026	0026	0026
EXP	0020	0020	0020	0020
ICL	0020	0020	0020	0020
IJP	0020	0020	0020	0020

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L-I-S-T-I-N-G \*\*\*\*\*

**M. J. N. M.**

# CRAN CRCS

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SIZE OF PROGRAM CCC945 HEXADECIMAL BYTES PAGE 005

**SAMPLE /**

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111

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•

[illegible]



14.3







ISND KEEPS TRACK OF THE TYPE OF BOUNDARY LIKELY TO BE ENCOUNTERED  
 = 0 BOUNDARY OF AMBIANT ATMOSPHERE  
 = +1 ENTERING CLOUD FROM AMBIANT ATMOSPHERE  
 = -1 EXACT BOUNDARY FOR EXITING CLOUD  
 = -2 APPROXIMATE BOUND FOR EXITING CLOUD

ISN 0042 GU TO 40  
 ISN 0043 32 CONTINUE

WE CANNOT ENTER A CLOUD ALONG THIS DIRECTION

QUICK LOOK (LSPECIALLY FOR THIN ATMOSPHERES )

ISN 0044 IF((CIN(6)\*GT(J).AND.(PT\*GE.(TCRT(INLAYER)-TCRT(JJ)+TCR(JJ))  
 /CIN(6)))GC TO 40  
 ISN 0045 PATH=CIN(3)/CIN(6)  
 ISN 0046 IF((CIN(6)\*LT(J).AND.(-PT\*LE.(TCRT(JJ)/CIN(6))))GC TO 46  
 ISN 0047 PATH=C.  
 ISN 0048 PTHX=1500.  
 ISN 0049 IEND=C  
 ISN 0050 GU TO 40

20 CONTINUE  
 TOLD=TCLOUD(INCLD)  
 DU 22 I=16

22 CLOUD(I)=CIN(I)

WE ARE IN A CLOUD SPECIFIED BY INCLD

HOW FAR MUST WE GO TO GET OUT

ASSUME WE WILL NOT GET OUT OF CLOUD AND CORRECT LATER

PTMX=2.\*CLOUD(INCLD.9)

ISN 0057

PAGE 002

ISN 0058 IEND=-2  
 ISN 0059 21 CONTINUE  
 ISN 0060 GNDHT=CLOUD(INCLD.3)  
 ISN 0061 PTHX=INLAYER)-CLOUD(INCLD.3)  
 ISN 0062 40 CONTINUE  
 ISN 0063 PTH=C.

IS PHUTEN-GGING-UP OR DOWN

IF(CIN(6)\*GE.0.)GC TO 4

PHUTEN IS GOING DOWN

HTCIN(3)+GNDHT

TEND=-PT/CIN(6)

PTMX=ANIN(TCND,PTMX)

IF(PTMX\*ES.IG(J))JEND=0

EPS=EPS+PTMX

HOW TRACK DOWNWARDS UNTILL WE GET TO FT OR PTHX.

WHICHEVER COMES FIRST

WE=CIN(6)

XLC=0.

IF(JJ\*AG.1)XLC=XH(JJ-1)

OPTH=CIN(3)+GNDHT-XLC/

DPTDPT\*(TCL(JJ)+TCL)

J=J

IF(DPT\*GE.1)GC TO 44

IF((DPT\*EPS).GE.PTHX)GC TO 45

IF((J\*ES.1)GC TO 55

PTDPT=PT

J=J-1

DC 43 I=1, JJM

JEJM=J+1

DPTDPT\*(TCL(J)+TCLD)

IF(DPT\*GE.1)GC TO 44

IF((DPT\*EPS).GE.PTHX)GC TO 45

PTDPT=PT

J=J-1

PTDPT=PT

43 CONTINUE

ORIGINAL PAGE IS  
 OF POOR QUALITY

IF WE GET TO THIS POINT WE HAVE MADE AN ERROR

ISN 0059  
ISN 0103

GO TO 55  
44 CONTINUE

WE HAVE USED UP ALL OF OUR PT

ISN 0101  
ISN 0103  
ISN 0104  
ISN 0105  
ISN 0107  
ISN 0109  
ISN 0109

IF (DPT.LE.2.) GO TO 55  
PATH=PTH+PT/CPI\*DPH  
PATH=MIN1(PATH,PTHMA)  
IF (PATH.NE.PTHMA) GO TO 441  
GO TO 45  
441 CONTINUE  
PT=0.

UPDATE ALONG PATH

ISN 0111  
ISN 0111

GO TO 50  
45 CONTINUE

WE HAVE COME TO A BOUNDARY

ISN 0112  
ISN 0113  
ISN 0113  
ISN 0115  
ISN 0116

DPH=(PTHX-FTH)  
DPT=DPH\*(TCL(J)+TCLD)  
DPT=DPH  
PATH=PTH+DPH  
IF (DND.EG.0) GO TO 46  
THE BOUNDARY IS A CLOUD

IS BOUNDARY APPROXIMATE-- IF SC. UPDATE AND BACKTRACK

ISN 0118

IF (DND.EG.-2) GO TO 50

UPDATE THE PHOTON

ISN 0120  
ISN 0121  
ISN 0122  
ISN 0123

DC 47 JI=1.5  
47 JIN(JI)=CIN(JI)+PTHX\*CIN(JI+3)  
DC 471 JI=1.5  
J=J

PAGE 003

ORIGINAL PAGE IS  
OF POOR QUALITY

ISN 0124

IF (CIN(3).LT.XH(NLAYER)) GO TO 472

ISN 0126  
ISN 0127  
ISN 0128

471 CONTINUE  
472 JJ=J  
IF (BND.GT.0) GO TO 48

COMING OUT OF THE CLOUD

ISN 0130  
ISN 0131  
ISN 0132  
ISN 0133

DC 49 IJ=1.6  
49 CLOUD(IJ)=CIN(IJ)  
INCL=1  
CALL TRANS(INCLC,INCLC)

DC 499 IJ=1.6

ISN 0135  
ISN 0136  
ISN 0137

499 CIN(IJ)=CLOUD(IJ)  
CALL TRANS2(CN,VN,WN,CN,VN,WN,INCLC,INCLC)  
INCL=0

CONTINUE TRACKING

ISN 0138  
ISN 0139

GO TO 10  
45 CONTINUE

GOING INTO THE CLOUD  
CHANGE COORDINATE SYSTEMS

ISN 0140  
ISN 0141  
ISN 0142  
ISN 0143

DC 486 IJ=1.6  
488 CLOUD(IJ)=CIN(IJ)  
INCL=1  
CALL TRANS(ENT,INCLC)

DC 489 IJ=1.6

ISN 0144  
ISN 0145  
ISN 0146  
ISN 0147

489 CIN(IJ)=CLOUD(IJ)  
INCL=ENT  
CALL TRANS2(CN,VN,WN,CN,VN,WN,INCLC,INCLC)

CONTINUE TRACKING

ISN 0148  
ISN 0149

GO TO 10  
4 CONTINUE

PHOTON GOING UP OR HORIZONTALLY

ORIGINAL PAGE IS  
OF POOR QUALITY

PAGE 004

PHOTON TRAVELS HORIZONTALLY

```
ISN 0192 J=JJ
ISN 0193 PTH=0
ISN 0194 PT=PT
ISN 0195 PATH=PT/(TCL(JJ)+TCLD)
ISN 0196 PTEG
ISN 0197 IF(PATH*LE*PTHX)GU TO 50
ISN 0198 PT=PTS
ISN 0199 GU TO 45
ISN 0200 401 CONTINUE
C
C PHOTON GOING UP
C
ISN 0201 TTUPE=(TPRT-CIN(3))/CIN(6)
ISN 0202 PTHX=AMIN(TTOP,PTHX)
ISN 0203 IF(PTHX*EQ*TTOP)INDC=0
ISN 0204 PTH=0
ISN 0205 OPTHE=(X(JJ)-(CIN(3)+ENDHT))/CIN(6)
ISN 0206 DPT=DPHT*(TCL(JJ)+TCLD)
ISN 0207 J=JJ
ISN 0208 IF(DPT*GE*PT)GU TO 44
ISN 0209 EP=EP+PTHX
ISN 0210 IF((OPTHE*PS)*GE*PTHX)GC TC 45
ISN 0211 PT=PT-CP1
ISN 0212 PTH=DPHT
ISN 0213 IF(JJ*EG*NEAYER)GU TO 55
ISN 0214 JJ=JJ+1
ISN 0215 DC 402 JL=JJP,NLAYER
ISN 0216 J=JL
ISN 0217 OPTHEUX(J)/CIN(6)
ISN 0218 DPT=DPHT*(TCL(JJ)+TCLD)
ISN 0219 IF(DPT*GE*PT)GU TO 44
ISN 0220 IF((OPTHEUX*PS)*GE*PTHX)GC TC 45
ISN 0221 PT=PT-CP1
ISN 0222 PTH=DPHT
ISN 0223 402 CONTINUE
C
```

IF WE REACH THIS POINT WE HAVE EFREC

```
ISN 0191 GU TO 55
ISN 0192 46 CONTINUE
C
ISN 0193 BOUNDARY WHICH IS NOT A CLOUD BOUNDARY
ISN 0194 IF(CIN(6)*GT*0)GU TO 461
ISN 0195 DC 463 J=1,2
ISN 0196 463 CIN(IJ)=CIN(IJ)+PATH*CIN(IJ+3)
ISN 0197 JJ=1
C
```

GROUND BOUNDARY

```
ISN 0194 ISCAT=1
ISN 0195 IF(INCLD*EQ*0)GU TO 462
C
```

IN A CLOUD

```
ISN 0201 DU 464 J=1,6
ISN 0202 464 CLCRO(IJ)=CIN(IJ)
ISN 0203 INCL=1
ISN 0204 CALL TRANS(INCLD,INDC)
ISN 0205 CG(1)=CGHC(1)
ISN 0206 CG(2)=CGHC(2)
ISN 0207 RETURN
ISN 0208 462 CONTINUE
ISN 0209 CG(1)=CIN(1)
ISN 0210 CG(2)=CIN(2)
ISN 0211 RETURN
ISN 0212 461 CONTINUE
C
```

PHOTON EXITS ATMOSPHERE

```
ISN 0213 IOUT=1
ISN 0214 IF(ITEST*EQ*0)GU TO 810
ISN 0215 WRITE(8,811)ICUT,PT,PTH,PATH,PTHX,PTH*PTHX,INCLD,JJ
ISN 0216 WRITE(6,812)(CIN(IPT),IPT=1,6)
ISN 0217 811 FORMAT(10G,2X,'IOUT=',I2,'PT=',E14.6,'PTH=',E14.7,'PATH=',E14.7,
ISN 0218
```

**PAGE 005**

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ORIGINAL PAGE IS  
OF POOR QUALITY

```

C  CONTINUE-TRACKING
C
C  GU TO 10
C  S2 CONTINUE
C
C  UPDATE CU-ORD VECTOR ALONG PATH
C
C  DC 51 IJ=1,3
C  51- CINC(IJ)CINC(IJ)+PATH*CINC(IJ+3)
C  JJ=J
C  IF(IJTEST.EQ.CJCC TO 9C6
C  WRITE(6,9C7)INCLD.PATH.(CINC(IJ),IJP=1,6)
C  EC7 FURMAT(1H,'FCSTRACK INCLD=',I2.4X,'PATH=',E14.7/1H,'CINC=',6I2X,
C  'E14.7)
C  EC6 CONTINUE
C
C  55- CONTINUE
C  WRITE(6,9C8)INCLD.IJ.(CINC(IJ),IJP=1,6).FT
C  551 FURMAT(1H,'12C(1M,*)1PC.14HTRACKING ERRCH/
C  '1M3.6HINCLD:12.2A,2HJ=,13.2X,3FJ=,13/
C  '1PC.4HCIN=,6(E14.7,2X)/
C  '1PC.3HET=,E14.7)
C  WRITE(6,9C9)FTM.PTHMX.IEND.PTI
C  552 FURMAT(1H,'PTM=,E14.7,4X,'PTHMX=',E14.7,4X,'IEND=',I2/
C  '1M3.6HINCLD:12.2A,2HJ=,13.2X,3FJ=,13/
C  '1PC.4HCIN=,6(E14.7,2X)/
C  '1PC.3HET=,E14.7)
C  RETURN
C  END
  
```

PAGE 006

\*\*\*\*\* C R T R A N C R C S R E F E R E N C E L I S T I N G \*\*\*\*\*

SYMBGL	INTERAL	STATEMENT	NUMBERS	C R C S	R E F E R E N C E	L I S T I N G	PAGE 006
J	0000	0000	0000	0000	0000	0000	0000
J	0001	0001	0001	0001	0001	0001	0001
W	0002	0002	0002	0002	0002	0002	0002
AS	0003	0003	0003	0003	0003	0003	0003
CG	0004	0004	0004	0004	0004	0004	0004
DX	0005	0005	0005	0005	0005	0005	0005
MT	0006	0006	0006	0006	0006	0006	0006
IJ	0007	0007	0007	0007	0007	0007	0007
IX	0008	0008	0008	0008	0008	0008	0008
IY	0009	0009	0009	0009	0009	0009	0009
JI	0010	0010	0010	0010	0010	0010	0010
JJ	0011	0011	0011	0011	0011	0011	0011
JL	0012	0012	0012	0012	0012	0012	0012
PT	0013	0013	0013	0013	0013	0013	0013
UN	0014	0014	0014	0014	0014	0014	0014
VN	0015	0015	0015	0015	0015	0015	0015
WN	0016	0016	0016	0016	0016	0016	0016
XH	0017	0017	0017	0017	0017	0017	0017
AX	0018	0018	0018	0018	0018	0018	0018
AD5	0019	0019	0019	0019	0019	0019	0019
ALB	0020	0020	0020	0020	0020	0020	0020
CIN	0021	0021	0021	0021	0021	0021	0021
DPT	0022	0022	0022	0022	0022	0022	0022
EPS	0023	0023	0023	0023	0023	0023	0023
IJP	0024	0024	0024	0024	0024	0024	0024
IJ3	0025	0025	0025	0025	0025	0025	0025
INC	0026	0026	0026	0026	0026	0026	0026
JJM	0027	0027	0027	0027	0027	0027	0027
JJP	0028	0028	0028	0028	0028	0028	0028
PTH	0029	0029	0029	0029	0029	0029	0029
PTI	0030	0030	0030	0030	0030	0030	0030
PTS	0031	0031	0031	0031	0031	0031	0031
PTT	0032	0032	0032	0032	0032	0032	0032





ORIGINAL PAGE IS  
OF POOR QUALITY

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\*\*\*\*\*--CCNMCN--INFORMATION--\*\*\*\*\*

VAR.	NAME	TYPE	REL.	ADDR.	VAR.	NAME	TYPE	REL.	ADDR.
TEST	1#4	CCCCC							

[illegible]



SYMBOL	INTERNAL STATEMENT NUMBER	CC07	CC07	CC07	CC07	CC08	CC09	CC10	CC10	CC11	CC11	CC12
1	0000	0000	0000	0007	0007	0007	0007	0010	0010	0011	0011	CC12
INDC	0001	0000	0000	0007	0007	0007	0007	0010	0010	0011	0011	CC12
CLCLOD	0002	0000	0000	0007	0007	0007	0007	0010	0010	0011	0011	CC12
CLCLOD	0003	0000	0000	0007	0007	0007	0007	0010	0010	0011	0011	CC12
CLCLOD	0004	0000	0000	0007	0007	0007	0007	0010	0010	0011	0011	CC12
NCLCJ1	0005	0000	0000	0007	0007	0007	0007	0010	0010	0011	0011	CC12
CLCLOD	0006	0000	0000	0007	0007	0007	0007	0010	0010	0011	0011	CC12
CLCLOD	0007	0000	0000	0007	0007	0007	0007	0010	0010	0011	0011	CC12
CLCLOD	0008	0000	0000	0007	0007	0007	0007	0010	0010	0011	0011	CC12
CLCLOD	0009	0000	0000	0007	0007	0007	0007	0010	0010	0011	0011	CC12
CLCLOD	0010	0000	0000	0007	0007	0007	0007	0010	0010	0011	0011	CC12
CLCLOD	0011	0000	0000	0007	0007	0007	0007	0010	0010	0011	0011	CC12
CLCLOD	0012	0000	0000	0007	0007	0007	0007	0010	0010	0011	0011	CC12
CLCLOD	0013	0000	0000	0007	0007	0007	0007	0010	0010	0011	0011	CC12
CLCLOD	0014	0000	0000	0007	0007	0007	0007	0010	0010	0011	0011	CC12
CLCLOD	0015	0000	0000	0007	0007	0007	0007	0010	0010	0011	0011	CC12
CLCLOD	0016	0000	0000	0007	0007	0007	0007	0010	0010	0011	0011	CC12
CLCLOD	0017	0000	0000	0007	0007	0007	0007	0010	0010	0011	0011	CC12
CLCLOD	0018	0000	0000	0007	0007	0007	0007	0010	0010	0011	0011	CC12
CLCLOD	0019	0000	0000	0007	0007	0007	0007	0010	0010	0011	0011	CC12
CLCLOD	0020	0000	0000	0007	0007	0007	0007	0010	0010	0011	0011	CC12
CLCLOD	0021	0000	0000	0007	0007	0007	0007	0010	0010	0011	0011	CC12
CLCLOD	0022	0000	0000	0007	0007	0007	0007	0010	0010	0011	0011	CC12
CLCLOD	0023	0000	0000	0007	0007	0007	0007	0010	0010	0011	0011	CC12
CLCLOD	0024	0000	0000	0007	0007	0007	0007	0010	0010	0011	0011	CC12
CLCLOD	0025	0000	0000	0007	0007	0007	0007	0010	0010	0011	0011	CC12
CLCLOD	0026	0000	0000	0007	0007	0007	0007	0010	0010	0011	0011	CC12
CLCLOD	0027	0000	0000	0007	0007	0007	0007	0010	0010	0011	0011	CC12
CLCLOD	0028	0000	0000	0007	0007	0007	0007	0010	0010	0011	0011	CC12
CLCLOD	00											

LABEL	DEFINED	REFERENCES	CROSS	REFERENCE	LISTING	PAGE
1	0000	0000	0000	0000	0000	003
2	0000	0000	0000	0000	0000	003

TRANSL- SIZE CF PROGRAM 000102--HEXADECIMAL-BYTES-PAGE-004

[illegible]

\*\*\*\*\*  
CENTRAL INFORMATION

NAME OF COMMON BLOCK \*CLPAR\* SIZE OF BLOCK CC0198 HEXADECIMAL EYES

VAR.	NAME	TYPE	REL.	ADDR.	VAR.	NAME	TYPE	REL.	ADDR.	VAR.	NAME	TYPE	REL.	ADDR.
NCLCUU	I*4		N.R.		NCLCU	I*4	N.R.			CLCUD	R*4	QC008		

[illegible]

VAR.	NAME	TYPE	REL.	ADDR.	VAR.	NAME	TYPE	REL.	ADDR.
CCCC	M#4	CCCC			CCCC	M#4	CCCC		
					CCCC	M#4	CCCC		

LABEL	ADDR	LABEL	ADDR	LABEL	ADDR	PAGE	DOCS
1	C000CE	2	C0012E				

\*\*\*\*\* NAME=... MAIN:OPT=02,LINECNT=92,SIZE=COCK, \*\*\*\*\*

\*CPFLUNS IN EFFECT# .... SOURCE,EECDIC,NOLIST,NUDECK,LC/0,NAP,NUECIT,IC,XREF.

```
#STATISTIC# SOURCE STATEMENTS = 13 ,PFCGRAM SIZE = 466
```

#STATISTICS# :NU DIAGNOSTICS GENERATED

```
***** END OF COMPILE *****
```

LEVEL 21.6 (JEC 72) CS/360 FCETRAN H DATE 76.320/21.06.53

```

      COMPILER=OPTIONS=NAME=MAIN,CFT=2,LINECNT=32,SIZE=0000K,
      SOURCE=EUCLID,NLIST,NCCCHK,LAD,MAP,NCE0IT,IC,XREF
      SUBROUTINE TRANS,X1,X2,X3,X,Y,Z,I,INC)

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TRANS2 CONVERTS DIRECTION COSINE VECTORS

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C
C      INDC=-1  CONVERTS X,Y,Z TO CLUC(1) COORDINATES
C      +1      CONVERTS X,Y,Z TO GENERAL FROM CIRCULAR
C      INDC=0  CONVERTS DIRECTOR COSINE VECTORS
C      INDC=2  CONVERTS ORIENTATION COSINE VECTORS

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154 0003 \_\_\_\_\_ COMMON/CLFAN/NCLJUD.ACLCL+CLCUC(10,10) \_\_\_\_\_

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FACT=+1.

154 CODE \_\_\_\_\_ IF (INDC.LT.0) FACT=-1.

$Cf = CL(0,0)(1,7)$

[illegible]

$x_1 = \lambda x + C7 - YV4(\delta$

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SYMBOL INTERNAL STATEMENT NUMBERS  
 I 0002 0010 0011  
 X 0002 0004  
 Y 0002 0005  
 Z 0002 0005  
 C7 0010 0012  
 C8 0011 0012  
 X1 0004 0012  
 X2 0002 0012  
 X3 0002 0014  
 Y1 0005 0012  
 Y2 0005 0014  
 FACT 0007 0008  
 INCC 0002 0008  
 CLOUD 0002 0010  
 NCCLOD 0002 0002  
 TRANS2 0002 0002

TRANS2 / SIZE OF PROGRAM 000103 HEXADECIMAL BYTES PAGE 003

NAME	TAG	TYPE	ADD.	NAME	TAG	TYPE	ADD.	NAME	TAG	TYPE	ADD.
C7 SF	R#4	R#4	0000A4	XX SF	Y	F	0000A4	XX SF	Y	F	0000A4
A2 SF	R#4	R#4	0000A4	YY SF	Y	F	0000A4	YY SF	Y	F	0000A4
FACT SF	R#4	R#4	0000A4	INCC	Y	F	0000A4	INCC	Y	F	0000A4
NCCLOD	C	I#4	N#R.	TRANS2	R#4	R#4	0000C8	TRANS2	R#4	R#4	0000C8

\*\*\*\*\* COMMON INFORMATION \*\*\*\*\*

NAME OF COMMON BLOCK \* CLP#\* SIZE OF BLOCK 000198 HEXADECIMAL BYTES

VAR. NAME TYPE REL. ADDR. VAR. NAME TYPE REL. ADDR. VAR. NAME TYPE REL. ADDR.  
 NCCLOD I#4 N#R. NCCLOD R#4 C00008

\*OPTIONS IN EFFECT\* NAME MAINOPT=02,LINECNT=02,SIZE=0000K.

\*OPTIONS-IN-EFFECT\* SOURCE=000000,NOCT=0,NODECK,LCAD,MAP,NCEdit,IO,XREF

\*STATISTICS\* SOURCE STATEMENTS = 15 .PROGRAM SIZE = 480

\*STATISTICS\* NO DIAGNOSTICS GENERATED

\*\*\*\*\* END OF COMPILATION \*\*\*\*\*

101K BYTES OF CORE NOT USED

LEVEL 21.0 (DEC 72)

CS/360 FCRTAN H

DATE 76-324/21.47.01

COMPILER OPTIONS - NAME MAIN,CPT=02,LINECNT=02,SIZE=0000K.

SOURCE=000000,NOCT=0,NODECK,LCAD,MAP,NCEdit,IO,XREF

SURPOLINE CLOUD(1,NOCT,C01STEXT)

DIMENSION C(2)

CLAMPON/CLP#NCCLOD,NCCLOD,CLC000(16,10)

CLAMPON/CLP#NCCLOD,NCCLOD,CLC000(16,10)

NCUT=0

CLC000(1)=0.

CLC000(1)=0.

IF (CLC000(K+3))1,0,2

1 FACT=1.

GO TO 3

2 FACT=1.

3 CONTINUE

K2=MOD(K,3)+1

K3=MOD(K+1,3)+1

K4=K2+3

K5=K3+3

C(K)=FACT\*CLC000(1,3+K)

C(K2)=CLC000(K2)+C(K)-CLC000(K2+3)/CLC000(K2+3)

C(K3)=CLC000(K3)+C(K)-CLC000(K3+3)/CLC000(K3+3)

IF (ABS(C(K2))>LE.CLOUD(1,K4).AND.(ABS(C(K3))>LE.CLOUD(1,K5)))GO TO 7

6 CONTINUE

7 RETURN

7 EXT(1,1)=C(1)



LEVEL 21.6 (DEC 72)

CS/360 FORTRAN H

DATE 76-324/21.47.09

COMPILER OPTIONS -

NAME= MAIN,CPI=02,LINECNT=62,SIZE=0000K,  
SOURCE=CLCUDC,NCLIST,NLCCCK,LCCAD,WAF,NCCDIT,IC,XREF

SUBROUTINE CLNP

DIMENSION THETAC(10),ZCL(10)

COMMON/CLPAR/NCLCUD,NCLC1,CLCUD(10,10)

COMMON/CLCUD/INC(10),TCLCUD(10),ACLE(10)

COMMON/CHRAD/RC(10),AC(10),EC(10),CC(10),XCL(10),YCL(10),ZCL(10)

\*TPOC(10),CLEN(10)

COMMON/CCNST/PI,PI

READ(5,1) NCLCUD

IF(NCLCUD.EQ.7)THETURN

READ(5,2)(HC(K),AC(K),JC(K),CC(K),XCL(K),YCL(K),THETAC(K),INC(K),

CLCUD(K),KE1,NCLCUD)

\*NCLCUD

\*WHERE

AC(N),YCL(K) ARE X AND Y COORDINATES OF THE CENTER

OF MASS OF THE CLOUD

HC(K) = ALTITUDE OF LOWER SURFACE OF K TH CLOUD

IN KILOMETERS.

AC(K),YCL(K),CC(K) = DIMENSIONS OF THE K TH CLOUD IN

THE X,Y, AND Z DIRECTIONS OF THE CLOUD COORDINATE

SYSTEM.

THETAC(K) = ANGLE BETWEEN THE X-AXIS OF THE CLOUD-AND

THAT OF THE GENERAL COORDINATE SYSTEM

(MEASURED CLOCKWISE IN DEGREES LOOKING UP

FROM THE GROUND)

INC(K) = INDICATION OF THE ATMOSPHERIC

CONSTITUTION APPROPRIATE TO THIS CLOUD.

FORMAT(12)

1 2 FORMAT(F5.5,F8.3,F8.5,13.E5.3)

PI=3.14159

RAUCN=PI/180.

DC 5 I=1,NCLCUD

TPOC(I)=THETAC(I)

THETAC(I)=THETAC(I)\*RADCCN

5 CONTINUE

DC 3 I=1,NCLCUD

DC 3 J=1,10

CLCUD(I,J)=0.

3 FORMING CLOUD (I,J) ARRAY

DC 4 I=1,NCLCUD

CLCUD(I,4)=AC(I)\*0.5

CLCUD(I,5)=HC(I)\*0.5

CLCUD(I,6)=CC(I)\*0.5

CLCUD(I,7)=XCL(I)

CLCUD(I,8)=YCL(I)

CLCUD(I,9)=HC(I)+CLCUD(I,6)

ZCL(I)=CLCUD(I,9)

CLCUD(I,10)=THETAC(I)

CLCUD(I,11)=SIN(THETAC(I))

CLCUD(I,12)=COS(THETAC(I))

\*CLCUD(I,6)

4 CLCUD(I,9)=SQRT(CLCCUD(I,10))

CLCUD(I,11)

10 SPECIFICATION PARAMETERS FOR EACH OF UP TO

10 CLOUDS

CLCUD POINTER

XMC,YMC,ZMC COORDINATES OF CENTER OF MASS OF

THE CLOUD

A,B,C THE HALF-DIMENSIONS OF EACH SIDE OF THE

CLOUD

US(THETAC),SIN(THETAC) WHERE THETAC IS THE

ORIENTATION OF THE CLOUD

R, RADIUS OF THE CIRCUMSCRIBING SPHERE AROUND

THE CLOUD

R\*\*2 SQUARE OF THE RADIUS(PARAMETER J=9)

SIX VECTOR POSITION OF THE PHOTON AT LAST

SCATTERING IN GENERAL SPACE

SIX VECTOR POSITION OF THE PHOTON AT LAST

SCATTERING IN CLOUD SYSTEM UNDER CONSIDERATION

SIX VECTOR POSITION OF NEW SCATTERING POINT

IN THE LAST SYSTEM (CLOUD OR GENERAL)

COORDINATE SYSTEM INDICATOR

C GENERAL SYSTEM

1 THRU 10 CLOUD SYSTEM

X-XC,Y-YC,Z-ZC COMPLETED FOR 1 TH CLOUD

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ISN C319  
ISN C340  
ISN C341

95 CONTINUE  
RETURN  
END

PAGE 002

\*\*\*\*\*F C R T R A N C R C S S R E F E R E N C E L I S T I N G\*\*\*\*\*

INTERNAL STATEMENT NUMBERS

J 0011 0013 0013 0014 0014 0018 0019 0020 0021 0024 0025 0028 0037

K 0027 0028 0033 0037

AS 0014 0020 0021 0028 0028

JJ 0012 0020 0021 0028 0028

KK 0016 0036

PC 0018 0019

PS 0015 0020

UN 0015 0020

VN 0015 0020

WN 0015 0020

CIN 0015 0020

JCM 0015 0020

NM 0015 0020

PCL 0015 0020

PATH 0015 0020

SCUT 0015 0020

SOAT 0015 0020

CLOUD 0015 0020

COORD 0015 0020

INCLD 0015 0020

NCLD1 0015 0020

CLETR 0015 0020

CLCROD 0015 0020

CLCROD 0015 0020

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PAGE 003

\*\*\*\*\*F C R T R A N C R C S S R E F E R E N C E L I S T I N G\*\*\*\*\*

LABEL DEFINED REFERENCES

0 0010 0011 0016 0018 0018 0021 0025 0031

7 0027

8 0019

9 0028

10 0034

99 0035

/ CLETR / SIZE OF PROGRAM 0003AE HEXADECIMAL BYTES PAGE 004

NAME	I-SF	TAG	TYPE	ADD.	NAME	J-SF	TAG	TYPE	ADD.	NAME	K-SF	TAG	TYPE	ADD.	NAME	AS-S	TAG	TYPE	ADD.
JJ	C	I*	R*	N.R.	KK	SF	C	R*	N.R.	PC	SF	C	R*	N.R.	PC	SF	C	R*	N.R.
UN	C	I*	R*	N.R.	VN	SF	C	R*	N.R.	PC	SF	C	R*	N.R.	PC	SF	C	R*	N.R.
CCM	SF	C	R*	0000B4	NM	SF	C	R*	0000B3	CCRO	SF	C	R*	0000B3	CCRO	SF	C	R*	0000B3
SCUT	C	I*	R*	N.R.	CLCROD	F	C	R*	N.R.	CLCROD	F	C	R*	N.R.	CLCROD	F	C	R*	N.R.
NCLD1	C	I*	R*	N.R.	SURT	SF	C	R*	N.R.	CLCROD	F	C	R*	N.R.	CLCROD	F	C	R*	N.R.
ENTER	SF	XR	I*	0000C0	NCLJUD	F	C	I*	0000C0	NENTER	SF	C	I*	0000C8	NENTER	SF	C	I*	0000C8

\*\*\*\*\*COMMON INFORMATION\*\*\*\*\*

NAME OF COMMON BLOCK \*CLPAR\* SIZE OF BLOCK 000198 HEXADECIMAL BYTES

VAR. NAME	TYPE	REL. ADDR.	VAR. ADDR.	VAR. NAME	TYPE	REL. ADDR.	VAR. ADDR.
NCLCROD	I*	0000C0	0000C0	NCLD1	I*	N.R.	N.R.

NAME OF COMMON BLOCK \*URENTE\* SIZE OF BLOCK 000030 HEXADECIMAL BYTES

VAR. NAME	TYPE	REL. ADDR.	VAR. ADDR.	VAR. NAME	TYPE	REL. ADDR.	VAR. ADDR.
CLCROD	R*	0000C0	0000C0	CLCROD	R*	N.R.	N.R.

NAME OF COMMON BLOCK \*PHUT\* SIZE OF BLOCK 00006C HEXADECIMAL BYTES

VAR. NAME	TYPE	REL. ADDR.	VAR. ADDR.	VAR. NAME	TYPE	REL. ADDR.	VAR. ADDR.
CIN	R*	N.R.	N.R.	UN	R*	N.R.	N.R.
JJ	I*	N.R.	N.R.	SCUT	R*	N.R.	N.R.

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NAME	TAG	TYPE	ADD.	NAME	TAG	TYPE	ADD.	NAME	TAG	TYPE	ADD.
I SFA	I	SFA	000093	K SF	K	SF	00009C	JK SF	JK	SF	000CA0
ENT SFA	X	X	000000	NAM SF	NAM	SF	0000AB	DIST SFA	XR	R	0000C0
INDC SFA	X	X	0000AC	PLANE SF	PLANE	SF	0000C0	SDIST		R	0000B4
JENIEH F	X	X	0000CC	NLINTER SF	NLINTER	SF	000090	NPLANE SFA	SFA	I	0000BC

LABEL - ADDR LABEL ADDR LABEL ADDR LABEL ADDR PAGE-005

NAME= MAIN,OPT=C2,LINECNT=82,SIZE=C500K,  
\*OPTIONS IN EFFECT#

\*OPTIONS IN EFFECT\* SOURCE, E, ECUIC, NULIST, NODECK, LCAD, MAP, NCEDIT, ID, XREF

~~\*STAT-151-K-54~~ ~~SOURCE-STATEMENTS-~~ ~~26~~ ~~PROGRAM-SIZE-~~ ~~718~~

\*STATISTICS# NJ DIAGNOSTICS GENERATED

\*\*\*\*\* END CF COMPILATION \*\*\*\*\*

181K BYTES OF CORE NOT USED

LEVEL 21.6 (DEC 72) CS/36C FCSTRAN H DATE 76.324/21.47.34

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CCMPILER CPTIONS - NAME= MAIN,CFT=J2,LINECNT=92,SIZE=9000X,

```

SUPERUTINE PLANE(I,INDC ,ENT,NFLANE,CIST)

CONSTRUCTING A PLANE OF THE CLOUD AND DETERMINES THE DISTANCE THROUGH A PLANE OF THE CLOUD AND DETERMINES THE DISTANCE

TO THE POINT OF ENTRY (ENT(I,J)) FROM THE LAST POSITION

PLANSIGN-C(3)-ENT(10-3)-DISK(10)

COMMON/CLFAN/KCT000.KCT001.CTCTCFC(6)  
COMMON/CLFAN/KCT000.KCT001.CTCTCFC(6)  
COMMON/CLFAN/KCT000.KCT001.CTCTCFC(6)

--- NPLANE = 0  
CALL TEANS(1,1,300)

\_\_\_\_\_  $\chi^2 = 1.0$

```
IF (ABS(CLCORG(K)).LE.CLCUG(1.3+K)) GC=10.6
IF (CLCORG(K).LT.CLCUG(1.3+K)) FACT=-1
```

$$1 + (CUCCH(K) + G) \cdot CUCCH(1 - g + K)) \cdot FAC(1 - g + K)$$

$$C(K) \equiv FAC(1 - g + K) \cdot CUCCH(1 - g + K)$$
$$y = C(x)$$

```
IF (CLOC(K)-U)*CLOC(K)>.GT.0.) CL IC 6
IF (CLOC(K)+K).EQ.0.) GO TO 6
```

$$K^2 = \lambda_0(\kappa, \varepsilon) + 1$$
$$X(C_{\mathbb{R}}^0(X)) = X(C_{\mathbb{R}}^0(X) + 1, \mathbb{R}) + 1$$
$$N = 2 \times 10^6$$

```

K3=K2+1
IF (AUB(C(K2)) .LE. CLOUD*(1,K4) .AND. AES(C(K2)) .LE. CLOUD (1,K5)) GO

```

ITC /  
CONTINENTAL

2000

PLANET = 1  
LAT(1,1) = C(11)

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DIST(I)=(ENT(I,1))-CLC

• (1) 11

7.4  
55

\*\*\*\*\*C H I R A N C H C S S R E F E R E N C E L I S T I N G \*\*\*\*\*

SYMBOL INVENT

U.S. DEPARTMENT OF AGRICULTURE

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OF POOR QUALITY

K5	0026	0027
ADS	0027	0027
ENT	0028	0028
MUD	0029	0029
DIS1	0030	0030
FACT	0031	0031
INCC	0032	0032
SORT	0033	0033
CLOUD	0034	0034
CUGU	0035	0035
NCLDI	0036	0036
PLANE	0037	0037
TRANS	0038	0038
CLCJRD	0039	0039
NPLANE	0040	0040

[illegible]

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PLANE 1

[illegible]

\*\*\*\*\*  
 C-CH-4-1-CONFIDENTIAL  
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ORIGINAL PAGE'S  
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NAME	OF COMMON BLOCK	*CLPAR*	SIZE OF BLOCK	CC0198 HEXADECIMAL EYTES
...	...	...	...	...

VAR.	NAME	TYPE	REL.	ADDR.	VAR.	NAME	TYPE	REL.	ADDR.	VAR.	NAME	TYPE	REL.	ADDR.
NCLCUD	1#4		N.H.		NCLC1	1#4	N.F.			CLCUD	R#4			C00008

NAME OF COMMON BLOCK	*UPONTE*	SIZE OF BLOCK	COO30	HEXADECIMAL	BYTES
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WAR.	NAME	TYPE	REL.	ADDR.	VAR.	NAME	TYPE	REL.	ADDR.	VAR.	NAME	TYPE	REL.	ADDR.
CCCCD	R#4		N.F.		CLCCRD	R#4		CCCCD						

LABEL	ADDR	LABEL	ADDR	LABEL	ADDR	PAGE 005
6	CC02C2	7	CC02EE			

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*OPTIONS IN EFFECT #103#
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\*OPTIONS IN EFFECT\* SOURCE,ECODIC,NOLIST,NUDECK,LCAD,MAP,NCEDIT,ID,XFREE.

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*STATISTICS*
SOURCE STATEMENTS = 37 ,PROGRAM SIZE = 1042
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# \*STATISTICS\* NU CLIASTICS GENERATED

\*\*\*\*\* END OF COMPILATION \*\*\*\*\*

LEVEL 21.6 (JEG 72) CS/16C FCRTAN H DATE 76.324/21.47.47

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-----C-MPILE-OPTIONS -- NAME= MAIN,CFT=02,LINECNT=62,SIZE=000K,
SOURCE,EOC)IC,NLLIST,NCCCK,LCAD,MAP,NCEUIT,IC,XREF
ISN C002
ISN C003
ISN C004
SUBROUTINE TRANS (ICORD,INCO)
COMMON/CLPAR/NCLOUD,NCLC1,CLEUD(10,10)
COMMON/CFRONT/CFURD(0),CLECRD(6)

```

1-1	CLOUD
C	IF INDC= POSITIVE CONVERSION TO CLOUD COORDINATE
C	COORDINATE SYSTEM TO GENERAL SYSTEM TAKES PLACE.
C	IF INDC= NEGATIVE---CONVERSION TO CLOUD COORDINATE
C	SYSTEM FROM GENERAL GENERAL COORDINATE SYSTEM TAKES PLACE.
1	IF(INDC)1,1,2
1	CLCROD(1)=CLOC(1)+CLOC(1)*CLOC(1)/7+(CLOC(2)-CLOC(1)
ISN C006	
ISN C107	







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**PAGE 005**

5 000102

• 321E=3215 •

- C/D, MAP, NCEDIT, IC, XREF

SIZE = 932

TICS... GENERATED...

END OF COMPIATION \*\*\*\*\*

CATE 76.324/21.48.22

11-3715-28-1N23N17.

CE CR, LEAD, MAF, NCEDII, IC, XREF,  
#2, CY2, CZ2, CX, CY, CZ)

1770. 1771. 1772. 1773. 1774. 1775. 1776. 1777. 1778. 1779. 1780. 1781. 1782. 1783. 1784. 1785. 1786. 1787. 1788. 1789. 1790. 1791. 1792. 1793. 1794. 1795. 1796. 1797. 1798. 1799. 1800. 1801. 1802. 1803. 1804. 1805. 1806. 1807. 1808. 1809. 1810. 1811. 1812. 1813. 1814. 1815. 1816. 1817. 1818. 1819. 1820. 1821. 1822. 1823. 1824. 1825. 1826. 1827. 1828. 1829. 1830. 1831. 1832. 1833. 1834. 1835. 1836. 1837. 1838. 1839. 1840. 1841. 1842. 1843. 1844. 1845. 1846. 1847. 1848. 1849. 1850. 1851. 1852. 1853. 1854. 1855. 1856. 1857. 1858. 1859. 1860. 1861. 1862. 1863. 1864. 1865. 1866. 1867. 1868. 1869. 1870. 1871. 1872. 1873. 1874. 1875. 1876. 1877. 1878. 1879. 1880. 1881. 1882. 1883. 1884. 1885. 1886. 1887. 1888. 1889. 1890. 1891. 1892. 1893. 1894. 1895. 1896. 1897. 1898. 1899. 1900. 1901. 1902. 1903. 1904. 1905. 1906. 1907. 1908. 1909. 1910. 1911. 1912. 1913. 1914. 1915. 1916. 1917. 1918. 1919. 1920. 1921. 1922. 1923. 1924. 1925. 1926. 1927. 1928. 1929. 1930. 1931. 1932. 1933. 1934. 1935. 1936. 1937. 1938. 1939. 1940. 1941. 1942. 1943. 1944. 1945. 1946. 1947. 1948. 1949. 1950. 1951. 1952. 1953. 1954. 1955. 1956. 1957. 1958. 1959. 1960. 1961. 1962. 1963. 1964. 1965. 1966. 1967. 1968. 1969. 1970. 1971. 1972. 1973. 1974. 1975. 1976. 1977. 1978. 1979. 1980. 1981. 1982. 1983. 1984. 1985. 1986. 1987. 1988. 1989. 1990. 1991. 1992. 1993. 1994. 1995. 1996. 1997. 1998. 1999. 2000. 2001. 2002. 2003. 2004. 2005. 2006. 2007. 2008. 2009. 2010. 2011. 2012. 2013. 2014. 2015. 2016. 2017. 2018. 2019. 2020. 2021. 2022. 2023. 2024. 2025. 2026. 2027. 2028. 2029. 2030. 2031. 2032. 2033. 2034. 2035. 2036. 2037. 2038. 2039. 2040. 2041. 2042. 2043. 2044. 2045. 2046. 2047. 2048. 2049. 2050. 2051. 2052. 2053. 2054. 2055. 2056. 2057. 2058. 2059. 2060. 2061. 2062. 2063. 2064. 2065. 2066. 2067. 2068. 2069. 2070. 2071. 2072. 2073. 2074. 2075. 2076. 2077. 2078. 2079. 2080. 2081. 2082. 2083. 2084. 2085. 2086. 2087. 2088. 2089. 2090. 2091. 2092. 2093. 2094. 2095. 2096. 2097. 2098. 2099. 2100. 2101. 2102. 2103. 2104. 2105. 2106. 2107. 2108. 2109. 2110. 2111. 2112. 2113. 2114. 2115. 2116. 2117. 2118. 2119. 2120. 2121. 2122. 2123. 2124. 2125. 2126. 2127. 2128. 2129. 2130. 2131. 2132. 2133. 2134. 2135. 2136. 2137. 2138. 2139. 2140. 2141. 2142. 2143. 2144. 2145. 2146. 2147. 2148. 2149. 2150. 2151. 2152. 2153. 2154. 2155. 2156. 2157. 2158. 2159. 2160. 2161. 2162. 2163. 2164. 2165. 2166. 2167. 2168. 2169. 2170. 2171. 2172. 2173. 2174. 2175. 2176. 2177. 2178. 2179. 2180. 2181. 2182. 2183. 2184. 2185. 2186. 2187. 2188. 2189. 2190. 2191. 2192. 2193. 2194. 2195. 2196. 2197. 2198. 2199. 2200. 2201. 2202. 2203. 2204. 2205. 2206. 2207. 2208. 2209. 2210. 2211. 2212. 2213. 2214. 2215. 2216. 2217. 2218. 2219. 2220. 2221. 2222. 2223. 2224. 2225. 2226. 2227. 2228. 2229. 2230. 2231. 2232. 2233. 2234. 2235. 2236. 2237. 2238. 2239. 2240. 2241. 2242. 2243. 2244. 2245. 2246. 2247. 2248. 2249. 2250. 2251. 2252. 2253. 2254. 2255. 2256. 2257. 2258. 2259. 2260. 2261. 2262. 2263. 2264. 2265. 2266. 2267. 2268. 2269. 2270. 2271. 2272. 2273. 2274. 2275. 2276. 2277. 2278. 2279. 2280. 2281. 2282. 2283. 2284. 2285. 2286. 2287. 2288. 2289. 2290. 2291. 2292. 2293. 2294. 2295. 2296. 2297. 2298. 2299. 2300. 2301. 2302. 2303. 2304. 2305. 2306. 2307. 2308. 2309. 2310. 2311. 2312. 2313. 2314. 2315. 2316. 2317. 2318. 2319. 2320. 2321. 2322. 2323. 2324. 2325. 2326. 2327. 2328. 2329. 2330. 2331. 2332. 2333. 2334. 2335. 2336. 2337. 2338. 2339. 2340. 2341. 2342. 2343. 2344. 2345. 2346. 2347. 2348. 2349. 2350. 2351. 2352. 2353. 2354. 2355. 2356. 2357. 2358. 2359. 2360. 2361. 2362. 2363. 2364. 2365. 2366. 2367. 2368. 2369. 2370. 2371. 2372. 2373. 2374. 2375. 2376. 2377. 2378. 2379. 2380. 2381. 2382. 2383. 2384. 2385. 2386. 2387. 2388. 2389. 2390. 2391. 2392. 2393. 2394. 2395. 2396. 2397. 2398. 2399. 2400. 2401. 2402. 2403. 2404. 2405. 2406. 2407. 2408. 2409. 2410. 2411. 2412. 2413. 2414. 2415. 2416. 2417. 2418. 2419. 2420. 2421. 2422. 2423. 2424. 2425. 2426. 2427. 2428. 2429. 2430. 2431. 2432. 2433. 2434. 2435. 2436. 2437. 2438. 2439. 2440. 2441. 2442. 2443. 2444. 2445. 2446. 2447. 2448. 2449. 2450. 2451. 24

THE DIRECTION CCINES OF THE  
2 DIRECTIONS.

U=C Y 1 \* C 2 2 - C 2 1 \* C Y 2  
V=C 2 1 \* C X 2 - C X 1 \* C 2 2  
W=C X 1 \* C Y 2 - C X 2 \* C Y 1  
T=3 5 4 2 T ( 4 4 4 - V \* V \* W \* W )

T T T Z  
 \ \ \ X  
 U V W U  
 = = = T D  
 X Y Z U Z  
 U U U X E

~~PAGE 002~~

## STRENGTHS

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1

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ကုမ္ပဏီ  
လီမိတက်  
ပတ်ဝန်းကျင်  
လီမိတက်

500

4060

NAME / SIZE OF PROGRAM 0001E6 HEXADECIMAL BYTES PAGE 003

| NAME | TAG | TYPE | ADD.   |
|------|-----|------|--------|
| CPI  | F   | R#4  | 000084 |
| CPI  | F   | R#4  | 000094 |
| CPI  | F   | R#4  | 0000A4 |

3215

CAC.MAP-NCEDIT.ID-X-SEE

5176 - 5364

TYPE GENERATED



LEVEL 21.6 (DEC 72)

CS/360 FORTRAN M

DATE 76.324/21.48.31

```

COMPILER OPTIONS - NAME= MAIN,CFT=02,LINECNT=92,SIZE=0000K,
SOURCE=EDC01C,NLIST=INDECK,LCAO,WAP,NCEdit,IC,XREF
SUBROUTINE JIM(CUT,CIN,CP,SP,CZ,SB)
C**
C** SUBROUTINE JIM
C**
DIMENSION CCLT(4)
DIMENSION GIN(4)

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C*****
C** THIS SUBROUTINE IS THE FCAL FCINT OF THE PROGRAM. IT COMPUTES
C** THE DIRECTION COSINES AFTER SCATTERING GIVEN THE DIRECTION
C** CLINES BEFORE SCATTERING. THE SCATTERING ANGLE AND THE AZIMUTH
C** REFERENCE TO THE MERIDIAN.
C*****

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13N C035 CX=GIN(4)
13N C036 CY=GIN(5)
13N C037 CZ=GIN(6)
13N C038 CCLT(1)=CIN(1)
13N C039 CCLT(2)=CIN(2)
13N C040 CCLT(3)=CIN(3)
13N C041 IF(CX*EC*0.0AND.CY*EU*0) GO TO 10
13N C042 PHIEATANE(CY,CX)
13N C043 GO TO 11
13N C044 10 PHIEC.
13N C045 11 SINPHI=SIN(PHI)
13N C046 COSPHI=COS(PHI)
13N C047 CNECA*CA+CY*CY
13N C048 CU=CU+CU*CU
13N C049 SINPHI=SGRT(CN/CO)
13N C050 DT=5*CP
13N C051 DP=5*4SF
13N C052 UCST*CU
13N C053 CX = CU*CX-BF*SINPHI+BC*CUSEPHI
13N C054 CY = CU*CY+BF*CUSEPHI+BC*SINPHI
13N C055 CZ = CU*CZ
13N C056 CONTINUE
13N C057 CCLT(4)=CX
13N C058 CCLT(5)=CY
13N C059 CCLT(6)=CZ
13N C060 RETURN
13N C061 END
13N C062

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168

ORIGINAL PAGE IS  
OF POOR QUALITY

PAGE 002

\*\*\*\*\*F C R T H A N C R C S S R E F E R E N C E L I S T I N C\*\*\*\*\*

| SYMBOL | INTERNAL STATEMENT NUMBERS         |
|--------|------------------------------------|
| BC     | C024 C025                          |
| BP     | C024 C025                          |
| CB     | C021 C026                          |
| CD     | C020 C026                          |
| CP     | C016 C019                          |
| CX     | C013 C018 C024 C028                |
| CY     | C013 C018 C025 C029                |
| CZ     | C019 C023 C026 C030                |
| SA     | C021 C022                          |
| SP     | C022 C024                          |
| CIN    | C006 C007 C008 C009 C010           |
| COS    | C017                               |
| JIM    | C015 C016 C017                     |
| PHI    | C013                               |
| SIN    | C003 C008 C009 C010 C028 C029 C030 |
| SGRT   | C010                               |
| ATAJ2  | C015                               |
| COSPHI | C017 C024 C025                     |
| SINPHI | C017 C024 C025                     |
| SINPHI | C026                               |

LABEL DEFINED REFERENCES  
1 0012  
10 0016  
11 0018

NAME TAG TYPE ADD. NAME TAG TYPE ADD. NAME TAG TYPE ADD. NAME TAG TYPE ADD.  
10 0012A 11 0012A 1 000254 NR  
\*OPTIONS IN EFFECT\* NAME= MAIN,OPT=02,LINECNT=02,SIZE=000000.  
\*OPTIONS IN EFFECT\* SOURCE=EBODIC,NOLIST,NODECK,LCAD,MAP,NCEDIT,IO,XREF  
\*STATISTICS\* SOURCE=STATISTICS= 41,PROGRAM=SIZE= 736  
\*STATISTICS\* NO DIAGNOSTICS GENERATED  
\*\*\*\*\* END OF COMPILATION \*\*\*\*\*  
LEVEL 21.6 (DEC 72) CS/300 FCRTNAN H DATE 76.324/21.48.40  
177K BYTES OF CORE NOT USED

LABEL ADDR LABEL ADDR LABEL ADDR LABEL ADDR LABEL ADDR LABEL ADDR LABEL ADDR LABEL ADDR LABEL ADDR LABEL ADDR  
10 0012A 11 0012A 1 000254 NR

NAME TAG TYPE ADD. NAME TAG TYPE ADD. NAME TAG TYPE ADD. NAME TAG TYPE ADD.  
10 0012A 11 0012A 1 000254 NR  
\*OPTIONS IN EFFECT\* NAME= MAIN,OPT=02,LINECNT=02,SIZE=000000.  
\*OPTIONS IN EFFECT\* SOURCE=EBODIC,NOLIST,NODECK,LCAD,MAP,NCEDIT,IO,XREF  
\*STATISTICS\* SOURCE=STATISTICS= 41,PROGRAM=SIZE= 736  
\*STATISTICS\* NO DIAGNOSTICS GENERATED  
\*\*\*\*\* END OF COMPILATION \*\*\*\*\*  
LEVEL 21.6 (DEC 72) CS/300 FCRTNAN H DATE 76.324/21.48.40  
177K BYTES OF CORE NOT USED

NAME TAG TYPE ADD. NAME TAG TYPE ADD. NAME TAG TYPE ADD. NAME TAG TYPE ADD.  
10 0012A 11 0012A 1 000254 NR  
\*OPTIONS IN EFFECT\* NAME= MAIN,OPT=02,LINECNT=02,SIZE=000000.  
\*OPTIONS IN EFFECT\* SOURCE=EBODIC,NOLIST,NODECK,LCAD,MAP,NCEDIT,IO,XREF  
\*STATISTICS\* SOURCE=STATISTICS= 41,PROGRAM=SIZE= 736  
\*STATISTICS\* NO DIAGNOSTICS GENERATED  
\*\*\*\*\* END OF COMPILATION \*\*\*\*\*  
LEVEL 21.6 (DEC 72) CS/300 FCRTNAN H DATE 76.324/21.48.40  
177K BYTES OF CORE NOT USED

NAME TAG TYPE ADD. NAME TAG TYPE ADD. NAME TAG TYPE ADD. NAME TAG TYPE ADD.  
10 0012A 11 0012A 1 000254 NR  
\*OPTIONS IN EFFECT\* NAME= MAIN,OPT=02,LINECNT=02,SIZE=000000.  
\*OPTIONS IN EFFECT\* SOURCE=EBODIC,NOLIST,NODECK,LCAD,MAP,NCEDIT,IO,XREF  
\*STATISTICS\* SOURCE=STATISTICS= 41,PROGRAM=SIZE= 736  
\*STATISTICS\* NO DIAGNOSTICS GENERATED  
\*\*\*\*\* END OF COMPILATION \*\*\*\*\*  
LEVEL 21.6 (DEC 72) CS/300 FCRTNAN H DATE 76.324/21.48.40  
177K BYTES OF CORE NOT USED

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OF POOR QUALITY

NAME TAG TYPE ADD. NAME TAG TYPE ADD. NAME TAG TYPE ADD. NAME TAG TYPE ADD.  
10 0012A 11 0012A 1 000254 NR  
\*OPTIONS IN EFFECT\* NAME= MAIN,OPT=02,LINECNT=02,SIZE=000000.  
\*OPTIONS IN EFFECT\* SOURCE=EBODIC,NOLIST,NODECK,LCAD,MAP,NCEDIT,IO,XREF  
\*STATISTICS\* SOURCE=STATISTICS= 41,PROGRAM=SIZE= 736  
\*STATISTICS\* NO DIAGNOSTICS GENERATED  
\*\*\*\*\* END OF COMPILATION \*\*\*\*\*  
LEVEL 21.6 (DEC 72) CS/300 FCRTNAN H DATE 76.324/21.48.40  
177K BYTES OF CORE NOT USED

LABEL DEFINED REFERENCES  
1 C002  
2 C003

XSECTM / SIZE OF PROGRAM C002C6 HEXADECIMAL BYTES PAGE 004

| NAME | S | TAG | TYPE   | ADD. | NAME | TAG | TYPE   | ADD. | NAME | TAG | TYPE   | ADD. |
|------|---|-----|--------|------|------|-----|--------|------|------|-----|--------|------|
| PHI  | F | R*  | 000000 |      | PHI  | F   | 000000 |      | PHI  | F   | 000000 |      |
| PHI  | F | R*  | 000000 |      | PHI  | F   | 000000 |      | PHI  | F   | 000000 |      |
| PHI  | F | R*  | 000000 |      | PHI  | F   | 000000 |      | PHI  | F   | 000000 |      |

LABEL ADDR LABEL ADDR LABEL ADDR PAGE-005

1 C00130 2 000102

\*OPTIONS IN EFFECT\* NAME= MAIN,OPT=02,LINECNT=92,SIZE=0000K.

\*OPTIONS IN EFFECT\* SOURCE=ERCDIC,NULIST,NODECK,LCPD,MAP,NCECIT,IO,XREF

\*STATISTICS\* SOURCE STATEMENTS= 26-PROGRAM SIZE= 710

\*STATISTICS\* NO DIAGNOSTICS GENERATED

\*\*\*\*\* END OF COMPILATION \*\*\*\*\*

181K BYTES OF CORE NOT USED

LEVEL 21.6 (DEC 72)

CS/360 FORTRAN M

DATE 76.324/21.48.49

COMPILER OPTIONS - NAME= MAIN,OPT=02,LINECNT=92,SIZE=0000K.

SOURCE=ERCDIC,NULIST,NODECK,LCPD,MAP,NCECIT,IO,XREF

SLEP ROUTINE ANGLE(M,ETA,XX)

170

C\*\* SUBROUTINE ANGLE M

C\*\*  
C\*\*  
C\*\*  
C  
C THIS SUBROUTINE PERFORMS A TABLE LOOK-UP FOR THE  
C SCATTERING ANGLE GIVEN A RECTANGULARLY DISTRIBUTED NUMBER  
C BETWEEN 0 AND 1  
C

154 C003 DIMENSION XI(5,100),YI(5,100)  
154 C004 DIMENSION S11(100,5),S12(100,5,2), S22(100,5,2), S32(100,5,2)

154 C005 1 S32(100,5,2), S44(100,5,2)

154 C006 DIMENSION X(5,100)

154 C007 DIMENSION CDF (5,100)

154 C008 COMMON S11, S12, S22, S33, S34, S44, X, XI, YI, CDF

154 C009 COMMON/PARAM/IND,NDCALNKA(S),NUNK(S),NMAX,IST,WAV,FACTOR,NM

154 C010 1,NMAX

154 C011 COMMON/SCAT/N,INDIC(S),JK,IGNC

154 C012 COMMON/CCNST/PI,TPI

154 C013 NUNENUNK(JK)

154 C014 DO 1 I=1,NM

154 C015 IF (XX,LE,YI(M,1)) GO TO 2

154 C016 1 CONTINUE

154 C017 2 IF (I,EG,1) GO TO 3

154 C018 IF (XX,EG,1.) GO TO 4

154 C019 NGENUV/2

154 C020 I=I+1

154 C021 IF (I,GT,N2) I=I-2

154 C022 I=I-1

154 C023 I=I

154 C024 O1=(X1(M,12)-X1(M,11))/(Y1(M,12)-Y1(M,11))

154 C025 O2=((X1(M,13)-X1(M,11))/(Y1(M,13)-Y1(M,11))-O1)/(Y1(M,13)-Y1(M,12))

154 C026 )

154 C027 BETA=X1(M,11)+(XX-Y1(M,11))\*(O1+(XX-Y1(M,12))\*O2)

154 C028 5 RETURN

154 C029 3 CONTINUE

154 C030 O1=X1(2,1)/Y1(M,1)

154 C031 O2=(X1(M,2)/Y1(M,2)-O1)/(Y1(M,2)-Y1(M,1))

154 C032 BETA=XX\*(O1+(XX-Y1(M,1))\*O2)

154 C033 GO TO 5

154 C034 4 BETA=PI

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ISN C037  
ISN C038  
GC TO S  
END

\*\*\*\*\*F C R T M A N C N C S S R E F E R E N C E L I S T I N G \*\*\*\*\*

| INTERNAL STATEMENT NUMBERS |      |      |      |      |      |      |      |      |      |
|----------------------------|------|------|------|------|------|------|------|------|------|
| SYMBOL                     | C012 | C014 | C017 | C022 | C023 | C025 | C026 | C028 | C033 |
| I                          | C012 | C014 | C017 | C022 | C023 | C025 | C026 | C028 | C033 |
| M                          | C012 | C014 | C017 | C022 | C023 | C025 | C026 | C028 | C033 |
| N                          | C012 | C014 | C017 | C022 | C023 | C025 | C026 | C028 | C033 |
| 01                         | C012 | C014 | C017 | C022 | C023 | C025 | C026 | C028 | C033 |
| 02                         | C012 | C014 | C017 | C022 | C023 | C025 | C026 | C028 | C033 |
| 11                         | C012 | C014 | C017 | C022 | C023 | C025 | C026 | C028 | C033 |
| 12                         | C012 | C014 | C017 | C022 | C023 | C025 | C026 | C028 | C033 |
| 13                         | C012 | C014 | C017 | C022 | C023 | C025 | C026 | C028 | C033 |
| 14                         | C012 | C014 | C017 | C022 | C023 | C025 | C026 | C028 | C033 |
| 15                         | C012 | C014 | C017 | C022 | C023 | C025 | C026 | C028 | C033 |
| 16                         | C012 | C014 | C017 | C022 | C023 | C025 | C026 | C028 | C033 |
| 17                         | C012 | C014 | C017 | C022 | C023 | C025 | C026 | C028 | C033 |
| 18                         | C012 | C014 | C017 | C022 | C023 | C025 | C026 | C028 | C033 |
| 19                         | C012 | C014 | C017 | C022 | C023 | C025 | C026 | C028 | C033 |
| 20                         | C012 | C014 | C017 | C022 | C023 | C025 | C026 | C028 | C033 |
| 21                         | C012 | C014 | C017 | C022 | C023 | C025 | C026 | C028 | C033 |
| 22                         | C012 | C014 | C017 | C022 | C023 | C025 | C026 | C028 | C033 |
| 23                         | C012 | C014 | C017 | C022 | C023 | C025 | C026 | C028 | C033 |
| 24                         | C012 | C014 | C017 | C022 | C023 | C025 | C026 | C028 | C033 |
| 25                         | C012 | C014 | C017 | C022 | C023 | C025 | C026 | C028 | C033 |
| 26                         | C012 | C014 | C017 | C022 | C023 | C025 | C026 | C028 | C033 |
| 27                         | C012 | C014 | C017 | C022 | C023 | C025 | C026 | C028 | C033 |
| 28                         | C012 | C014 | C017 | C022 | C023 | C025 | C026 | C028 | C033 |
| 29                         | C012 | C014 | C017 | C022 | C023 | C025 | C026 | C028 | C033 |
| 30                         | C012 | C014 | C017 | C022 | C023 | C025 | C026 | C028 | C033 |
| 31                         | C012 | C014 | C017 | C022 | C023 | C025 | C026 | C028 | C033 |
| 32                         | C012 | C014 | C017 | C022 | C023 | C025 | C026 | C028 | C033 |
| 33                         | C012 | C014 | C017 | C022 | C023 | C025 | C026 | C028 | C033 |
| 34                         | C012 | C014 | C017 | C022 | C023 | C025 | C026 | C028 | C033 |
| 35                         | C012 | C014 | C017 | C022 | C023 | C025 | C026 | C028 | C033 |
| 36                         | C012 | C014 | C017 | C022 | C023 | C025 | C026 | C028 | C033 |
| 37                         | C012 | C014 | C017 | C022 | C023 | C025 | C026 | C028 | C033 |
| 38                         | C012 | C014 | C017 | C022 | C023 | C025 | C026 | C028 | C033 |
| 39                         | C012 | C014 | C017 | C022 | C023 | C025 | C026 | C028 | C033 |
| 40                         | C012 | C014 | C017 | C022 | C023 | C025 | C026 | C028 | C033 |
| 41                         | C012 | C014 | C017 | C022 | C023 | C025 | C026 | C028 | C033 |
| 42                         | C012 | C014 | C017 | C022 | C023 | C025 | C026 | C028 | C033 |
| 43                         | C012 | C014 | C017 | C022 | C023 | C025 | C026 | C028 | C033 |
| 44                         | C012 | C014 | C017 | C022 | C023 | C025 | C026 | C028 | C033 |
| 45                         | C012 | C014 | C017 | C022 | C023 | C025 | C026 | C028 | C033 |
| 46                         | C012 | C014 | C017 | C022 | C023 | C025 | C026 | C028 | C033 |
| 47                         | C012 | C014 | C017 | C022 | C023 | C025 | C026 | C028 | C033 |
| 48                         | C012 | C014 | C017 | C022 | C023 | C025 | C026 | C028 | C033 |
| 49                         | C012 | C014 | C017 | C022 | C023 | C025 | C026 | C028 | C033 |
| 50                         | C012 | C014 | C017 | C022 | C023 | C025 | C026 | C028 | C033 |
| 51                         | C012 | C014 | C017 | C022 | C023 | C025 | C026 | C028 | C033 |
| 52                         | C012 | C014 | C017 | C022 | C023 | C025 | C026 | C028 | C033 |
| 53                         | C012 | C014 | C017 | C022 | C023 | C025 | C026 | C028 | C033 |
| 54                         | C012 | C014 | C017 | C022 | C023 | C025 | C026 | C028 | C033 |
| 55                         | C012 | C014 | C017 | C022 | C023 | C025 | C026 | C028 | C033 |
| 56                         | C012 | C014 | C017 | C022 | C023 | C025 | C026 | C028 | C033 |
| 57                         | C012 | C014 | C017 | C022 | C023 | C025 | C026 | C028 | C033 |
| 58                         | C012 | C014 | C017 | C022 | C023 | C025 | C026 | C028 | C033 |
| 59                         | C012 | C014 | C017 | C022 | C023 | C025 | C026 | C028 | C033 |
| 60                         | C012 | C014 | C017 | C022 | C023 | C025 | C026 | C028 | C033 |
| 61                         | C012 | C014 | C017 | C022 | C023 | C025 | C026 | C028 | C033 |
| 62                         | C012 | C014 | C017 | C022 | C023 | C025 | C026 | C028 | C033 |
| 63                         | C012 | C014 | C017 | C022 | C023 | C025 | C026 | C028 | C033 |
| 64                         | C012 | C014 | C017 | C022 | C023 | C025 | C026 | C028 | C033 |
| 65                         | C012 | C014 | C017 | C022 | C023 | C025 | C026 | C028 | C033 |
| 66                         | C012 | C014 | C017 | C022 | C023 | C025 | C026 | C028 | C033 |
| 67                         | C012 | C014 | C017 | C022 | C023 | C025 | C026 | C028 | C033 |
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| 69                         | C012 | C014 | C017 | C022 | C023 | C025 | C026 | C028 | C033 |
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| 74                         | C012 | C014 | C017 | C022 | C023 | C025 | C026 | C028 | C033 |
| 75                         | C012 | C014 | C017 | C022 | C023 | C025 | C026 | C028 | C033 |
| 76                         | C012 | C014 | C017 | C022 | C023 | C025 | C026 | C028 | C033 |
| 77                         | C012 | C014 | C017 | C022 | C023 | C025 | C026 | C028 | C033 |
| 78                         | C012 | C014 | C017 | C022 | C023 | C025 | C026 | C028 | C033 |
| 79                         | C012 | C014 | C017 | C022 | C023 | C025 | C026 | C028 | C033 |
| 80                         | C012 | C014 | C017 | C022 | C023 | C025 | C026 | C028 | C033 |
| 81                         | C012 | C014 | C017 | C022 | C023 | C025 | C026 | C028 | C033 |
| 82                         | C012 | C014 | C017 | C022 | C023 | C025 | C026 | C028 | C033 |
| 83                         | C012 | C014 | C017 | C022 | C023 | C025 | C026 | C028 | C033 |
| 84                         | C012 | C014 | C017 | C022 | C023 | C025 | C026 | C028 | C033 |
| 85                         | C012 | C014 | C017 | C022 | C023 | C025 | C026 | C028 | C033 |
| 86                         | C012 | C014 | C017 | C022 | C023 | C025 | C026 | C028 | C033 |
| 87                         | C012 | C014 | C017 | C022 | C023 | C025 | C026 | C028 | C033 |
| 88                         | C012 | C014 | C017 | C022 | C023 | C025 | C026 | C028 | C033 |
| 89                         | C012 | C014 | C017 | C022 | C023 | C025 | C026 | C028 | C033 |
| 90                         | C012 | C014 | C017 | C022 | C023 | C025 | C026 | C028 | C033 |
| 91                         | C012 | C014 | C017 | C022 | C023 | C025 | C026 | C028 | C033 |
| 92                         | C012 | C014 | C017 | C022 | C023 | C025 | C026 | C028 | C033 |
| 93                         | C012 | C014 | C017 | C022 | C023 | C025 | C026 | C028 | C033 |
| 94                         | C012 | C014 | C017 | C022 | C023 | C025 | C026 | C028 | C033 |
| 95                         | C012 | C014 | C017 | C022 | C023 | C025 | C026 | C028 | C033 |
| 96                         | C012 | C014 | C017 | C022 | C023 | C025 | C026 | C028 | C033 |
| 97                         | C012 | C014 | C017 | C022 | C023 | C025 | C026 | C028 | C033 |
| 98                         | C012 | C014 | C017 | C022 | C023 | C025 | C026 | C028 | C033 |
| 99                         | C012 | C014 | C017 | C022 | C023 | C025 | C026 | C028 | C033 |
| 100                        | C012 | C014 | C017 | C022 | C023 | C025 | C026 | C028 | C033 |

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\*\*\*\*\*F C R T M A N C R C S S R E F E R E N C E L I S T I N G \*\*\*\*\*

| REFERENCES |         |            |  |  |  |  |  |  |  |
|------------|---------|------------|--|--|--|--|--|--|--|
| LABEL      | DEFINED | REFERENCES |  |  |  |  |  |  |  |
| 1          | C016    | C013       |  |  |  |  |  |  |  |
| 2          | C017    | C014       |  |  |  |  |  |  |  |
| 3          | C018    | C017       |  |  |  |  |  |  |  |
| 4          | C019    | C018       |  |  |  |  |  |  |  |
| 5          | C020    | C019       |  |  |  |  |  |  |  |

SIZE OF PROGRAM C00230 HEXADECIMAL BYTES

| SIZE OF PROGRAM C00230 HEXADECIMAL BYTES |     |      |      |      |     |      |      |      |     |
|--|-----|------|------|------|-----|------|------|------|-----|
| NAME                                     | TAG | TYPE | ADD. | NAME | TAG | TYPE | ADD. | NAME | TAG |
| 1  | 1   | 1    | 1    | 1    | 1   | 1    | 1    | 1    | 1   |
| 2  | 2   | 2    | 2    | 2    | 2   | 2    | 2    | 2    | 2   |
| 3  | 3   | 3    | 3    | 3    | 3   | 3    | 3    | 3    | 3   |
| 4  | 4   | 4    | 4    | 4    | 4   | 4    | 4    | 4    | 4   |
| 5  | 5   | 5    | 5    | 5    | 5   | 5    | 5    | 5    | 5   |

\*\*\*\* COMMON INFORMATION \*\*\*\*

| SIZE OF BLOCK C07530-HEXADECIMAL BYTES |      |      |      |       |      |      |      |      |       |
|--|------|------|------|-------|------|------|------|------|-------|
| VAR.                                   | NAME | TYPE | REL. | ADDR. | VAR. | NAME | TYPE | REL. | ADDR. |
| 1                                      | S11  | R#4  |      |       | 1    | S22  | R#4  |      |       |
| 2                                      | S12  | R#4  |      |       | 2    | S23  | R#4  |      |       |
| 3                                      | S13  | R#4  |      |       | 3    | S24  | R#4  |      |       |
| 4                                      | S14  | R#4  |      |       | 4    | S25  | R#4  |      |       |
| 5                                      | S15  | R#4  |      |       | 5    | S26  | R#4  |      |       |

NAME OF COMMON BLOCK \* PARAM\* SIZE OF BLOCK 000048 HEXADECIMAL BYTES

| VAR. NAME | TYPE | REL. ADDR. | VAR. NAME | TYPE | REL. ADDR. | VAR. NAME | TYPE | REL. ADDR. |
|-----------|------|------------|-----------|------|------------|-----------|------|------------|
| IND       | I*4  | N.R.       | NSCA      | I*4  | N.R.       | NUMK      | I*4  | 00001C     |
| KMAX      | I*4  | N.R.       | IST       | I*4  | N.R.       | FACTOR    | R*4  | N.R.       |
| NM        | I*4  | N.R.       | NMAX      | I*4  | N.R.       |           |      |            |

NAME OF COMMON BLOCK \* SCAT\* SIZE OF BLOCK 000020 HEXADECIMAL BYTES

| VAR. NAME | TYPE | REL. ADDR. | VAR. NAME | TYPE | REL. ADDR. | VAR. NAME | TYPE | REL. ADDR. |
|-----------|------|------------|-----------|------|------------|-----------|------|------------|
| N         | I*4  | N.R.       | INDIC     | I*4  | N.R.       | JK        | I*4  | 000018     |
|           |      |            |           |      |            | IGND      | I*4  | N.R.       |

NAME OF COMMON BLOCK \* CONST\* SIZE OF BLOCK 000008 HEXADECIMAL BYTES

| VAR. NAME | TYPE | REL. ADDR. | VAR. NAME | TYPE | REL. ADDR. | VAR. NAME | TYPE | REL. ADDR. |
|-----------|------|------------|-----------|------|------------|-----------|------|------------|
| PI        | I*4  | N.R.       | PI        | I*4  | N.R.       |           |      |            |

LEVEL 21.6 (DEC 72) CS/360 FCSTRAN H DATE 76.324/21.49.00

COMPILER OPTIONS - NAME= MAINCLPT=02, LINECNT=02, SIZE=0000K,  
SOURCE, EBCDIC, NLIST, NCDECK, LCAD, MAP, NCEDIT, IC, XREF

SUBROUTINE ELEMENTS (BETA, S, K)

SUBROUTINE ELEMENTS

THIS SUBROUTINE COMPUTES THE ALL SCATTERING MATRIX ELEMENTS  
FOR THE SCATTERING ANGLE BETA.

DIMENSION S(6), X(5,100), S11(100,5), S12(100,5,2), S22(100,5,2),  
S33(100,5,2), S34(100,5,2), S44(100,5,2)

DIMENSION X1(5,100), Y1(5,100)

DIMENSION CDF (5,100)

COMMON S11, S12, S22, S33, S34, S44, X, X1, Y1, CDF

COMMON /CONST/ FL, IPL

COMMON /SCAT/ N, INU1(15), JK, ICND

COMMON /ACC/ AC1, AC2, AC3

I=JK

IF (INDIC(JK).EQ.0) RETURN

IF (K.EQ.1) CALL XSCALM(BETA, S(1), X, S11, N, 1)

IF (K.EQ.2) S(1)=1.

CALL X32(BETA, S(2), X, S12, N, 1, K)

CALL X32(BETA, S(3), X, S33, N, 1, K)

CALL X32(BETA, S(4), X, S34, N, 1, K)

IF (INDIC(JK).NE.3) RETURN

CALL X32(BETA, S(5), X, S22, N, 1, K)

CALL X32(BETA, S(6), X, S44, N, 1, K)

RETURN

END

INTERNAL STATEMENT NUMBERS

| SYMBOL | INTERNAL STATEMENT NUMBERS                        | CRCS  | REFERENCE | LISTING |
|--------|---|---|-----------|---------|
| I      | 0010 0017 0018 0019 0020 0021 0022 0023           | 0023  |           |         |
| K      | 0024 0025 0026 0027 0028 0029 0030 0031 0032 0033 | 0023 0022 0023 0023 0023 0023 0023 0023 0023 0023 |           |         |
| N      | 0034 0035 0036 0037 0038 0039 0040 0041 0042 0043 | 0023 0023 0023 0023 0023 0023 0023 0023 0023 0023 |           |         |
| S      | 0044 0045 0046 0047 0048 0049 0050 0051 0052 0053 | 0023 0023 0023 0023 0023 0023 0023 0023 0023 0023 |           |         |
| X      | 0054 0055 0056 0057 0058 0059 0060 0061 0062 0063 | 0023 0023 0023 0023 0023 0023 0023 0023 0023 0023 |           |         |
| JK     | 0064 0065 0066 0067 0068 0069 0070 0071 0072 0073 | 0023 0023 0023 0023 0023 0023 0023 0023 0023 0023 |           |         |

\*\*\*\*\*END OF COMPILATION\*\*\*\*\*

177K-BYTES-OF-CORE-NOT-USED

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|    |     |        |
|----|-----|--------|
| PI | C27 | CCCC   |
| XI | C29 | CCCCC  |
| VI | C31 | CCCCCC |

| ELEMENTS / | SIZE | CF | PROGRAM | CCCC2EE | HEXADECIMAL | BYTES | PAGE | 0033 |
|------------|------|----|---------|---------|-------------|-------|------|------|
|------------|------|----|---------|---------|-------------|-------|------|------|

| NAME  | TAG | TYPE | ADD.   | NAME  | TAG | TYPE | ADD.   | NAME  | TAG | TYPE | ADD.   |
|-------|-----|------|--------|-------|-----|------|--------|-------|-----|------|--------|
| I SFA | C   | I#4  | CC1144 | K SFA | C   | I#4  | CC1142 | S SFA | C   | I#4  | CC1140 |
| X SFA | C   | K#4  | CC1140 | JK F  | C   | I#4  | CC1142 | PI    | C   | R#4  | CC1140 |
| X     | C   | K#4  | CC1140 | ACI   | C   | R#4  | N.R.   | AC2   | C   | R#4  | N.R.   |
| COH   | C   | R#4  | N.R.   | S11   | SFA | C    | CC1140 | S12   | SFA | C    | CC1140 |
| COH   | C   | R#4  | CC1140 | S34   | SFA | C    | CC1140 | S34   | SFA | C    | CC1140 |
| COH   | C   | R#4  | CC1140 | BETA  | SFA | C    | CC1140 | TPI   | C   | R#4  | CC1140 |
| COH   | C   | R#4  | CC1140 | XSECM | SFA | C    | CC1140 | INDIC | C   | I#4  | CC1140 |

\*\*\*\*\*  
COMMON INFORMATION  
\*\*\*\*\*

[illegible]

| VAR. | NAME | TYPE | REL. | ADDR.  | VAR. | NAME | TYPE | REL.   | ADDR. | N.R.       |
|------|------|------|------|--------|------|------|------|--------|-------|------------|
| S11  | R#4  | G#4  | S12  | C0C7C0 | S22  | X    | H#4  | C0I770 | S33   | H#4 C02710 |
| S24  | R#4  | F#4  | S44  | C0J6J0 |      |      |      |        | XI    | H#4 N.R.   |
| Y1   | R#4  | GDF  |      | N.R.   |      |      |      | C0C5F0 |       |            |

| NAME OF COMMON BLOCK | * CCNST* | SIZE OF BLOCK | HEXADECIMAL BYTES |
|----------------------|----------|---------------|-------------------|
| CC0008               |          |               |                   |

| VAR. | NAME | TYPE | REL. | ADDR. | VAR. | NAME | TYPE | REL. | ADDR. | VAR. | NAME | TYPE | REL. | ADDR. |
|------|------|------|------|-------|------|------|------|------|-------|------|------|------|------|-------|
| F1   | N#4  |      |      | N.R.  |      | TP1  | R+4  |      | N.F.  |      |      |      |      |       |

| NAME OF COMMON BLOCK * | SCAT* | SIZE OF BLOCK | COCC020 | HEXADECIMAL BYTES |
|------------------------|-------|---------------|---------|-------------------|
| ...                    | ...   | ...           | ...     | ...               |

| VAR. | NAME | TYPE   | REL. | ADDR. | VAR.  | NAME | TYPE   | REL. | ADDR. | VAR. | NAME | TYPE   | REL. | ADDR. |
|------|------|--------|------|-------|-------|------|--------|------|-------|------|------|--------|------|-------|
| "    | I#4  | C0C0C0 |      |       | INDIC | I#4  | COC0C4 |      |       | JK   | I#4  | Q0QC18 |      |       |
|      |      |        |      |       |       |      |        |      |       |      | IGND | I#4    | N#R. |       |

| NAME OF COMMON BLOCK | ACC# | SIZE OF BLOCK | CCCCC HEXADECIMAL BYTES |
|----------------------|------|---------------|-------------------------|
| COMMON BLOCK 1       | 1    | 100           | 0000000000              |
| COMMON BLOCK 2       | 2    | 200           | 0000000000              |
| COMMON BLOCK 3       | 3    | 300           | 0000000000              |
| COMMON BLOCK 4       | 4    | 400           | 0000000000              |
| COMMON BLOCK 5       | 5    | 500           | 0000000000              |
| COMMON BLOCK 6       | 6    | 600           | 0000000000              |
| COMMON BLOCK 7       | 7    | 700           | 0000000000              |
| COMMON BLOCK 8       | 8    | 800           | 0000000000              |
| COMMON BLOCK 9       | 9    | 900           | 0000000000              |
| COMMON BLOCK 10      | 10   | 1000          | 0000000000              |

| VAR.     | NAME  | TYPE  | REL. | ADDR. | VAR.  | NAME | TYPE  | REL. | ADDR. | VAR.  | NAME | TYPE  | REL.  | ADDR. |
|----------|-------|-------|------|-------|-------|------|-------|------|-------|-------|------|-------|-------|-------|
| .....AC1 | ..... | ..... | N..  | R#4   | ..... | AC2  | ..... | R#4  | ..... | ..... | AC3  | ..... | N..R. | ..... |

```
*OPTIONS IN EFFECT*      NAME=      MAIN.CPT=C2.LINECNY=92.SIZE=6000K.
```

\*OPTIONS IN EFFECT\* SOURCE,EBCDIC,NULIST,NUDECK,LCAD,NAP,NCEDIT,IC,XREF

```
#STATISTICS# SOURCE STATEMENTS = 24 ,PROGRAM SIZE = 750
```

#STATISTICS\* -AND- DIAGNOSTICS-GENERATED-

\*\*\*\*\* END CF COMPILATION \*\*\*\*\*

LEVEL: 21.6 (DEC 72)

CS/260 FCETRA H

DATE : 76.324/21.49.07.

```

COMPILER OPTIONS - NAME=CPT=35,LINECNT=22,SIZE=0000X,
SOURCE=PHI.C,LIST,NGDECK=K,L,40,MAF,NGCT=IC,XREF,
SUBROUTINE XSE(PHI,P,X,Y,N,N,K)
ISN 0002

```

COMMUNIST PARTY, U.S.A.  
C C C  
S U B C U T I N E X S

THIS SUBROUTINE COMPUTES PHASE FUNCTIONS BY TABLE LOOK-UP  
AND INTERPOLATION.

C\*\*  
C\*\*  
C\*\*

```
ISN 0003 DIMENSION X(5,100),Y(100,5,2)
ISN 0004 DO 1 I=2,N
ISN 0005 IF (PHI-1,X(M,1)) GO TO 2
ISN 0007 1 CONTINUE
ISN 0008 DEX(N,M,K)
ISN 0009 RETURN
ISN 0010 2 CONTINUE
ISN 0011 NZEN/2
ISN 0012 IZ=I+1
ISN 0013 IF (I-GT-N2) I3=I-2
ISN 0014 I1=I-1
ISN 0015 I2=I
ISN 0016 D1=(Y(I2,M,K)-Y(I1,M,K))/(X(M,I2)-X(M,I1))
ISN 0017 D2=((Y(I3,M,K)-Y(I1,M,K))/(X(M,I3)-X(M,I1))-D1)/(X(M,I3)-X(M,I2))
ISN 0018 DEX(I1,M,K)+(PHI-X(M,I1))*(D1+(PHI-X(M,I2))*D2)
ISN 0019 RETURN
ISN 0021 END
```

PAGE 002

\*\*\*\*\*F C R T R A N C R C S S R E F E R E N C E L I S T I N G\*\*\*\*\*

SYMBOL INTERNAL STATEMENT NUMBERS

| SYMBOL | INTERNAL STATEMENT NUMBERS         |
|--------|------------------------------------|
| B      | 0002 0003 0019                     |
| I      | 0004 0005 0012 0013 0015 0019      |
| K      | 0006 0007 0017 0018 0019           |
| M      | 0008 0009 0017 0018 0019 0019 0019 |
| N      | 0010 0011 0017 0018 0019 0019      |
| X      | 0012 0013 0017 0018 0019 0019      |
| Y      | 0014 0015 0017 0018 0019 0019      |
| D1     | 0016 0017 0018 0019 0019           |
| D2     | 0018 0019 0019 0019 0019           |
| I1     | 0020 0021 0022 0023 0024           |
| I2     | 0025 0026 0027 0028 0029           |
| I3     | 0030 0031 0032 0033 0034           |
| N2     | 0035 0036 0037 0038 0039           |
| PHI    | 0040 0041 0042 0043 0044           |
| X52    | 0045 0046 0047 0048 0049           |

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PAGE 003

\*\*\*\*\*F C R T R A N C R C S S R E F E R E N C E L I S T I N G\*\*\*\*\*

LABEL DEFINED REFERENCES

| 1 | 0007 | 0004 |
|---|------|------|
| 2 | 0010 | 0005 |

SIZE OF PROGRAM 000306 HEXADECIMAL BYTES PAGE 004

| NAME  | TAG  | ADD.   | TYPE | ACD.   | NAME  | TAG   | TYPE | ADD.   | NAME  | TAG   | TYPE | ADD.   |
|-------|------|--------|------|--------|-------|-------|------|--------|-------|-------|------|--------|
| B S   | N F  | 000000 | R*4  | 000000 | I SF  | X F   | R*4  | 000000 | K F   | M F   | I*4  | 000000 |
| D2 SF | N2 S | 000000 | R*4  | 000000 | PHI F | PHI F | R*4  | 000000 | Y F   | X F   | R*4  | 000000 |
|       |      |        |      |        |       |       |      |        | 12 SF | I3 SF | R*4  | 000000 |
|       |      |        |      |        |       |       |      |        | X52   | X52   | R*4  | 000000 |

PAGE 005

\*OPTIONS IN EFFECT\* NAME= MAIN,OPT=02,LINECNT=92,SIZE=0000K.

\*OPTIONS IN EFFECT\* SOURCE=ERCOIC,NOLIST,NUDECK,LCAD,MAP,NCEDIT,ID,XREF

\*STATISTICS\* SOURCE STATEMENTS = 20 ,PROGRAM SIZE = 774

\*STATISTICS\* NO DIAGNOSTICS GENERATED

\*\*\*\*\* END OF COMPILATION \*\*\*\*\*

181K BYTES OF CCRE NOT USED

LEVEL 21.6 (DEC 72)

CS/J36 FCRTAN M

DATE 76.324/21.49.16

COMPILER-OPTIONS= NAME= MAIN,OPT=02,LINECNT=92,SIZE=0000K,  
SOURCE=ERCOIC,NOLIST,NUDECK,LCAD,MAP,NCEDIT,ID,XREF  
SUBROUTINE RECALL(COUT,JETA,C3)

ISN 0002

C\*\*  
C\*\*  
C\*\*

S U E R C U T I N E R E N E

C\*\*  
C\*\*  
C\*\*  
C\*\*

THIS SUBROUTINE RENEWS THE SCATTERING MATRIX AFTER A REAL  
SCATTERING

```

15N 0003 DIMENSION SSIN(10),SCUT(6),S11(100,5),S12(100,5,2),S2
15N 0004 12(100,5,2),S23(100,5,2),S34(100,5,2),S44(100,5,2),S(6)
15N 0005 DIMENSION X(5,100)
15N 0006 DIMENSION X1(5,1,10),Y1(5,100)
15N 0007 DIMENSION CDF(5,100)
15N 0008 COMMON/SCUT/SCUT,SCUT,SCUT
15N 0009 COMMON/PHI/CIN(6),UN,VN,MN,JJ,SCUT(16),INCLD
15N 0010 COMMON/SCAT/M,INDIC(5),TK,FEND
15N 0011 CALL FIXALL(CUT(4),CUT(5),CUT(6),CIN(4),CIN(5),CIN(6),UN,VN,MN,
15N 0012 PHI,AT,CI)
15N 0013 CKEAT
15N 0014 VN=DI
15N 0015 *NEC1
15N 0016 CALL ROTATE(SCUT,SSIN,PHI)
15N 0017 IF(ISCAT.NE.3)GO TO 10
15N 0018 IF(INDIC(JK).EQ.1)GO TO 10
15N 0019 K1=2
15N 0020 IF(IMPX.NE.0)K1=1
15N 0021 CALL ELEMIS(ETA,5,K1)
15N 0022 IF(INDIC(JK).EQ.3)CALL GENSCA(SSIN,SCUT,S,2)
15N 0023 IF(INDIC(JK).NE.3)CALL SCATMI(SSIN,SCUT,S,2)
15N 0024 GO TO 2
15N 0025 1 CALL SCATRA(SSIN,SCUT,CB,2)
15N 0026 2 CONTINUE
15N 0027 DL 3 1=1,6
15N 0028 3 CIN(1)=SCUT(1)
15N 0029 RETURN
15N 0030 10 CONTINUE
15N 0031 C
15N 0032 REHEW GROUND SCATTERING
15N 0033 IF(IRCUD.EQ.0)CALL LAUBHT(CCUT,S,2)
15N 0034 IF(IRCUD.NE.0)CALL GENSCA(CCUT,CIN,IRCUD,S,2)
15N 0035 CALL GENSCA(SSIN,SCUT,S,2)
15N 0036 ISCAT=0
15N 0037 CLTC 2
15N 0038 END

```

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PAGE 002

\*\*\*\*\*F C R T R A N C R C S S R E F E R E N C E L I S T I N G\*\*\*\*\*

SYMBOL INTERNAL STATEMENT NUMBERS

|       |      |                          |                          |
|-------|------|--------------------------|--------------------------|
| I     | 0001 | 0032                     | 0032                     |
| N     | 0010 |                          |                          |
| X     | 0003 | 0023                     | 0024 0026 0035 0037 0039 |
| A1    | 0011 | 0012                     |                          |
| D1    | 0011 | 0013                     |                          |
| CB    | 0029 |                          |                          |
| C1    | 0011 | 0014                     |                          |
| JJ    | 0029 |                          |                          |
| JK    | 0010 | 0024                     | 0026                     |
| AT    | 0021 | 0023                     |                          |
| VN    | 0005 | 0011                     | 0012                     |
| MN    | 0005 | 0011                     | 0013                     |
| X1    | 0005 | 0011                     | 0014                     |
| Y1    | 0005 |                          |                          |
| CDF   | 0010 |                          |                          |
| CIN   | 0005 | 0011                     | 0011 0011 0032 0035 0037 |
| IMP   | 0005 |                          |                          |
| PHI   | 0011 | 0015                     |                          |
| S11   | 0011 |                          |                          |
| S12   | 0011 |                          |                          |
| S22   | 0011 |                          |                          |
| S33   | 0011 |                          |                          |
| S34   | 0011 |                          |                          |
| S44   | 0011 |                          |                          |
| ETA   | 0011 |                          |                          |
| CUT   | 0011 | 0011 0011 0032 0035 0037 |                          |
| INDC  | 0011 |                          |                          |
| IMPJ  | 0011 |                          |                          |
| IMPJ  | 0011 |                          |                          |
| IMPJ  | 0011 |                          |                          |
| SDTH  | 0011 |                          |                          |
| SCUT  | 0011 | 0024 0026 0029 0039      |                          |
| SSIN  | 0011 | 0024 0026 0029 0039      |                          |
| INCLD | 0011 |                          |                          |
| INDIC | 0011 | 0024 0026                |                          |





\*STATISTICS\* NO DIAGNOSTICS GENERATED

\*\*\*\*\* END OF COMPILE \*\*\*\*\*

177K BYTES OF CORE NOT USED

LEVEL 21.6 (DEC 72)

CS/360 FCRTAN H

DATE 76.324/21.49.23

COMPILER OPTIONS - NAME= MAIN,OPT=02,LINECNT=22,SIZE=0000K,  
SOURCE=ECGIC,NLIST,NODECK,LCD,MAP,NCEdit,IC,XREF

ISN 0002  
ISN 0003  
ISN 0004  
ISN 0005  
ISN 0006  
ISN 0007  
ISN 0008  
ISN 0009  
ISN 0010  
ISN 0011  
ISN 0012  
ISN 0013  
ISN 0014  
ISN 0015

\*\*\*\*\* F C R T A N C R C S S R E F E R E N C E L I S T I N G \*\*\*\*\*

PAGE 002

SYMBOL INTERNAL STATEMENT NUMBERS

AI 0002 0004 0006 0008 0010 0012 0014

AI 0002 0004 0006 0008 0010 0012 0014

AI 0002 0004 0006 0008 0010 0012 0014

AI 0002 0004 0006 0008 0010 0012 0014

AI 0002 0004 0006 0008 0010 0012 0014

AI 0002 0004 0006 0008 0010 0012 0014

AI 0002 0004 0006 0008 0010 0012 0014

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181K BYTES OF CORE NOT USED

LEVEL 21.6 (DEC 72)

CS/360 FCRTAN H

DATE 76.324/21.49.32

COMPILER OPTIONS - NAME= MAIN,OPT=02,LINECNT=22,SIZE=0000K,  
SOURCE=ECGIC,NLIST,NODECK,LCD,MAP,NCEdit,IC,XREF

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THIS SUBROUTINE ACCUMULATES A NEW (GENERAL) SCATTERING INTO  
THE CUMULATIVE SCATTERING MATRIX BY POST MULTIPLICATION  
(SUITABLE FOR BACKWARDS CODE)

SSIN(16) = CUMULATIVE SCATTERING MATRIX PRIOR TO SCATTERING  
(INPUT)

KS = SCATTERING MATRIX FOR GENERAL SCATTERING  
KS = INPUT (INPUT) (1) FOR HYPERMETRIC SCATTERING,  
RETURN ONLY THE FIRST COLUMN OF SCUT. (2) RETURN ALL OF SCUT

SCUT = TRANSFORMED SCATTERING MATRIX (OUTPUT)  
SCUT = SSIN\*5

DIMENSION SSIN(16), SCUT(16),S(6)

IF (KS.EC.1) GO TO 20

GO TO 10

IS = 1+4

IS = 1+8

IS = 1+12

SCUT(I) = SSIN(I)\*S(1)+SSIN(I+5)\*S(2)



```

1SN C003 DIMENSION SSIN(10),SOUT(10),S(6)
1SN C004 IF(KS=1) GO TO 20
1SN C005 DO 10 I=1,4
1SN C006   IS = I+4
1SN C007   I13 = I+12
1SN C008   I13 = I+12
1SN C009   SOUT(I) = SSIN(I)*SIN(I5)*S(2)
1SN C010   SOUT(I5) = SSIN(I5)*SIN(I)*S(2)
1SN C011   SOUT(I9) = SSIN(I9)*S(3)-SSIN(I12)*S(4)
1SN C012   SOUT(I13) = SSIN(I13)*S(3)+SSIN(I9)*S(4)
1SN C013   GO TO 10 CONTINUE
1SN C014   RETURN
1SN C015   DO 20 J=1,4
1SN C016   IS = J+4
1SN C017   I13 = J+12
1SN C018   SOUT(I) = SSIN(I)*SIN(I5)*S(2)
1SN C019   SOUT(I5) = SSIN(I5)*SIN(I)*S(2)
1SN C020   SOUT(I9) = SSIN(I9)*S(3)-SSIN(I12)*S(4)
1SN C021   SOUT(I13) = SSIN(I13)*S(3)+SSIN(I9)*S(4)
1SN C022   GO TO 20 CONTINUE
1SN C023   RETURN
1SN C024   END

```

PAGE 002

\*\*\*\*F O R T R A N C R C S S R E F E R E N C E L I S T I N G\*\*\*\*

```

SYMBOL INTERNAL STATEMENT NUMBERS
1 C003 C007 C008 C010 C011 C012 C016 C017 C018 C018
5 C003 C008 C010 C011 C012 C013 C018 C018
15 C007 C010 C011 C017 C018
19 C008 C012 C013
KS C008 C012 C013
113 C008 C012 C013
SOUT C008 C012 C013
SSIN C008 C010 C011 C012 C012 C013 C018 C018
SCALM C002

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PAGE 003

\*\*\*\*E C R T R A N C R C S S R E F E R E N C E L I S T I N G\*\*\*\*

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LABEL DEFINED REFERENCES
10 C014 C008
20 C016 C004
21 C018 C016

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SCALM / SIZE OF PROGRAM C00280 HEXADECIMAL BYTES PAGE 004

| NAME  | TAG | TYPE | ADD.   | NAME   | TAG | TYPE | ADD. | NAME   | TAG | TYPE | ADD. |
|-------|-----|------|--------|--------|-----|------|------|--------|-----|------|------|
| 1 SF  |     | I*4  | C00300 | S      | F   | XR   | I*4  | C00000 |     |      |      |
| KS    |     | I*4  | C00000 | I13 SF |     | XR   | I*4  | C00000 |     |      |      |
| SCALM |     | R*4  | C00000 |        |     |      |      |        |     |      |      |

PAGE 005

LABEL ADDR

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10 C0010E 20 C0010E 21 C0010E

\*OPTIONS IN EFFECT\* NAME= MAIN,OPT=02,LINECNT=82,SIZE=0000K.

\*OPTIONS IN EFFECT\* SOURCE=ECDC,LCAD,MAP,NCEDIT,IC,XREF

\*STATISTICS\* SOURCE STATEMENTS = 15,PRCGRAM SIZE = 640

\*STATISTICS\* NO DIAGNOSTICS GENERATED

\*\*\*\*END OF COMPILATION\*\*\*\*

181K BYTES OF CORE NOT USED

LEVEL 21.0 (DEC 72)

CS/360 FCRTKAN H

DATE 76.324/21.49.50

```

COMPILER OPTIONS - NAME= MAIN,OPT=02,LINECNT=82,SIZE=0000K,
SOURCE=ECDC,LCAD,MAP,NCEDIT,IC,XREF
SUBROUTINE SCALM (SSIN,SOUT,CE,KS)

```

C SUBROUTINE SCALM

C THIS SUBROUTINE ACCUMULATES A NEW FAYLEIGH SCATTERING  
C INTO THE CUMULATIVE SCATTERING MATRIX BY POST-MULTIPLICATION  
C (SUBROUTINE SCALM)

C SSIN(16) = CUMULATIVE SCATTERING MATRIX PRIOR TO SCATTERING  
C (INPUT)  
C CU = COSINE OF THE SCATTERING ANGLE (INPUT)

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OF POOR QUALITY

```

C      KS = INDICATOR(INPUT) (=1, HYPCIPETICAL SCATTERING; COMPUTE ONLY.
C      FIRST COLUMN OF SOUT AND USE SCATTERING MATRIX NOT
C      NORMALIZED BY S11)
C      (=2, REAL SCATTERING; COMPUTE ALL CP-SOUT, USE
C      SCATTERING MATRIX NORMALIZED SO THAT S11=1)
C      SOUT(16) = RESULTANT CUMULATIVE SCATTERING MATRIX AFTER
C      RAYLEIGH SCATTERING(COINPUT)
C      DIMENSION SSIN(16),SOUT(16)
C      CO2=CO*CO
C      T1=0.75*(1+CO2)
C      T2=0.75*(CO2-1.)
C      T3=1.5*CO
C      IF(KS.EQ.1) GO TO 20
C      T2=12/T1
C      T3=T3/T1
C      T1=1.
C      DO 10 I=1,4
C      IS=I+4
C      IS=I+3
C      IS=I+2
C      IS=I+1
C      SOUT(I) = SSIN(I) + SSIN(IS)*T2
C      SOUT(IS) = SSIN(IS) + SSIN(I)*T2
C      SOUT(I5) = SSIN(I5)*T3
C      SOUT(I13) = SSIN(I13)*T3
C      10 CONTINUE
C      RETURN
C      20 DO 21 I=1,4
C      IS=I+4
C      IS=I+3
C      IS=I+2
C      IS=I+1
C      SOUT(I) = SSIN(I)*T1+SSIN(IS)*T2
C      RETURN
C      21 CONTINUE
C      END

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**T L S I N G**

[illegible]

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| SYMBOL | INTERNAL-STATEMENT-NUMBERS | 0017 | 0018 | 0023 | 0024 | 0025 | 0025 |
|--------|----------------------------|------|------|------|------|------|------|
| C012   | 0014                       | 0015 | 0016 | 0017 | 0018 | 0023 | 0024 |
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| C014   | 0014                       | 0015 | 0016 | 0017 | 0018 | 0023 | 0024 |
| C015   | 0014                       | 0015 | 0016 | 0017 | 0018 | 0023 | 0024 |
| C016   | 0014                       | 0015 | 0016 | 0017 | 0018 | 0023 | 0024 |
| C017   | 0014                       | 0015 | 0016 | 0017 | 0018 | 0023 | 0024 |
| C018   | 0014                       | 0015 | 0016 | 0017 | 0018 | 0023 | 0024 |
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| C020   | 0014                       | 0015 | 0016 | 0017 | 0018 | 0023 | 0024 |
| C021   | 0014                       | 0015 | 0016 | 0017 | 0018 | 0023 | 0024 |
| C022   | 0014                       | 0015 | 0016 | 0017 | 0018 | 0023 | 0024 |
| C023   | 0014                       | 0015 | 0016 | 0017 | 0018 | 0023 | 0024 |
| C024   | 0014                       | 0015 | 0016 | 0017 | 0018 | 0023 | 0024 |
| C025   | 0014                       | 0015 | 0016 | 0017 | 0018 | 0023 | 0024 |
| C026   | 0014                       | 0015 | 0016 | 0017 | 0018 | 0023 | 0024 |
| C027   | 0014                       | 0015 | 0016 | 0017 | 0018 | 0023 | 0024 |
| C028   | 0014                       | 0015 | 0016 | 0017 | 0018 | 0023 | 0024 |
| C029   | 0014                       | 0015 | 0016 | 0017 | 0018 | 0023 | 0024 |
| C030   | 0014                       | 0015 | 0016 | 0017 | 0018 | 0023 | 0024 |
| C031   | 0014                       | 0015 | 0016 | 0017 | 0018 | 0023 | 0024 |
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| C036   | 0014                       | 0015 | 0016 | 0017 | 0018 | 0023 | 0024 |
| C037   | 0014                       | 0015 | 0016 | 0017 | 0018 | 0023 | 0024 |
| C038   | 0014                       | 0015 | 0016 | 0017 | 0018 | 0023 | 0024 |
| C039   | 0014                       | 0015 | 0016 | 0017 | 0018 | 0023 | 0024 |
| C040   | 0014                       | 0015 | 0016 | 0017 | 0018 | 0023 | 0024 |
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7-I-S-T-I-N-G

**SECRET**

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SCATRA / SIZE CF PRGGRAM C00244 HEXADECIMAL BYTES PAGE-004

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**LABEL**      **AM**

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*OPTIONS IN EFFECT*
NAME= MAIN.OPT=LS.LINECNT=82,SIZE=800CK.
      1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35 36 37 38 39 40 41 42 43 44 45 46 47 48 49 50 51 52 53 54 55 56 57 58 59 60 61 62 63 64 65 66 67 68 69 70 71 72 73 74 75 76 77 78 79 80 81 82 83 84 85 86 87 88 89 90 91 92 93 94 95 96 97 98 99 100
```

\*OPTIONS..IN EFFECT\*-----SOURCE,EBUDIC,NULIST,NUDECK,LCAD,MAP,NGEDIT,IC,XREF.

```
*STATISTICS* SOURCE STATEMENTS = 26 ,PROGRAM SIZE = 580
```

STATISTICS\* NU CLIASTICS GENERATED









```

C      IHC0=0    LANGERTIAN GROUND
C      KUOH FHEMEL ( GAUSSIAN SLOPE DISTRIBUTION)
C      XTH,XPH = INPUT RANDOM NUMBERS
DIMENSION COUT(3),CIN(3)
COMMON/CONSTY(P,T,P)
COMMON/PREN/PN,SIG,SIG2,WNG(3),ZX,ZY
IF(IHC0.NE.0)GO TO 100
LANGERTIAN REFLECTION
PHI=PI*XPH
SP=SIN(PHI)
CP=COS(PHI)
SN=SQRT(1.-XTH*XTH)
COUT(4)=SN*CP
CUT(C)=SN*SP
CUT(G)=XTH
DO 2 J=1,3
2 CUT(J)=CIN(J)
RETURN
100 CONTINUE
THIS SECTION IS FOR NON-LANGERTIAN REFLECTION
GENERATE SLOPES FROM GAUSSIAN DISTRIBUTION
103 CONTINUE
CALL GAUSS(XTH,*SIG,G,.ZX)
CALL GAUSS(XPH,*SIG,G,.ZY)
LN=SQRT(ZX*ZX+ZY*ZY+1.)
COMPUTE NORMAL TC SLOPE
WNG(1)=-ZX/LN
WNG(2)=-ZY/LN
WNG(3)=1./LN
DO IF1 J=1,3
JP=J+J
GG+CIN(JP)*WNG(J)
101 CONTINUE
CHECK TC SEE IF SLOPE IS FEASIBLE.
IF(G.GT.C)GO TO 103
IF(NGT,-TRY AGAIN)
102 CONTINUE
DO ICE J=1,3
JP=J+J
CUT(JPF)=-2.*G*WNG(J)+CIN(JF)
102 CONTINUE
GO TO 3
END

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PAGE 002

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PAGE 003

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| L20  | -  | -   | R**  | 0000C |   |      |   |    |     | R**  | 0000B |   |      |    |     | R**  | 0000B |
| L21  | -  | -   | R**  | N.F.C |   |      |   |    |     | R**  | 0000B |   |      |    |     | R**  | 0000B |
| L22  | -  | -   | R**  | 0000C |   |      |   |    |     | R**  | 0000B |   |      |    |     | R**  | 0000B |
| L23  | -  | -   | R**  | 0000C |   |      |   |    |     | R**  | 0000B |   |      |    |     | R**  | 0000B |
| L24  | -  | -   | R**  | 0000C |   |      |   |    |     | R**  | 0000B |   |      |    |     | R**  | 0000B |
| L25  | -  | -   | R**  | 0000C |   |      |   |    |     | R**  | 0000B |   |      |    |     | R**  | 0000B |
| L26  | -  | -   | R**  | 0000C |   |      |   |    |     | R**  | 0000B |   |      |    |     | R**  | 0000B |
| L27  | -  | -   | R**  | 0000C |   |      |   |    |     | R**  | 0000B |   |      |    |     | R**  | 0000B |
| L28  | -  | -   | R**  | 0000C |   |      |   |    |     | R**  | 0000B |   |      |    |     | R**  | 0000B |
| L29  | -  | -   | R**  | 0000C |   |      |   |    |     | R**  | 0000B |   |      |    |     | R**  | 0000B |
| L30  | -  | -   | R**  | 0000C |   |      |   |    |     | R**  | 0000B |   |      |    |     | R**  | 0000B |
| L31  | -  | -   | R**  | 0000C |   |      |   |    |     | R**  | 0000B |   |      |    |     | R**  | 0000B |
| L32  | -  | -   | R**  | 0000C |   |      |   |    |     | R**  | 0000B |   |      |    |     | R**  | 0000B |
| L33  | -  | -   | R**  | 0000C |   |      |   |    |     | R**  | 0000B |   |      |    |     | R**  | 0000B |
| L34  | -  | -   | R**  | 0000C |   |      |   |    |     | R**  | 0000B |   |      |    |     | R**  | 0000B |
| L35  | -  | -   | R**  | 0000C |   |      |   |    |     | R**  | 0000B |   |      |    |     | R**  | 0000B |
| L36  | -  | -   | R**  | 0000C |   |      |   |    |     | R**  | 0000B |   |      |    |     | R**  | 0000B |
| L37  | -  | -   | R**  | 0000C |   |      |   |    |     | R**  | 0000B |   |      |    |     | R**  | 0000B |
| L38  | -  | -   | R**  | 0000C |   |      |   |    |     | R**  | 0000B |   |      |    |     | R**  | 0000B |
| L39  | -  | -   | R**  | 0000C |   |      |   |    |     | R**  | 0000B |   |      |    |     | R**  | 0000B |
| L40  | -  | -   | R**  | 0000C |   |      |   |    |     | R**  | 0000B |   |      |    |     | R**  | 0000B |
| L41  | -  | -   | R**  | 0000C |   |      |   |    |     | R**  | 0000B |   |      |    |     | R**  | 0000B |
| L42  | -  | -   | R**  | 0000C |   |      |   |    |     | R**  | 0000B |   |      |    |     | R**  | 0000B |
| L43  | -  | -   | R**  | 0000C |   |      |   |    |     | R**  | 0000B |   |      |    |     | R**  | 0000B |
| L44  | -  | -   | R**  | 0000C |   |      |   |    |     | R**  | 0000B |   |      |    |     | R**  | 0000B |
| L45  | -  | -   | R**  | 0000C |   |      |   |    |     | R**  | 0000B |   |      |    |     | R**  | 0000B |
| L46  | -  | -   | R**  | 0000C |   |      |   |    |     | R**  | 0000B |   |      |    |     | R**  | 0000B |
| L47  | -  | -   | R**  | 0000C |   |      |   |    |     | R**  | 0000B |   |      |    |     | R**  | 0000B |
| L48  | -  | -   | R**  | 0000C |   |      |   |    |     | R**  | 0000B |   |      |    |     | R**  | 0000B |
| L49  | -  | -   | R**  | 0000C |   |      |   |    |     | R**  | 0000B |   |      |    |     | R**  | 0000B |
| L50  | -  | -   | R**  | 0000C |   |      |   |    |     | R**  | 0000B |   |      |    |     | R**  | 0000B |
| L51  | -  | -   | R**  | 0000C |   |      |   |    |     | R**  | 0000B |   |      |    |     | R**  | 0000B |
| L52  | -  | -   | R**  | 0000C |   |      |   |    |     | R**  | 0000B |   |      |    |     | R**  | 0000B |
| L53  | -  | -   | R**  | 0000C |   |      |   |    |     | R**  | 0000B |   |      |    |     | R**  | 0000B |
| L54  | -  | -   | R**  | 0000C |   |      |   |    |     | R**  | 0000B |   |      |    |     | R**  | 0000B |
| L55  | -  | -   | R**  | 0000C |   |      |   |    |     | R**  | 0000B |   |      |    |     | R**  | 0000B |
| L56  | -  | -   | R**  | 0000C |   |      |   |    |     | R**  | 0000B |   |      |    |     | R**  | 0000B |
| L57  | -  | -   | R**  | 0000C |   |      |   |    |     | R**  | 0000B |   |      |    |     | R**  | 0000B |
| L58  | -  | -   | R**  | 0000C |   |      |   |    |     | R**  | 0000B |   |      |    |     | R**  | 0000B |
| L59  | -  | -   | R**  | 0000C |   |      |   |    |     | R**  | 0000B |   |      |    |     | R**  | 0000B |
| L60  | -  | -   | R**  | 0000C |   |      |   |    |     | R**  | 0000B |   |      |    |     | R**  | 0000B |
| L61  | -  | -   | R**  | 0000C |   |      |   |    |     | R**  | 0000B |   |      |    |     | R**  | 0000B |
| L62  | -  | -   | R**  | 0000C |   |      |   |    |     | R**  | 0000B |   |      |    |     | R**  | 0000B |
| L63  | -  | -   | R**  | 0000C |   |      |   |    |     | R**  | 0000B |   |      |    |     | R**  | 0000B |
| L64  | -  | -   | R**  | 0000C |   |      |   |    |     | R**  | 0000B |   |      |    |     | R**  | 0000B |
| L65  | -  | -   | R**  | 0000C |   |      |   |    |     | R**  | 0000B |   |      |    |     | R**  | 0000B |
| L66  | -  | -   | R**  | 0000C |   |      |   |    |     | R**  | 0000B |   |      |    |     | R**  | 0000B |
| L67  | -  | -   | R**  | 0000C |   |      |   |    |     | R**  | 0000B |   |      |    |     | R**  | 0000B |
| L68  | -  | -   | R**  | 0000C |   |      |   |    |     | R**  | 0000B |   |      |    |     | R**  | 0000B |
| L69  | -  | -   | R**  | 0000C |   |      |   |    |     | R**  | 0000B |   |      |    |     | R**  | 0000B |
| L70  | -  | -   | R**  | 0000C |   |      |   |    |     | R**  | 0000B |   |      |    |     | R**  | 0000B |

\*\*\*\*\*  
 CENCA INFORMATION\*\*\*\*\*

[illegible]

| VAR. | NAME | TYPE | REL. | ADDR. | - VAR. | NAME  | TYPE | REL. | ADDR. | VAR. | NAME | TYPE | REL. | ADDR. |
|------|------|------|------|-------|--------|-------|------|------|-------|------|------|------|------|-------|
| PI   | N#4  | N#4  | N#F. | TPL   | R#4    | CUCUQ |      |      |       |      |      |      |      |       |

[illegible]

| A4E | TYPE | REL. | ADDR.  | VAR. | NAME | TYPE | REL. | ADDR.  | VAR. | NAME | TYPE | REL.   | ADDR. |
|-----|------|------|--------|------|------|------|------|--------|------|------|------|--------|-------|
| FN  | H#4  | N.R. | C0C018 | #SIG | SIG  | R#4  | N.R. | C0C0C4 | #NG  | NG   | R#4  | 00UCOC |       |
|     | H#4  |      | ZX     | ZY   |      |      |      |        |      |      |      |        |       |

LABEL ADDR LABEL ADDR LABEL ADDR LABEL ADDR LABEL ADDR

PAGE 005

2 001F4 100 000200 103 000212

```
1 *OPTIONS IN EFFECT*
NAME= MAIN,OPT=02,LANE CNT=32,SIZE=0.001K.
```

3 \*OPTIONS IN EFFECT\*

```
#STATISTICS# SOURCE STATEMENTS = 37 , PROGRAM SIZE = 890
```

\*STATISTICS\* NO DIAGNOSTICS GENERATED

# END OF COMPILATION

173K EYTES OF CORE NOT USED

LEVEL 21.0 (DEC 72)

DATE ... 76.324/21.53.40

```
CCCOMPILER OPTIONS - NAME= MAIN.CFT=2,LINECNT=52,SIZE=3000K,
SOURCE=CCDIC,NLTS1,NLCCCHK,LOCAL,MAP,NGED IT,IC,XREF
SUBROUTINE GENSG(C,CUT,CIN,TRCCE,S,KI)
```

6  
7  
8  
9  
10  
11

COMPUTES FRESNEL MATRIX ELEMENTS MULTIPLIED BY  
FACTORS APPROPRIATE TO SCATTERING

```

DIMENSION CIA(3),CUT(3),S(6)
COMMON/FREN/FN,*SI,*SIGZ,ANG(3),ZX,ZY
COMMON/CONST/PI,PI1
FACTORS APPROPRIATE TO SCATTERING

```

```

GENERATE ANGULAR FACTORS
CUSCHI=(1.-(COUT(4)*CIN(4)+COUT(5)*CIN(5)+COUT(6)*CIN(6)))/.5.

```

```

CCSCFI=SUB1(C13CH1)
CCSHIF=-CIN(2)
C2=SUB1(CCU1(4)-C14(4))*2+(CU1(5)-CIN(5))*2+(CU1(6)-CIN(6))*2

```

[illegible]

PACIFIC/COSTIN/CUSH  
GENERAL-PACIFIC/FRESNEL MATRIX ELEMENTS  
COSHTH=3\*HT(1)-(1-COSCHT)\*CSCCH/(N\*(N+1))  
COSHTH=(N+CSCCH)/(N+CSCCH)  
XPRP=(COSCH-FN+COSHTH)/(COSCH+FNCOSHHT)

$$S(1) = 511 \quad S(2) = 512$$

$$S(1) = (511 + 1) \cdot 2 / 2.$$
$$S(E) = 544$$
$$S(a) = c$$

$E(E) = 525$

215-62

(151)

5

22

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```

134 0035 X=XMC-1.
134 0036 X=XMC/XN
134 0037 DO 1 KK=1,2
134 0038 IF (KK.EC.2) GO TO 1
134 0039 IF (IND.EC.1).AND.(KK.EC.2) GO TO 1
134 0040 WRITE (6,61) KK
134 0041 ANCRMEFACT=PI
134 0042 ANCRME=XNCRM*XMC
134 0043 ANCRME2=XNCRM**2
134 0044 NALDE=NALE
134 0045 IF ((IR.EC.EC.1).AND.(IRSECT.EC.1)) NALEL=1
134 0046 DO 10 IALDEI,NALUL
134 0047 WRITE (6,61) IALDEI
134 0048 WRITE (6,61)
134 0049 NALDE=IALDE
134 0050 CALL ALBERC (NALDE,ALDPT)
134 0051 IF (NALDE.EC.1) WRITE (6,62) NALE
134 0052 DO 20 IGE1,3
134 0053 IF ((IND.EC.5).OR.(IND.EC.7).AND.(IC.EC.1)) GO TO 20
134 0054 WRITE (6,62) IGE1
134 0055 IF ((IFL.EC.1) .AND. (WRITE (6,63)
134 0056 IF (IFL.EC.2) WRITE (6,63)
134 0057 WRITE (6,63) FITIT (1,IFL), FITIT (2,IFL), FITIT (1,IFL), FITIT (2,IFL)
134 0058 DO 30 IGE1,NSCL
134 0059 DO 40 NSCE1,3
134 0060 VAV(NSC)=VSAMP2 (IU,IS,NSC,KK,IALD)*XNCRM
134 0061 VSIG(NSC)=VSAMP3 (IU,IS,NSC,KK,IALD)*XNCRM2
134 0062 VSIG(NSC)=XNCRM*(VSIG(NSC)*XMC-VAV(NSC)*VAV(NSC))
134 0063 IF (VSIG(NSC).LT.0.) VSIG(NSC)=0.
134 0064 VSIG(NSC)=SQRT (VSIG(NSC))
134 0065 CONTINUE
134 0066 WRITE (6,64) IS, (VAV(NSC),VSIG(NSC),NSC=1,3)
134 0067 CONTINUE
134 0068 IF (IFL.EC.1) WRITE (6,65)
134 0069

```

```

134 0070 IF (IFL.EC.2) WRITE (6,652)
134 0071 WRITE (6,65) FITIT (1,IFL), FITIT (2,IFL), FITIT (1,IFL), FITIT (2,IFL)
134 0072 DO 50 IGE1,NSCL
134 0073 VSET (IS)=0.
134 0074 DO 60 NSCE1,3
134 0075 VAV(NSC)=VSAMP2 (IU,IS,NSC,KK,IALD)*XNCRM
134 0076 VSIG(NSC)=VSAMP3 (IU,IS,NSC,KK,IALD)*XNCRM2
134 0077 VSIG(NSC)=XNCRM*(VSIG(NSC)*XMC-VAV(NSC)*VAV(NSC))
134 0078 VSE(NSC)=VSIG(NSC)/XMC
134 0079 IF (VSE(NSC).LE.0.) VSE(NSC)=0.
134 0080 VSET (IS)=VSET (IS)+VSE(NSC)/XMC
134 0081 CONTINUE
134 0082 IF (VSET (IS).LE.0.) VSET (IS)=0.
134 0083 VSET (IS)=SQRT (VSET (IS))
134 0084 WRITE (6,66) IS, (VAV(NSC),VSE(NSC),NSC=1,3)
134 0085 CONTINUE
134 0086 WRITE (6,67)
134 0087 WRITE (6,67) (IS,*S(IS),VSET (IS),IS=1,NSCL)
134 0088
134 0089 C
134 0090 C
134 0091 C
134 0092 C
134 0093 C
134 0094 C
134 0095 C
134 0096 C
134 0097 C
134 0098 C
134 0099 C
134 0100 C
134 0101 C
134 0102 C
134 0103 C
134 0104 C
134 0105 C
134 0106 C
134 0107 C
134 0108 C
134 0109 C
134 0110 C
134 0111 C
134 0112 C
134 0113 C
134 0114 C
134 0115 C
134 0116 C
134 0117 C
134 0118 C
134 0119 C
134 0120 C

```

**SPECIAL AGENTS**

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**SECRET**

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**PAGE 004**

REFERENCE LISTING\*\*\*\*\*

\*\*\*\*\*  
C E T 2 A 2

[illegible]

| LABEL | DEFINED | REFERENCES     |
|-------|---------|----------------|
| 1     | 0120    | 0037 0038 0040 |
| 10    | 0119    | 0049           |
| 20    | 0118    | 0055           |
| 30    | 0077    | 0056           |
| 40    | 0072    | 0064           |
| 50    | 0058    | 0065           |
| 60    | 0051    | 0066           |
| 100   | 0117    | 0082           |
| 101   | 0125    | 0093           |
| 102   | 0116    | 0102           |
| 103   | 0114    | 0109           |
| 001   | 0018    | 0042           |

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## INTERNAL STATEMENT NUMBERS

SYMBOL

J 0117 0118 0124 0124  
 AL 0117 0118 0124 0124  
 CL 0117 0118 0124 0124  
 CG 0117 0118 0124 0124  
 PR 0117 0118 0124 0124  
 LJ 0117 0118 0124 0124  
 JI 0117 0118 0124 0124  
 J2 0117 0118 0124 0124  
 KK 0117 0118 0124 0124  
 PI 0117 0118 0124 0124  
 US 0117 0118 0124 0124  
 VS 0117 0118 0124 0124  
 WS 0117 0118 0124 0124  
 AUS 0117 0118 0124 0124  
 ALU 0117 0118 0124 0124  
 CHT 0117 0118 0124 0124  
 CZU 0117 0118 0124 0124  
 FLX 0117 0118 0124 0124  
 FNU 0117 0118 0124 0124  
 IFL 0117 0118 0124 0124  
 IJ2 0117 0118 0124 0124  
 IJ3 0117 0118 0124 0124  
 IND 0117 0118 0124 0124  
 MOD 0117 0118 0124 0124  
 SZU 0117 0118 0124 0124  
 TPI 0117 0118 0124 0124  
 UNR 0117 0118 0124 0124  
 VNR 0117 0118 0124 0124  
 XNH 0117 0118 0124 0124  
 XN2 0117 0118 0124 0124  
 AEPF 0117 0118 0124 0124  
 AMTF 0117 0118 0124 0124  
 AREG 0117 0118 0124 0124  
 CINR 0117 0118 0124 0124  
 CREC 0117 0118 0124 0124  
 FACT 0117 0118 0124 0124  
 FMTF 0117 0118 0124 0124  
 FTJF 0117 0118 0124 0124  
 IABJ 0117 0118 0124 0124  
 IALJ 0117 0118 0124 0124  
 IFCI 0117 0118 0124 0124  
 IFC3 0117 0118 0124 0124  
 IMTF 0117 0118 0124 0124  
 IQUV 0117 0118 0124 0124  
 IREC 0117 0118 0124 0124  
 ISUN 0117 0118 0124 0124  
 MALB 0117 0118 0124 0124  
 NALJ 0117 0118 0124 0124  
 NSOL 0117 0118 0124 0124  
 SANC 0117 0118 0124 0124  
 SOLC 0117 0118 0124 0124  
 TUIF 0117 0118 0124 0124  
 WSUN 0117 0118 0124 0124  
 XCAP 0117 0118 0124 0124  
 ALBPT 0117 0118 0124 0124  
 ARCJS 0117 0118 0124 0124  
 AUNIF 0117 0118 0124 0124  
 CLOUD 0117 0118 0124 0124  
 CNTRX 0117 0118 0124 0124  
 CNTRY 0117 0118 0124 0124  
 EDGEX 0117 0118 0124 0124  
 EUGLY 0117 0118 0124 0124  
 FACTR 0117 0118 0124 0124  
 IFACE 0117 0118 0124 0124  
 IIREC 0117 0118 0124 0124  
 IRESD 0117 0118 0124 0124  
 IRGLD 0117 0118 0124 0124  
 IRPAT 0117 0118 0124 0124  
 NALUL 0117 0118 0124 0124  
 NCLDI 0117 0118 0124 0124  
 NFRUL 0117 0118 0124 0124  
 NUNIF 0117 0118 0124 0124  
 VSAMP 0117 0118 0124 0124

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XFACE 0033 0024 0030  
 ANCHRM 0017 0018 0054  
 ALBUDJ 0055 0111 0042 0045 0047 0053 0055 0076 0078 0084 0086  
 INFLUX 0011 0040

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\*\*\*\*\* C M T H A N C R C S S R E F E R E N C E L I S T I N G \*\*\*\*\*

SYMBOL INTERNAL STATEMENT NUMBERS

INSHUT 0006 0070  
 INSHUT 0008  
 OUTPUT 0002  
 POINTR 0011  
 RECAN 0011

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\*\*\*\*\* C M T H A N C R C S S R E F E R E N C E L I S T I N G \*\*\*\*\*

LABEL DEFINED REFERENCES

| LABEL | DEFINED | REFERENCES     |
|-------|---------|----------------|
| 1     | 0127    | 0057           |
| 2     | 0057    | 0057           |
| 3     | 0102    | 0051           |
| 10    | 0128    | 0019 0020 0022 |
| 20    | 0068    | 0059           |
| 21    | 0068    | 0062           |
| 22    | 0068    | 0072           |
| 30    | 0058    | 0074           |
| 40    | 0113    | 0109           |
| 50    | 0126    | 0114           |
| 51    | 0126    | 0117           |
| 750   | 0047    | 0078           |
| 800   | 0131    | 0039           |
| 801   | 0132    | 0044           |
| 802   | 0132    | 0045           |
| 803   | 0132    | 0051 0082      |
| 804   | 0132    | 0080           |
| 805   | 0132    | 0100           |
| 806   | 0132    | 0034           |
| 807   | 0132    | 0036           |
| 808   | 0132    | 0040           |
| 809   | 0141    | 0050           |
| 810   | 0142    | 0108           |
| 821   | 0142    | 0112           |
| 825   | 0144    | 0116           |
| 826   | 0146    | 0124           |
| 827   | 0146    | 0103           |

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SIZE OF PROGRAM CODES HEXADECIMAL BYTES PAGE 006

| NAML   | J    | SF   | TAG  | TYPE | ADD.   | NAME   | TAG  | TYPE | ADD. | NAME   | TAG  | TYPE | ADD. |
|--------|------|------|------|------|--------|--------|------|------|------|--------|------|------|------|
| ANCHRM | 0017 | 0018 | 0054 | 104  | 0004A0 | ANCHRM | 0017 | 0018 | 0054 | ANCHRM | 0017 | 0018 | 0054 |
| ALBUDJ | 0055 | 0111 | 0042 | 104  | 0004A0 | ALBUDJ | 0055 | 0111 | 0042 | ALBUDJ | 0055 | 0111 | 0042 |
| INFLUX | 0011 | 0040 |      | 104  | 0004A0 | INFLUX | 0011 | 0040 |      | INFLUX | 0011 | 0040 |      |
| INSHUT | 0006 | 0070 |      | 104  | 0004A0 | INSHUT | 0006 | 0070 |      | INSHUT | 0006 | 0070 |      |
| INSHUT | 0008 |      |      | 104  | 0004A0 | INSHUT | 0008 |      |      | INSHUT | 0008 |      |      |
| OUTPUT | 0002 |      |      | 104  | 0004A0 | OUTPUT | 0002 |      |      | OUTPUT | 0002 |      |      |
| POINTR | 0011 |      |      | 104  | 0004A0 | POINTR | 0011 |      |      | POINTR | 0011 |      |      |
| RECAN  | 0011 |      |      | 104  | 0004A0 | RECAN  | 0011 |      |      | RECAN  | 0011 |      |      |
| ANCHRM | 0017 | 0018 | 0054 | 104  | 0004A0 | ANCHRM | 0017 | 0018 | 0054 | ANCHRM | 0017 | 0018 | 0054 |
| ALBUDJ | 0055 | 0111 | 0042 | 104  | 0004A0 | ALBUDJ | 0055 | 0111 | 0042 | ALBUDJ | 0055 | 0111 | 0042 |
| INFLUX | 0011 | 0040 |      | 104  | 0004A0 | INFLUX | 0011 | 0040 |      | INFLUX | 0011 | 0040 |      |
| INSHUT | 0006 | 0070 |      | 104  | 0004A0 | INSHUT | 0006 | 0070 |      | INSHUT | 0006 | 0070 |      |
| INSHUT | 0008 |      |      | 104  | 0004A0 | INSHUT | 0008 |      |      | INSHUT | 0008 |      |      |
| OUTPUT | 0002 |      |      | 104  | 0004A0 | OUTPUT | 0002 |      |      | OUTPUT | 0002 |      |      |
| POINTR | 0011 |      |      | 104  | 0004A0 | POINTR | 0011 |      |      | POINTR | 0011 |      |      |
| RECAN  | 0011 |      |      | 104  | 0004A0 | RECAN  | 0011 |      |      | RECAN  | 0011 |      |      |
| ANCHRM | 0017 | 0018 | 0054 | 104  | 0004A0 | ANCHRM | 0017 | 0018 | 0054 | ANCHRM | 0017 | 0018 | 0054 |
| ALBUDJ | 0055 | 0111 | 0042 | 104  | 0004A0 | ALBUDJ | 0055 | 0111 | 0042 | ALBUDJ | 0055 | 0111 | 0042 |
| INFLUX | 0011 | 0040 |      | 104  | 0004A0 | INFLUX | 0011 | 0040 |      | INFLUX | 0011 | 0040 |      |
| INSHUT | 0006 | 0070 |      | 104  | 0004A0 | INSHUT | 0006 | 0070 |      | INSHUT | 0006 | 0070 |      |
| INSHUT | 0008 |      |      | 104  | 0004A0 | INSHUT | 0008 |      |      | INSHUT | 0008 |      |      |
| OUTPUT | 0002 |      |      | 104  | 0004A0 | OUTPUT | 0002 |      |      | OUTPUT | 0002 |      |      |
| POINTR | 0011 |      |      | 104  | 0004A0 | POINTR | 0011 |      |      | POINTR | 0011 |      |      |
| RECAN  | 0011 |      |      | 104  | 0004A0 | RECAN  | 0011 |      |      | RECAN  | 0011 |      |      |

\*\*\*\*\* COMMON INFORMATION \*\*\*\*\*

[illegible]

```

C----- COMPILER OPTIONS - NAME= MAIN,CFT=2,LINECT=62,SIZE=9000K,
C SOURCE=EDCDDIC,NCLIST,NCCCK(LCA3),MAP,NCCDIT,IC,KREF
C SUBROUTINE ALBUDC,ALBPT
C COMMON/UNDA/ALB(ALB(50),ALB(2))
C COMMON/AP1/ALBPT,ALBPT(50),ALBPT(50),ALBPT(50)
C COMMON/MT/CCM/MTCT,NRREG,INTF
C-----
C SUBROUTINE ALBUDC
C THIS SUBROUTINE SERVES TWO FUNCTIONS
C A) IF IALB.GT.0 ALBUDC COMPLETES AND RETURNS THE VALUE OF THE
C SECOND ALBUDC AT THE POINT X=CG(1), Y=CG(2) FOR THE ALBUDC
C PATTERN SPECIFIED BY IALB.
C B) IF IALB.LT.0 ALBUDC PRINTS A DESCRIPTION OF THE ALBUDC
C PATTERN SPECIFIED BY IALB.
C-----
C VERSION FOR
C SINUSCUDAL ALBUDC PATTERNS FOR MTF DERIVATION
C-----
C DIMENSION FREQ(20),AUN(10)
C DATA FREQ/1.0,2.0,4.0,8.0,1.0,2.0,4.0,6.0,8.0,1.0,2.0,1.0,2.0,
C 14.0,16.0,18.0,20.0/
C AUN/1.0,7.0,6.0,5.0,4.0,2.0,1.95,1.50,1.0,0.7/
C NUNIF=10
C INTF=1
C NREQ=20
C IF(AUNIF(1).EQ.AUN(1))GO TO 201
C JC=20 I=1,NUNIF
C AUNIF(I)=AUN(I)
C NA=(NALE-NUNIF)/2
C UC=20 I=1,NA
C FNU(1)=FREQ(1)
C CONTINUE
C PI=3.141593
C TPI=2.*PI
C JI=5
C IF(MALB.GT.0)GO TO 102
C XALB=IALB*(IALB)
C SINUSCUDS
C IALB=(NALB-1)/2+1
C IUNREQD=(NALB-1.2)
C F=FLCAT(IUNREQD)
C ALBPT=0.
C IF(IALB.GE.0)ALBPT=BC+JUNREQD*(TPI*CG(1)+FREQ(IALB)+F*PI)
C IF(IALB.LT.0)ALBPT=ALB(6.111)*NALB,CG(1),FREQ(IALB),F
C RETURN
C UNIFORM PLANE
C CONTINUE
C IALB=VALJ-30
C XALB=AUN(IALB)
C IF(IALB.LE.0)WRITE(6,120)NALB,XALB
C IF(IALB.GT.0)ALBPT=XALB
C RETURN
C 120 FORMAT(1H,12,'-- UNIFORM PLANE, Z =',F7.4,' EVERYWHERE')
C 111 FORMAT(1H,12,'-- SINUSCUDAL PATTERN,')
C 1H,2X,A=(',F6.3,')+(',F6.3,')*CCS(2,PI*NU*X+F*PI)')
C 1H,5X,VAL = ',G14.7,'CYCLES/KM., F = ',F3.0)
C END

```

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| SYMBOL | INTERNAL STATEMENT NUMBERS |
|--------|----------------------------|
| F      | 0028 0030 0032             |
| I      | 0013 0014 0016 0017 0017   |
| UO     | 0021 0030 0032             |
| QI     | 0022 0030 0032             |
| CC     | 0015 0016 0020 0030        |
| PI     | 0015 0016 0020 0030        |
| ALB    | 0027 0011 0014 0037        |
| AUN    | 0027 0011 0014 0037        |
| LOS    | 0027 0011 0014 0037        |

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\*\*\*\*\* F C H T K A N C R C S S R E F E R E N C E L I S T I N G \*\*\*\*\*

LABEL DEFINED REFERENCES

102 0024  
111 0024  
120 0024  
200 0014  
201 0011  
202 0010

ALBEC / SIZE OF PROGRAM 000482 HEXADECIMAL BYTES PAGE 004

| NAME     | TAG | TYPE | ADD.   | NAME     | TAG | TYPE | ADD.   | NAME     | TAG | TYPE | ADD.   |
|----------|-----|------|--------|----------|-----|------|--------|----------|-----|------|--------|
| F SFA    | C   | R#4  | 00014C | EO SFA   | C   | R#4  | 000154 | ALB      | C   | R#4  | 000158 |
| CG FA    | C   | R#4  | 00014C | FI SFA   | C   | R#4  | 000160 | AEFF     | C   | R#4  | N.R.   |
| ALN F    | C   | R#4  | 00018A | TPB SFA  | C   | R#4  | 000164 | IBND SFA | C   | R#4  | 00016C |
| FREQ FA  | C   | R#4  | 0001AC | IALB SFA | C   | R#4  | 000174 | NALB F   | C   | R#4  | 000000 |
| INAL SFA | C   | R#4  | 000170 | ALB SFA  | C   | R#4  | 000174 | AFREG S  | C   | R#4  | 000050 |
| JALB SF  | C   | R#4  | 000178 | ALBIF S  | C   | R#4  | 00017C | IBCCM# F | XF  | R#4  | 000000 |
| NUNIF SF | C   | R#4  | 00000C | CUS      | XF  | R#4  | 000000 |          |     |      |        |

\*\*\*\*\* COMMON INFORMATION \*\*\*\*\*

NAME OF COMMON BLOCK \* GND\* SIZE OF BLOCK 000004 HEXADECIMAL BYTES

| VAR. NAME | TYPE | REL. ADDR. | VAR. NAME | TYPE | REL. ADDR. | VAR. NAME | TYPE | REL. ADDR. |
|-----------|------|------------|-----------|------|------------|-----------|------|------------|
| NALB      | R#4  | 00000C     | ALB       | R#4  | N.R.       | CG        | R#4  | 00000C     |

NAME OF COMMON BLOCK \* AFIT\* SIZE OF BLOCK 00025C HEXADECIMAL BYTES

| VAR. NAME | TYPE | REL. ADDR. | VAR. NAME | TYPE | REL. ADDR. | VAR. NAME | TYPE | REL. ADDR. |
|-----------|------|------------|-----------|------|------------|-----------|------|------------|
| NUNIF     | R#4  | 00000C     | ALBIF     | R#4  | 00000C     | FIUT      | R#4  | N.R.       |

NAME OF COMMON BLOCK \*MTFCOM\* SIZE OF BLOCK 000058 HEXADECIMAL BYTES

| VAR. NAME | TYPE | REL. ADDR. | VAR. NAME | TYPE | REL. ADDR. | VAR. NAME | TYPE | REL. ADDR. |
|-----------|------|------------|-----------|------|------------|-----------|------|------------|
| FNU       | R#4  | 00000C     | NFREQ     | R#4  | 00005C     | INTF      | R#4  | 000054     |

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| LABEL | ADDR   | LABEL | ADDR   | LABEL | ADDR   |
|-------|--------|-------|--------|-------|--------|
| 200   | 000232 | 202   | 00020C | 201   | 000208 |
|       |        |       |        | 102   | 0002E2 |

\*OPTIONS IN EFFECT\* NAME= MAIN,OPT=02,LINECNT=82,SIZE=0000C,

\*OPTIONS IN EFFECT\* SOURCE=ECDCIC,NULIST=NOJDECK,LCIC,NAP,NCLDIT,IC,XREF

\*STATISTICS\* SOURCE STATEMENTS = 44 ,PROGRAM SIZE = 1154

\*STATISTICS\* NO DIAGNOSTICS GENERATED

\*\*\*\*\* END OF COMPILATION \*\*\*\*\*

173K BYTES OF CORE NOT USED

COMPILER OPTIONS - NAME= MAINAUF2.LINENIT=82.SI2E=000JK.  
SOU=CS+EDGHE+MLIST+NUDECK+LCAD+MAP+NEEUIT+IG+XREF  
STRUCTURE AREG(NALB,AL,BL)  
DIMENSION Y(50),X(50)  
COMMON/AFIT/NUMIF,NUMIF(50),FTCT(50),AEFF(50)  
IF(NALB.LE.1)RETURN  
IF(ENUNIF-1  
IDENALB=NUMIF  
CC 1 151,IMI  
IDENALB=1  
Y=FTCT(IP)-FTCT(NALB)  
X(1)=Y/AUNIF(1)  
X(1)=Y  
1 CONTINUE  
CALL LINFIT(IMI,Y,X,AL,BL)  
ADENALB=1  
PC 2 151,ICD  
P=FTCT(1)-FTCT(NALB)  
AEFF(J)=P/(AL+BL\*1)  
2 CONTINUE  
AEFF(NALB)=1.  
RETURN  
END

\*\*\*\*\*C-A-I-A-N-C-A-C-S-F-E-R-E-N-C-E-L-I-S-T-I-N-G\*\*\*\*\* PAGE-002

| SYMBOL |      | INTERNAL STATEMENT NUMBERS |           |
|--------|------|----------------------------|-----------|
| I      | CC05 | CC13                       | CC12 CC13 |
| J      | CC17 | CC18                       | CC19      |
| X      | CC23 | CC18                       | CC15      |
| Y      | CC23 | CC12                       | CC15      |
| AL     | CC32 | CC13                       | CC12      |
| BL     | CC32 | CC13                       | CC12      |
| FI     | CC18 | CC19                       | CC19      |
| ID     | CC19 | CC13                       | CC13      |
| IP     | CC19 | CC11                       | CC11      |
| YY     | CC11 | CC12                       | CC13      |
| IDD    | CC16 | CC17                       | CC15      |
| IMH    | CC24 | CC19                       | CC21      |
| AEFF   | CC24 | CC22                       |           |
| APEG   | CC24 | CC22                       |           |
| FTUT   | CC24 | CC11                       | CC18      |
| NALB   | CC22 | CC22                       | CC16      |
| AUNIF  | CC22 | CC22                       |           |
| NUMIF  | CC24 | CC27                       | CC28      |
| LINFIT | CC25 |                            |           |

\*\*\*\*\*F-U-R-T-H-E-R-E-F-E-R-E-N-C-E-L-I-S-T-I-N-G\*\*\*\*\* PAGE-003

| LABEL | DEFINED | REFERENCES | /       |     | AREG / |     | SIZE OF PROGRAM 000396 HEXADECIMAL BYTES PAGE 004 |     |
|-------|---------|------------|---------|-----|--------|-----|---|-----|
|       |         |            | NAME    | TAG | NAME   | TAG | NAME  | TAG |
| 1     | CC14    | CC09       | AL SFA  | R*4 | CC09   | R*4 | CC09  | R*4 |
| 2     | CC20    | CC17       | IP SFA  | R*4 | CC17   | R*4 | CC17  | R*4 |
|       |         |            | AEFF S  | C   | CC15   | C   | CC15  | C   |
|       |         |            | AUNIF F | C   | CC24   | C   | CC24  | C   |

\*\*\*\*\*COMMON INFORMATION \*\*\*\*\*

| NAME OF COMMON BLOCK |      | * AFIT* SIZE OF BLOCK |           | CC025C HEXADECIMAL BYTES |            |
|----------------------|------|-----------------------|-----------|--------------------------|------------|
| VAR. NAME            | TYPE | REL. ADDR.            | VAR. NAME | TYPE                     | REL. ADDR. |
| NUMIF                | 1*4  | CC14                  | AUNIF     | R*4                      | CC09       |

| LABEL | ADDR | LABEL | ADDR | LABEL | ADDR | LABEL | ADDR | PAGE | 005 |
|-------|------|-------|------|-------|------|-------|------|------|-----|
|       |      |       |      |       |      |       |      |      |     |

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